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THAD T-7 MISSILE MONTE-CARLO TERMINAL HOMING SIMULATION UTILIZI--ETC(U)
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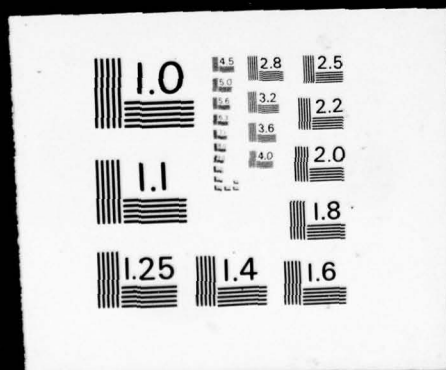
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TECHNICAL REPORT RG-7T-2

**THAD T-7 MSSSILE MONTE CARLO TERMINAL HOMING
SIMULATION UTILIZING ALS, DIGITAL/LINEAR AND TV
SEEKERS**

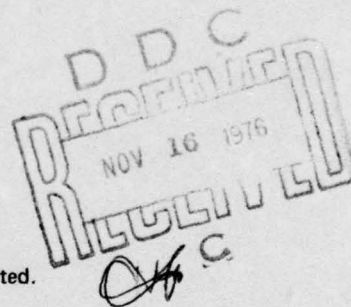
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1 JULY 1976

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U.S. ARMY MISSILE COMMAND

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The missile modeled in the program is the 7-in. HORNET airframe utilized as the basic flight test bed by the US Army Missile Command's Terminal Homing Accuracy Demonstration group. Two gimbaled seekers are modeled which null on the line-of-sight vector to provide an initial signal for proportional navigation guidance. Either model, one simulating a four-quadrant (laser) seeker (with digital and digital/linear signal processing logic options), and the other simulating a vidicon (optical contrast) seeker, can be optionally selected. Another input option permits simulation of either a direct fire (prelaunch target acquisition) mode, or an indirect fire (target acquisition after launch) mode. A number of print and plot output options provide versatility of data presentation.

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I. INTRODUCTION

The all-digital, Monte Carlo six degree of freedom (6 DOF) simulation program documented in this report provides a realistic method for the evaluation and analysis of a terminal homing weapons system. Missile hardware components, vehicle dynamics, environment descriptions, and target motion are simulated by identifiable program modules. In some cases (e.g., the actuator and autopilot modules), both high and low frequency models are available, allowing simulations to be tailored to user needs. The missile modeled in the program is the 7-in. HORNET airframe [1] utilized as the basic flight testbed by the US Army Missile Command's (MICOM's) Terminal Homing Accuracy Demonstration (THAD) group. Two gimballed seekers are modeled which null on the line-of-sight vector to provide an initial signal for proportional navigation guidance. Either model, one simulating a four-quadrant (laser) seeker (with digital and digital/linear signal processing logic options), and the other simulating a vidicon (optical contrast) seeker, can be optionally selected. Another input option permits simulation of either a direct fire (pre-launch target acquisition) mode, or an indirect fire (target acquisition after launch) mode. Preacquisition guidance during an indirect fire mode simulation is provided by a preprogrammed trajectory, where trajectory shaping can be accomplished by an input parameter. A number of print and plot output options provide versatility of data presentation. A Monte Carlo approach was developed for generating circular error probability (CEP) related information. This report presents a functional overview of the program, a detailed description of the individual modules and subroutines, a brief description (where appropriate) of the components modeled, and a guide to the use of the program.

II. FUNCTIONAL DESCRIPTION

The 6 DOF Monte Carlo Terminal Homing Simulation Program, shown in Figures 1 and 2, provides the capability of simulating flights of a THAD T-7 terminal homing seeker-missile under varying input conditions. The operation of the stochastic 6 DOF program is automatic when all initial conditions and time series error source distributions are specified along with the number of runs to be made. In the absence of Monte Carlo data inputs, the operation of the 6 DOF program reverts to that of the deterministic version.

Figure 1 is a flow chart of the executive control subroutines. This figure gives an overview of the basic program operation that is independent of hardware modeling and flight simulation. Control of the events shown in each of the blocks is accomplished primarily through use of input data read in on special card types. These card types are identified by numbers from 1 to 10. Section IV.A contains detailed explanations of each card type. A detailed description of Figure 1, along with an explanation of program flow relating to card type, is given in Section III.A.

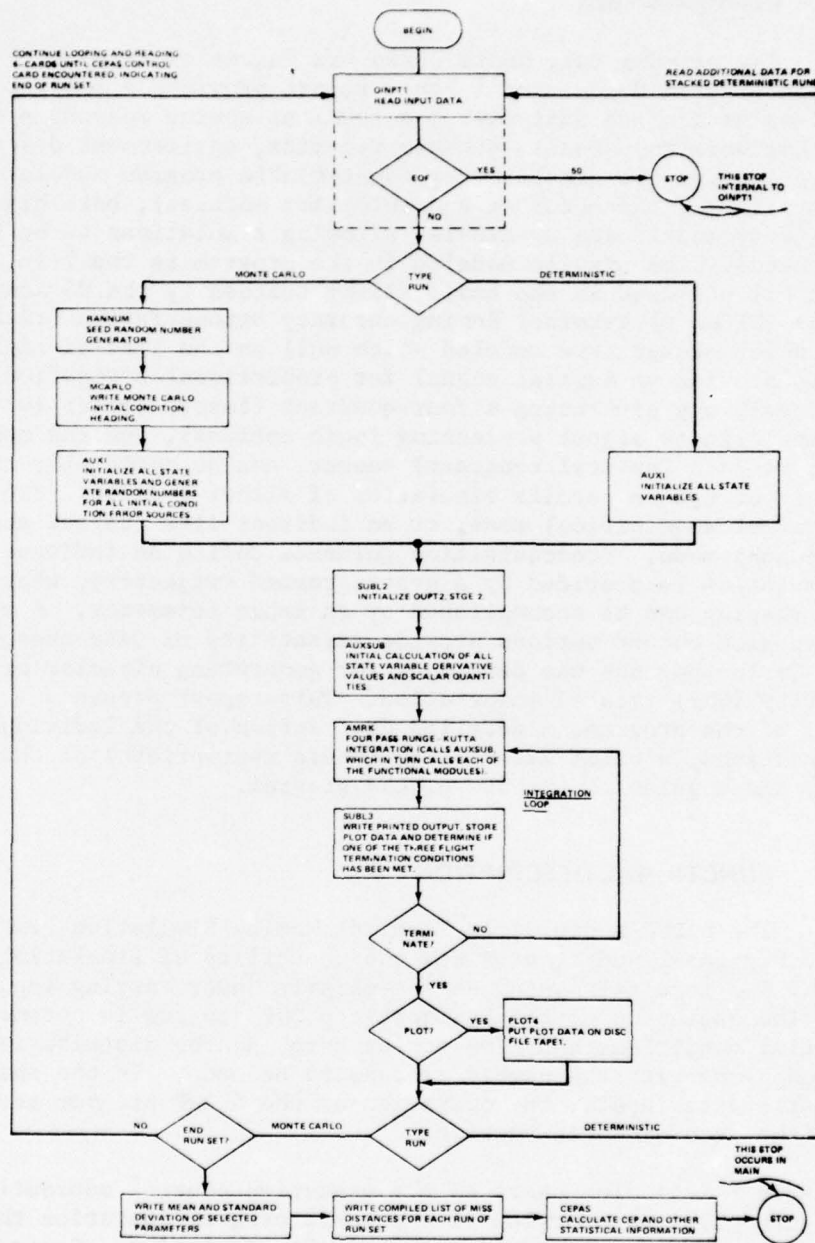


Figure 1. 6 DOF flowchart.

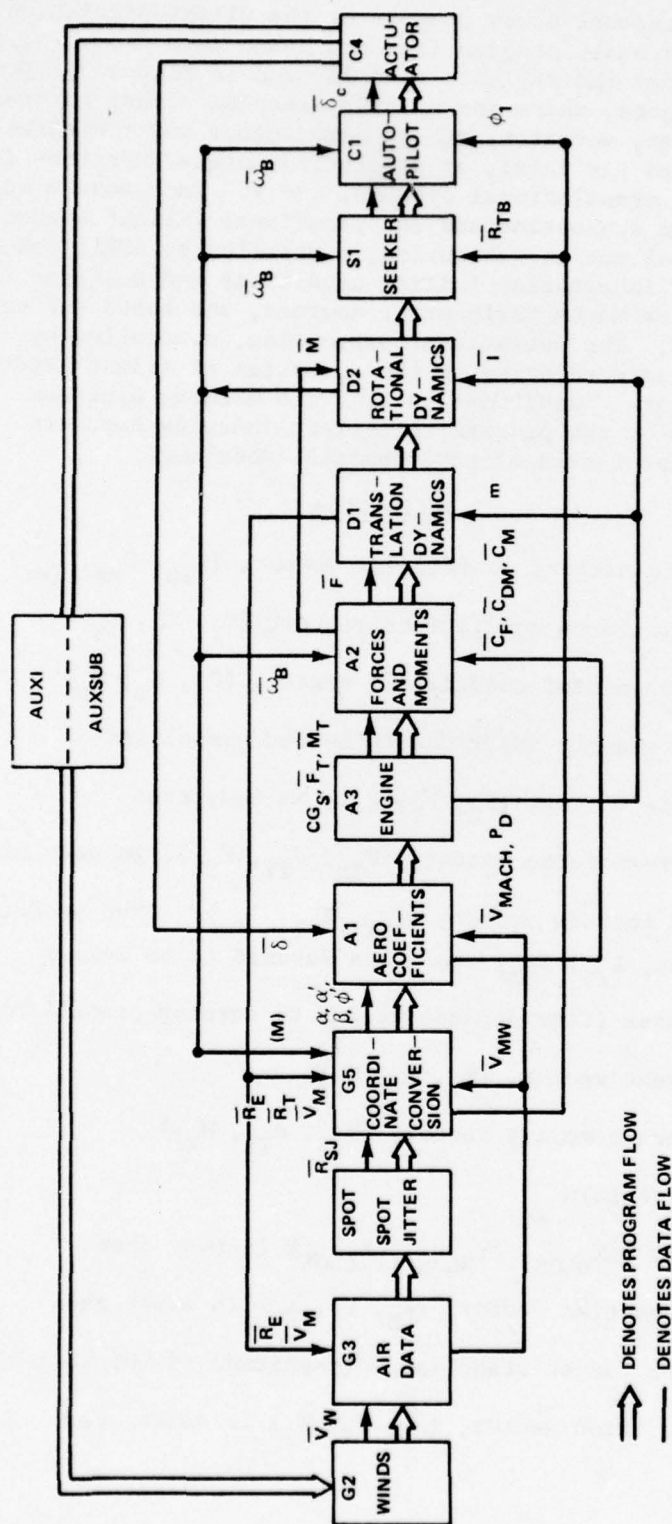


Figure 2. Modular block diagram.

Figure 2 is a functional block diagram of the flight simulation modules, depicting both basic program flow and basic data flow. A listing follows which defines the variable symbols used in Figure 2. The program is modularly designed, where the modules describe either hardware components (e.g., seeker, actuator, etc.), homogeneous environmental conditions (e.g., winds and air data), or simulation-unique functions (e.g., coordinate conversion, translational dynamic, etc.). Each module is made up of an initialization subroutine and an operational (flight execution) subroutine. The initialization subroutine, controlled by AUXI, calculates module constants, sets integration initial conditions and decision flags, draws random numbers for Monte Carlo error sources, and loads the numerical integration array. The operational subroutine, controlled by AUXSUB, contains all logic relating to the operation of flight hardware, time varying environmental conditions, etc. This modular approach facilitates adaptation of the program to reflect changing hardware components and different levels of environmental modeling.

<u>Variable</u>	<u>Definition</u>
\bar{C}_{DM}	Aerodynamic damping coefficient vector, $(C_{\ell p}, C_{mq}, C_{mr})$
\bar{C}_F	Aerodynamic force coefficient vector, (C_X, C_Y, C_Z)
\bar{C}_M	Aerodynamic moment coefficient vector, (C_ℓ, C_m, C_n)
CG_s	Center of gravity shift due to burned propellant
\bar{F}	Total force vector, (F_X, F_Y, F_Z) , in body axes
\bar{F}_T	Engine thrust force vector, (F_{TX}, F_{TY}, F_{TZ}) , in body axes
\bar{I}	Moment of inertia vector, (I_{XX}, I_{YY}, I_{ZZ}) . (The products of inertia, I_{XY}, I_{XZ} , etc., are assumed to be zero.)
m	Vehicle mass (time dependent, due to burning propellant)
\bar{M}	Total moment vector, (M_X, M_Y, M_Z)
\bar{M}_T	Engine thrust moment vector, (M_{TX}, M_{TY}, M_{TZ})
P_D	Dynamic pressure
\bar{R}_{TB}	LOS vector $(\Delta X_{BLOS}, \Delta Y_{BLOS}, \Delta Z_{BLOS})$ in body axes
\bar{R}_E	Missile position vector, (X_E, Y_E, Z_E) in earth axes
R_S	Missile to target slant range (magnitude of LOS vector)
\bar{R}_T	Target position vector, (X_T, Y_T, Z_T) in earth axes

<u>Variable</u>	<u>Definition</u>
\bar{R}_V	LOS vector, $(\Delta X_{LOS}, \Delta Y_{LOS}, \Delta Z_{LOS})$ in earth axes
\bar{V}_M	Missile velocity vector, (V_X, V_Y, V_Z) , in earth axes
V_{MACH}	Missile Mach number
\bar{V}_{MW}	Missile velocity vector, (V_{WX}, V_{WY}, V_{WZ}) , relative to the wind, in earth axes
\bar{V}_W	Wind velocity vector in earth axes
α	Missile angle of attack (pitch)
β	Missile angle of attack (yaw)
α'	Missile angle of attack (total)
ϕ_1	Euler roll angle measured between missile attitude gyro and body axes
ϕ'	Aerodynamic roll angle
$\bar{\delta}$	Fin position vector, $(\delta_1, \delta_2, \delta_3, \delta_4)$, for fins 1, 2, 3, and 4
$\bar{\delta}_c$	Commanded fin position vector, $(\delta_{c1}, \delta_{c2}, \delta_{c3}, \delta_{c4})$
$\bar{\omega}_\lambda$	Pitch and yaw rate command $(\omega_{\lambda Q}, \omega_{\lambda R})$ to autopilot from seeker
$\bar{\omega}_B$	Body angular rate vector, $(\omega_P, \omega_Q, \omega_R)$

The Monte Carlo approach takes advantage of the dual mode operation of the 6 DOF program. The initialization modules call MCARLO to randomize all initial condition error sources. Then in the flight execution module, MCARLO is called to generate time series random conditions.

III. SUBROUTINE DESCRIPTION

A. MAIN Program

MAIN is the primary executive routine of the simulation program. All subroutines and modules executed during a simulation run are either called from MAIN, or are called by subroutines or modules which are called by MAIN.

Figure 1 is a flow chart of MAIN. This figure illustrates executive subroutine flow that is independent of hardware modeling and flight simulation. Control of the events in each of the blocks is accomplished primarily through use of input data read in on special card types. These card types are identified by numbers ranging from 1 to 10. A detailed description of each card type is given in Section IV.A. The following will relate card type to program operation.

a. OINPT1 - Data Card Input Subroutine

This subroutine reads all input data and sorts the cards according to card type. If an end-of-file (EOF) is encountered in OINPT1, execution will be terminated. When a 6-card is encountered, OINPT1 stops reading data and control passes to the decision point shown immediately below OINPT1.

b. TYPE OF RUN - Deterministic or Monte Carlo

The type of run is dictated by the presence or absence of type 8-cards. If no 8-cards are encountered by OINPT1, the run is deterministic. If 8-cards are encountered, the run is Monte Carlo. (8-cards contain input data for random error sources.)

(1) RANNUM - Random Number Generator. This subroutine is called only if the run type is Monte Carlo. RANNUM seeds the random number sequence for the Monte Carlo run set. The seed is input by 3-card and must be an odd octal whole number. (Monte Carlo inputs are given in Section III.C.7).

(2) AUXI - Module Initialization Control Subroutine. This subroutine calls the modules shown in Figure 2 to initialize integrators and set decision flags. For Monte Carlo runs, random numbers are drawn for each of the error sources that are modeled in the modules. (A description of error sources is given in Section III.C). The program flow shown in Figure 2 is not hardwired into the program. The calling sequence is specified by 2-cards that are input through OINPT1; thus, any sequence may be used. However, the sequence shown is recommended due to the natural flow of the program and to the fact that some modules may initialize quantities that are required by other modules.

c. SUBL2 - Output Staging Subroutine

This subroutine calls OUP2, STEG2, and other executive subroutines as specified by 1-cards. Normally, only OUP2 and STEG2 are specified. STEG2 initializes some executive control flags. OUP2 initializes print and plot arrays.

d. AUXSUB - Operational Control Subroutine

This subroutine calls each of the modules shown in Figure 2. (AUXSUB calls the operational subroutine of each module, while AUXI calls the initialization subroutine of each module.) The operational subroutines are called to make the initial calculation of all state vector derivative values and scalar parameter values to initialize the numerical integration sequence.

As stated in b.(2), the program flow shown in Figure 2 is not hardwired into the program. AUXSUB calls the modules based on 2-card input data.

e. AMRK - Runge-Kutta Integration Subroutine

AMRK calls AUXSUB. AUXSUB then calls each of the operational subroutines of the modules shown in Figure 2. AMRK maintains control while making the four Runge-Kutta integration passes. When four passes have been completed (this completes an integration step), control passes to SUBL3.

f. SUBL3 - Output and Termination Control Subroutine

SUBL3 calls OUP3 to write output specified by 4-card and to store plot data specified by 7-card. Then SUBL3 calls STEG3, the integration control subroutine. STEG3 monitors flight time and flight termination switches. There are three conditions for flight termination. They are:

- 1) Ground impact (checked only if range to go is greater than 500 ft).
- 2) Target plane intercept.
- 3) Flight time exceeded.

The first two termination conditions are checked by G4, while the third is checked by STEG3.

g. TERMINATE

If none of the three flight termination conditions are met, control returns to AMRK and integration continues.

h. PLOT

Plotting is specified by 7-card. If 7-cards were input through OINPT1, then PLOT4 will be called at the end of each flight to store plot data on disc file TAPE1. TAPE1 is treated as an output file and must be disposed of at the end of the job to a remote terminal that has a Houston Instrument COMPILOT plotter. Section III.G.3 explains how to dispose of the plot file.

i. TYPE RUN - Deterministic or Monte Carlo

If the run is deterministic, control passes back to OINPT1. OINPT1 reads data for the next case. If no data cards are present, execution will terminate. If the run is Monte Carlo, control passes to the next decision point, END RUN SET.

j. END RUN SET

The end of the run set is indicated when the decision flag LSTEP is set to 11. LSTEP is set to 11 in OINPT1 when OINPT1 reads a 9-card. (A CEP control card must follow the 9-card.)

The number of runs in a set is dictated by the number of 6-cards input. Each 6-card generates one run. The end of the run set is indicated by placing a 9-card and a CEP control card in front of the last 6-card.

k. MEAN AND STANDARD DEVIATION

The mean and standard deviation of any parameter in the C-array may be calculated by specifying the parameter on a 10-card. The parameter value is sampled at the end of each flight (target impact), then the mean and standard deviation are calculated and printed at the end of the run set.

l. COMPILED LIST OF MISS DISTANCES

The Y and Z components and absolute magnitude of miss distance are compiled and printed at the end of each run set. The miss distances given in this list are then used to calculate a missile CEP. The miss distance components are referenced to the flight coordinate system described in Section II.C.10.

m. CEPAS - CEP Calculation Subroutine

The miss distance components (Y, Z) are saved from each run. Then a CEP, confidence intervals, and other statistical information are calculated from the set of miss distance components.

B. Modules

1. A1-Aerodynamic Coefficient Table Look-Up Subroutine

a. Functional Description

This subroutine utilizes the executive subroutines TABLE, TABL2, and TABL3 to retrieve the aerodynamic coefficients from data arrays stored in BLOCK DATA B. These aerodynamic coefficients are referenced to the wind axes coordinate system shown in Figure 3. For this coordinate system, a normal and axial force convention is used as opposed to a lift and drag force convention.

The independent variable arrays (Mach number, angle of attack, and fin setting) are stored in BLOCK DATA A.

The aerodynamic coefficient components and the independent variables of which they are a function are as follows:

- 1) Axial force coefficient at zero angle of attack -

$$C_{X0} = f_1(\text{MACH}) \quad .$$

- 2) Axial force trim coefficient -

$$\Delta C_X = f_1(\text{MACH}, \alpha') \quad .$$

- 3) Untrimmed normal force coefficient -

$$C_{N'}(\alpha') = f_1(\text{MACH}, \alpha') \quad .$$

- 4) Untrimmed pitching moment coefficient -

$$C_{m'}(\alpha') = f_2(\text{MACH}, \alpha') \quad .$$

- 5) Incremental pitching moment coefficient due to aerodynamic roll angle (ϕ') -

$$\Delta C_{m'} = f_3(\text{MACH}, \alpha') \quad .$$

- 6) Pitch control moment coefficient due to fins -

$$\left(\frac{C_{m'}}{\delta q} \right)_{\phi'=0} = f_4(\text{MACH}, \alpha', \delta q)$$

$$\frac{C_{m'}}{\delta r} \phi'=0 = f_4(\text{MACH}, \alpha', \delta r) \quad .$$

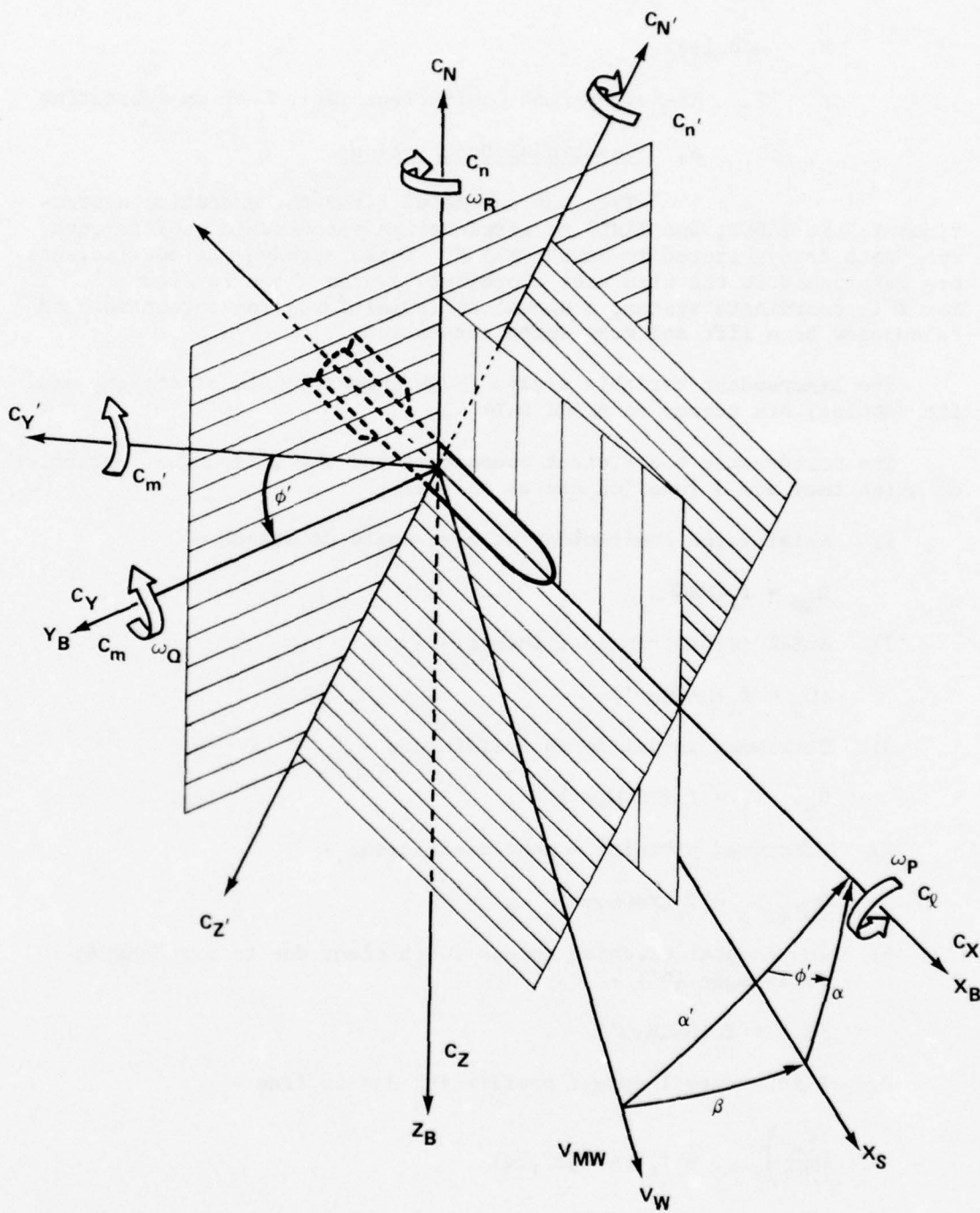


Figure 3. Wind axes coordinate system.

- 7) Incremental normal force coefficient due to aerodynamic roll angle (ϕ') -

$$\Delta C_{N'} = f_5(\text{MACH}, \alpha') \quad .$$

- 8) Normal force coefficient due to fin pitch position -

$$\left(\frac{C_{N'}}{\delta q} \right)_{\phi'=0} = f_6(\text{MACH}, \alpha', \delta q) \quad .$$

- 9) Normal force coefficient due to fin yaw position -

$$\left(\frac{C_{N'}}{\delta r} \right)_{\phi'=0} = f_6(\text{MACH}, \alpha', \delta r) \quad .$$

- 10) Incremental side force coefficient due to aerodynamic roll angle (ϕ') -

$$\Delta C_{Y'}(\phi') = f_7(\text{MACH}, \alpha') \quad .$$

- 11) Incremental yawing moment due to aerodynamic roll angle (ϕ') -

$$\Delta C_n = f_8(\text{MACH}, \alpha') \quad .$$

- 12) Incremental rolling moment due to aerodynamic roll angle -

$$\Delta C_{\ell'} = f_9(\text{MACH}, \alpha')$$

Lugs

$$\Delta C_{\ell'} = f_{10}(\text{MACH}, \alpha') \quad .$$

- 13) Rolling moment coefficient due to fin roll control -

$$\left(\frac{C_{\ell'}}{\delta p} \right)_{\phi'=0} = f_{11}(\text{MACH}, \alpha, \delta p)$$

- 14) Pitch, yaw, and roll damping coefficients -

$$C_{mq} = f_{12}(\text{MACH}, \alpha)$$

$$C_{nr} = f_{12}(\text{MACH}, \alpha)$$

$$C_{\ell p} = f_{13}(\text{MACH}, \alpha) \quad .$$

The independent variables and the dependent variables previously listed are stored in BLOCK DATA A and B and each dependent independent variable array is assigned to a COMMON BLOCK in their respective BLOCK DATA routines. When more than one independent variable is involved, the arrays containing the independent variables are located in a single COMMON BLOCK. For example, $C_m(\alpha')$ is a function of two independent variables, MACH and α' . COMMON BLOCK assignments are made according to the following data listing:

<u>Variable Name</u>	<u>Array Name</u>	<u>COMMON BLOCK</u>	<u>COMMON BLOCK Order</u>
$C_m(\alpha')$	CM	CMFUN	/CMFUN/CM (24)
α'	ALP1	CZARG	
MACH	AM1	CZARG	/CZARG/ALP1(6), AM1(4) .

The order in which the array name appears in the COMMON BLOCK is based upon which independent variable is held constant while the other is varied through its numerical range. The array name appearing first in a COMMON BLOCK is varied through its range while the second is held constant.

The instantaneous value of a coefficient is obtained from the data arrays by use of the executive subroutines (look-up subroutines) TABLE, TABL2, and TABL3. The look-up subroutines used depends upon the number of independent variables, e.g.:

- 1) One independent variable - use TABLE.
- 2) Two independent variables - use TABL2.
- 3) Three independent variables - use TABL3.

The instantaneous value of the independent variable is sent into the appropriate look-up subroutine, along with the COMMON BLOCK's containing the dependent and independent variable arrays. A linear interpolation is performed between appropriate points and the instantaneous value of the dependent variable is returned.

The force and moment coefficients of the control surfaces (fins) are given as a function of the ratio of the control surface coefficient to the average value of the combined angular displacement of the four control surfaces. The average value of the combined fin settings are computed in this module based upon the individual fin settings computed in the actuator module, C4.

b. Equations

(1) Fin Deflections. The average value of the combined fin settings based on individual fin settings are computed following the sign convention and fin setting configurations given in Figure 4. This figure illustrates the combined settings that produce pure attitudes of pitch, yaw, and roll.

The sign convention is based on the fin angular rotations that produce pure pitch. Thus, fin positive rotations (looking down the fin hinge toward the fin based) are:

- a) Fin No. 1 - positive counterclockwise (ΔF_1).
- b) Fin No. 2 - positive counterclockwise (ΔF_2).
- c) Fin No. 3 - positive clockwise (ΔF_3).
- d) Fin No. 4 - positive clockwise (ΔF_4).

Thus, the average value of the combined set is:

$$\delta p = \frac{(-\Delta F_1 - \Delta F_2 + \Delta F_3 + \Delta F_4)}{4} \text{ (roll)}$$

$$\delta q = \frac{(\Delta F_1 + \Delta F_2 + \Delta F_3 + \Delta F_4)}{4} \text{ (pitch)}$$

$$\delta r = \frac{(-\Delta F_1 + \Delta F_2 - \Delta F_3 + \Delta F_4)}{4} \text{ (yaw)}$$

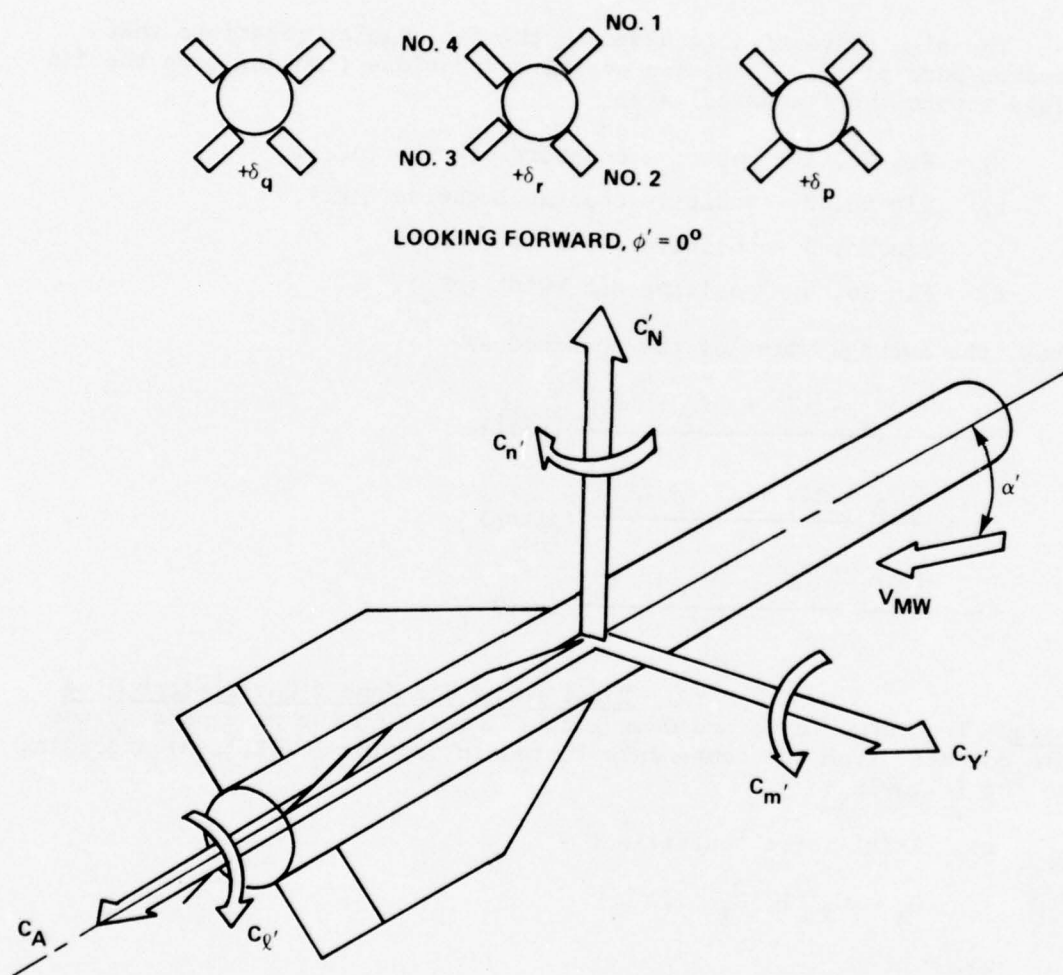
(2) Total Force and Moment Coefficient Wind Axes. The total force and moment coefficients in the wind axes system are computed from the components listed in Section III.B.1.(a) according to the following:

- a) Axial force coefficient -

$$C_A = C_{X0} + \Delta C_X$$

- b) Normal force coefficient -

$$C_{N'} = C_{N'}(\alpha') + \Delta C_{N'} \sin^2 2\phi' + \left(\frac{C_{N'}}{\delta q} \right)_{\phi'=0} (\delta q) \cos \phi' - \left(\frac{C_{N'}}{\delta r} \right)_{\phi'=0} (\delta r) \sin \phi'$$



NOTES:

1. C_N IS ALWAYS IN THE PLANE OF α'
2. TAIL DEFLECTIONS SHOWN ARE TRAILING EDGE DISPLACEMENTS.
3. TAIL HINGE MOMENTS HAVE THE SAME DIRECTION AS DEFLECTIONS δ_q .

Figure 4. Aero sign conventions - wind axes.

c) Pitching moment coefficient -

$$C_{m'} = C_{m'}(\alpha') + \Delta C_{m'} \sin^2 2\phi' + \left(\frac{C_{m'}}{\delta q} \right)_{\phi'=0} (\delta q) \cos \phi' - \left(\frac{C_{m'}}{\delta r} \right)_{\phi'=0} (\delta r) \sin \phi' .$$

d) Yawing moment coefficient -

$$C_{n'} = \Delta C_{n'} \sin 4\phi' + \left(\frac{C_{n'}}{\delta r} \right)_{\phi'=0} (\delta r) \cos \phi' + \left(\frac{C_{n'}}{\delta q} \right)_{\phi'=0} (\delta q) \sin \phi' .$$

e) Side force coefficient -

$$C_{Y'} = \Delta C_{Y'} \sin 4\phi' + \left(\frac{C_{Y'}}{\delta r} \right)_{\phi'=0} (\delta r) \cos \phi' + \left(\frac{C_{Y'}}{\delta q} \right)_{\phi'=0} (\delta q) \sin \phi' .$$

f) Rolling moment coefficient -

$$C_{\ell'} = \Delta C_{\ell'} \sin \phi' + \Delta C_{\ell'} \sin 4\phi' + \left(\frac{C_{\ell'}}{\delta p} \right)_{\phi'=0} (\delta p) .$$

(3) Total Force and Moment Aerodynamic

Coefficients - Body Axes. The aerodynamic forces and moments are computed in module A2 (forces and moments module) using the coefficients computed in this module. These forces and moments are computed in the missile body axes system; therefore, the coefficients previously computed must be transformed into the body system. The transformation is made based on the geometry given in Figure 3. Thus, the force and moment coefficients are:

a) Force coefficients -

$$\begin{aligned} C_X &= C_A^* \\ C_Y &= C_{Y'} \cos \phi' - C_{N'} \sin \phi' \\ C_Z &= -C_{Y'} \sin \phi' - C_{N'} \cos \phi' . \end{aligned}$$

*Axial force coefficient C_A is actually opposite in sign of C_X . This sign difference is accounted for in subroutine A2 when the forces are computed.

b) Moment coefficients -

$$C_{\ell} = C_{\ell'}$$

$$C_m = C_{n'} \sin \phi' + C_{m'} \cos \phi'$$

$$C_n = C_{n'} \cos \phi' - C_{m'} \sin \phi' .$$

c. Initialization Subroutine

Entry point AII in module C4I initializes the individual fin settings at time = 0 from data input on type 3 input cards (Section IV.A). Initial values of the fin settings are computed from the combined fin settings that produce pitch (δq), yaw (δr), and or roll (δp). The individual fin settings computed are:

$$\Delta F_1 = -\delta p + \delta q - \delta r .$$

$$\Delta F_2 = -\delta p + \delta q + \delta r .$$

$$\Delta F_3 = \delta p + \delta q - \delta r .$$

$$\Delta F_4 = \delta p + \delta q + \delta r .$$

The initialization equations for the individual fin settings are derived from the combined fin setting parameters under the constraint that

$$\Delta F_1 - \Delta F_2 - \Delta F_3 + \Delta F_4 = 0 .$$

d. Assumptions and Limitations

1) The combined fin settings that produce pure attitudes of pitch, yaw, and roll are given in Figure 4. The sign convention is based on the fin angular rotations that produce pure pitch.

a) A positive fin setting for pitch (δq) gives a negative pitching moment.

b) A positive fin setting for yaw (δr) gives a negative yawing moment.

c) A positive fin setting for roll (δp) gives a negative rolling moment.

2) Due to vehicle fin symmetry, the fin pitch and yaw moment coefficients are equal and the fin normal and side force coefficients are equal.

$$a) \quad \frac{C_{m'}}{\delta r} = \frac{C_{n'}}{\delta q} .$$

$$b) \quad \frac{C_{n'}}{\delta q} = \frac{C_{m'}}{\delta q} \quad .$$

$$c) \quad \frac{C_{n'}}{\delta r} = \frac{C_{m'}}{\delta q} \quad .$$

$$d) \quad \frac{C_{Y'}}{\delta r} = \frac{C_{Y'}}{\delta q} \quad .$$

$$e) \quad \frac{C_{Y'}}{\delta q} = \frac{C_{N'}}{\delta q} \quad .$$

$$f) \quad \frac{C_{N'}}{\delta r} = \frac{C_{N'}}{\delta q} \quad .$$

$$g) \quad C_{mr} = C_{mq} \quad .$$

3) In subroutine A1, the symbol for normal force coefficient $C_{N'}$, was changed to $C_{Z'}$. According to Figure 3, the force coefficient $C_{Z'}$, has opposite sign of $C_{N'}$. However, this sign change was not observed in programming the equation. Thus, the equation for normal force coefficient uses the symbol $C_{Z'}$, but has the sign convention of $C_{N'}$.

4) Limitations imposed upon the angle of attack for the purpose of interpolating in the aero coefficient tables (Tables 1 through 4) are as follows:

$$a) \quad \alpha' \leq 20^\circ \quad .$$

$$b) \quad \alpha \leq 20^\circ \quad .$$

$$c) \quad \beta \leq 20^\circ \quad .$$

e. Input/Output and Cross Reference of C-Array

The aero coefficient names are changed in A1 from that assigned in BLOCK DATA A and B. Table 2 is a cross reference of array names that are assigned in BLOCK DATA and the new names that are used in A1. Table 3 is a cross reference of symbols used in the text and their respective Fortran symbols.

2. A2 - Forces and Moments

a. Function Description

This module computes aerodynamic forces and moments acting on the vehicle, computes forces and moments acting on

TABLE 1. INPUT FROM OTHER MODULES - MODULE A1

Fortran Symbol	Symbol Used in Text	C Index	Definition
VMACH	MACH	204	Instantaneous value of Mach number
BALPHA	α	367	Instantaneous value of the vertical angle of attack, measured from the projection of the missile velocity with respect to the wind into the $X_B - Z_B$ plane and the X_B axis (deg)
BALPHY	β	368	Instantaneous value of the horizontal angle of attack, measured from the projection of the missile velocity relative to the wind into the $X_B - Z_B$ plane and the velocity relative to the wind (deg)
BALPHP	α'	369	Instantaneous value of the total angle of attack between vehicle X_B axis and the relative wind velocity (deg)
BPHIP	ϕ'	370	Instantaneous value of the aerodynamic roll angle between the plane containing the $Z_B - X_B$ axes and the plane containing the X_B velocity vector relative to the wind (deg)
BSURF1	ΔF_1	1103	Angular fin setting of fin No. 1, measured positive, counterclockwise (deg)
BSURF2	ΔF_2	1107	Angular fin setting of fin No. 2, measured positive, counterclockwise (deg)
BSURF3	ΔF_3	1111	Angular fin setting of fin No. 3, measured positive, clockwise (deg)
BSURF4	ΔF_4	1115	Angular fin setting of fin No. 4, measured positive, clockwise (deg)

TABLE 2. AERO COEFFICIENT COMMON BLOCK CROSS REFERENCE

	COMMON BLOCK	BLOCK DATA Arrays	A1 Arrays
A	NOS	NCX(6), NCZ(4), NCXO(2), NCZD(6)	NCX(6), NCN(4), NCO(2), NCD(6)
	CXARG	ALP(6), AM(3)	CXA(9)
	CZARG	ALP1(6), AM1(4)	CZA(10)
	CXOARG	AMZ(8)	CXB(8)
	CLDARG	ALP3(6), DEF(4), AM3(4)	CLA(14)
	CXFUN	CX(18)	CXF(18)
	CZFUN	CN(24)	CZF(24)
	DCZFUN	DCN(24)	DCF(24)
	CMFUN	CM(24)	CMF(24)
	DCMFUN	DCM(24)	DMF(24)
B	CXOFUN	CXO(8)	COF(8)
	CN2FUN	CN2(24)	C2F(24)
	CY2FUN	CY2(24)	CYF(24)
	CL2FUN	CL2(24)	CLF(24)
	CL3FUN	CL3(24)	C3F(24)
	CZDFUN	CN1(24), CN5(24), CN3(24), CN4(24)	CDF(92)
	CMDFUN	CM1(24), CM2(24), CM3(24), CM4(24)	MDF(92)
	CLDFUN	CL1(24), CL5(24), CL6(24), CL4(24)	DLF(92)
	CMQFUN	CMQ(24)	CQF(24)
	CLPFUN	CLP(24)	CPF(24)

TABLE 3. AERO COEFFICIENT MATHEMATICAL SYMBOL AND FORTRAN SYMBOL CROSS REFERENCE

Fortran Symbol	Symbol Used in Text	COMMON BLOCK Starting Point
CXO	C_{X0}	COF(1)
CX	ΔC_X	CXFUN(1)
CN	$C_{N'}(\alpha')$	CZFUN(1)
DCN	$\Delta C_{N'}$	DCZFUN(1)
CM	$C_{m'}(\alpha')$	CMFUN(1)
DCM	$\Delta C_{m'}$	DCMFUN(1)

TABLE 3. (Concluded)

Fortran Symbol	Symbol Used in Text	COMMON BLOCK Starting Point
CN2	$\Delta C_n'$	CN2FUN(1)
CY2	$\Delta C_Y'$	CY2FUN(1)
CL2	$\Delta C_{\ell}'$	CL2FUN(1)
CL3	$\Delta C_{\ell}'$ Lugs	CL3FUN(1)
CN1	$\left(\frac{C_N'}{\delta q}\right)_{\Phi'=0}$	CZDFUN(1)
CN5		CZDFUN(25)
CN3		CZDFUN(49)
CN4		CZDFUN(73)
CL1	$\left(\frac{C_{\ell}'}{\delta p}\right)_{\Phi'=0}$	CLDFUN(1)
CL5		CLDFUN(25)
CL6		CLDFUN(49)
CL4		CLDFUN(73)
CM1	$\left(\frac{C_m'}{\delta q}\right)_{\Phi'=0}$	CMDFUN(1)
CM2		CMDFUN(25)
CM3		CMDFUN(49)
CM4		CMDFUN(73)
CMQ	C_{mq}	CMQFUN(1)
CLP	$C_{\ell p}$	CLPFUN(1)

TABLE 4. OUTPUT - MODULE A1

Fortran Symbol	Symbol Used in Text	C Index	Definition
CX	C_X	1203	Total axial force coefficient value in body axis system
CY	C_Y	1204	Total side force coefficient value in body axis system
CZ	C_Z	1205	Total normal force coefficient value in body axis system
CLP	C_{lp}	1206	Roll moment damping coefficient
CMQ	C_{mq}	1207	Pitch moment damping coefficient
CNR	C_{nr}	1208	Yaw moment damping coefficient
CL	C_l	1209	Total rolling moment coefficient value in body axis system
CM	C_m	1210	Total pitching moment coefficient value in body axis system
CN	C_n	1211	Total yawing moment coefficient value in body axis system
BDL	δp	1231	Average value of the combined fin settings for roll control (deg)
BMD	δq	1232	Average value of the combined fin settings for pitch control (deg)
BDN	δr	1233	Average value of the combined fin settings for yaw control (deg)

the missile lugs due to launch rail motion and missile motion, and sums up all forces and moments acting on the vehicle computed in this module and those from other sources (such as thrust which is computed in A3). The resulting forces and moments output from this module are the total external forces and moments.

The aerodynamic forces and moments consist of those forces and moments acting on the vehicle and the moments on the movable control surface hinge points.

The aerodynamic forces and moments acting on the vehicle are computed using the aerodynamic coefficients determined by table lookup in subroutine A1.

Lug forces and moments are computed for missile motion along the launch rail if the input flag OPTN4 is greater than zero. The lug forces and moments are computed for two flight phases; viz, both lugs on the rail and rear lug only on the rail. Printed output concerning the events along the rail are controlled by this module. The events are (1) front lug rail clearance and (2) rear lug rail clearance. When the front lug clears the rail, the output is:

FRONT LUG CLEARS RAIL, T = (time) .

REL VEL = (airspeed), PITCH MOMENT = (pitching moment due to rear lug) .

TIPOFF RATES - ROLL, PITCH, and YAW missile rates following rear lug drop-off.

The output pitching moment is the pitching moment computed at the first time point after front lug clearance. No interpolation is made to determine the exact time of front rail clearance.

When the rear lug clears the rail, the output is:

REAR LUG CLEARS RAIL, T = (time) .

REL VEL = (airspeed), RAIL FORCE = (the Z-component of the rail force) .

The output rail force is the force exerted on both the front and rear lug at the time point just prior to front lug rail clearance. No interpolation is made to determine the exact time of rear lug rail clearance.

b. Equations

(1) Moments and Forces due to Aerodynamics and Thrust. Conventional aerodynamic force and moment equations are used to compute the forces and moments in the missile body axis system. They are

a) Vehicle aero forces -

$$F_{AXB} = P_D S_A (-C_X)^*$$

$$F_{AYB} = P_D S_A (C_Y)$$

$$F_{AZB} = P_D S_A (C_Z) ,$$

where P_D is dynamic pressure, S_A is the vehicle reference area, and the C subscripts are the aerodynamic coefficients.

b) Vehicle aero moments -

$$M_{AXB} = \left(C_{\ell} + C_{\ell p} \left(\frac{S_L}{2V_{MW}} \right) \omega_P \right) P_D S_A S_L$$

$$M_{AYB} = \left(C_m + C_{mq} \left(\frac{S_L}{2V_{MW}} \right) \omega_Q \right) P_D S_A S_L$$

$$M_{AZB} = \left(C_n + C_{nr} \left(\frac{S_L}{2V_{MW}} \right) \omega_R \right) P_D S_A S_L ,$$

where S_L is the vehicle reference length; C_{ℓ} , C_m , and C_n are the aero moment coefficients; $C_{\ell p}$, C_{mq} , and C_{nr} are the damping moment coefficients; V_{MW} is the missile velocity relative to the wind; and the ω subscripts are the vehicle rotation rates about their respective axes.

Due to a CG shift from the vehicle reference axes, delta moments due to aerodynamic forces and thrust are computed. The assumption that the shift occurs only along the X-axis is made. Thus,

$$\Delta Y_{CG} = 0$$

* C_X is sent into this module with the sign convention of C_A .

Therefore, the sign change is made here to account for the sign convention used in this program, namely $C_X = -C_A$.

and

$$\Delta Z_{CG} = 0$$

Therefore, delta body moments due to the CG shift are:

$$\Delta M_X = 0$$

$$\Delta M_Y = (F_{AZB} + F_{TZ}) \Delta X_{CG}$$

$$\Delta M_Z = (F_{AYB} + F_{TY}) \Delta X_{CG}$$

where F_{TY} and F_{TZ} are the thrust misalignment forces along the Y and Z body axes (computed in A3), and ΔX_{CG} is the CG shift as shown in Figure 5.

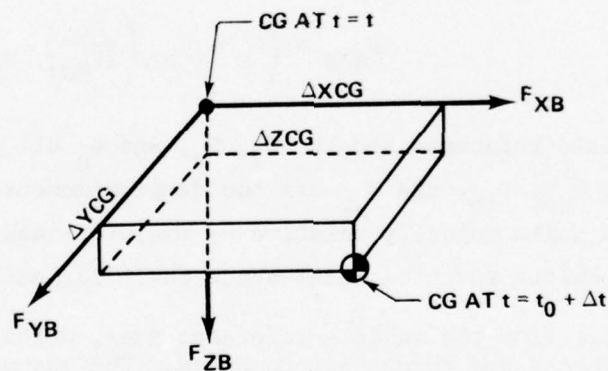


Figure 5. CG shift.

The sum total of the external body forces and moments computed in this module and input from the engine module (A3) are

$$\left. \begin{aligned} F_{XB} &= F_{AXB} + F_{TX} \\ F_{YB} &= F_{AYB} + F_{TY} \\ F_{ZB} &= F_{AZB} + F_{TZ} \end{aligned} \right\} \quad \text{(Components of total body forces)}$$

$$\begin{aligned}
 M_{XB} &= M_{AXB} + M_{XTH} \\
 M_{YB} &= M_{AYB} + \Delta M_Y + M_{YTH} \\
 M_{ZB} &= M_{AZB} + \Delta M_Z + M_{ZTH}
 \end{aligned}
 \left. \vphantom{\begin{aligned} M_{XB} \\ M_{YB} \\ M_{ZB} \end{aligned}} \right\} \text{(Components of total body forces)}$$

where F_{TX} is the thrust misalignment along the X-axis, and M_{XTH} , M_{YTH} , and M_{ZTH} are the body moments due to the initial thrust misalignment (at $t = 0$) computed in the engine module (A3). The missile lug forces and moments in the previously mentioned equations are added while the missile is still on the launch rail if the flag OPTN4 is set to non-zero.

(2) Moments and Forces Due to Lugs. The moments and forces acting on the missile while moving along the launch rail are shown in Figure 6. The variable symbols on the figure are defined as:

\bar{F}_{TH} - Thrust vector composed of (F_{TX}, F_{TY}, F_{TZ}) .

\bar{F}_{AERO} - Aerodynamic force vector composed of $(F_{AXB}, F_{AYB}, F_{AZB})$.

\bar{F}_{L1} - Force acting on front lug .

\bar{F}_{L2} - Force acting on rear lug .

\bar{W}_B - Weight vector.

\bar{M} - Total moment vector .

\bar{d}_1 - Front lug moment arm .

\bar{d}_2 - Rear lug moment arm .

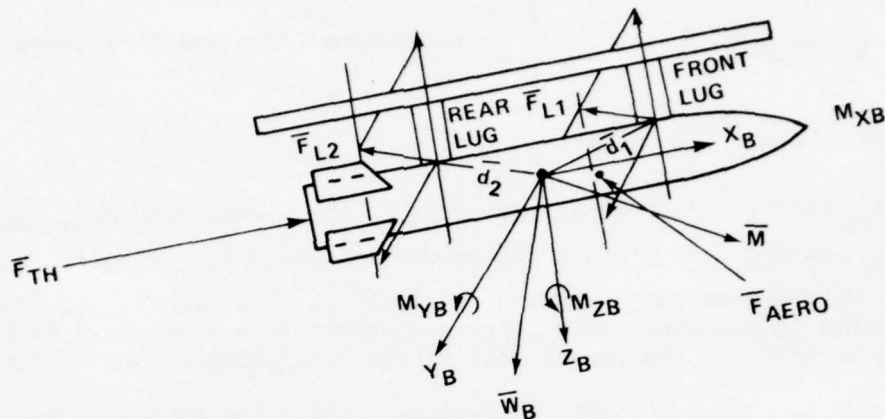


Figure 6. Missile free-body diagram.

The forces and moments are due to the missile motion and the rail motion (helicopter motion). The effect of rail motion is modeled as a moment [2] (computed in subroutine LTRAN) and is added to the total moments acting on the missile.

The forces and moments acting on the missile due to the lugs for the two flight phases are given as follows:

(a) Phase 1 - Missile Flight with Both Lugs on the Rail - Lug forces are:

$$F_{XLUG} = 0$$

$$F_{YLUG} = -(F_{YB} + mg C_{23})$$

$$F_{ZLUG} = mg (\ddot{z}_{RAIL} - C_{33}) - F_{ZB} \quad ,$$

where C_{23} and C_{33} are the (2,3) and (3,3) elements of the earth-to-body transformation matrix, M , defined in Section III.B.7, and \ddot{z}_{RAIL} is an unused rail acceleration term that is zeroed out in A2.

Lug moments are:

$$M_{XLUG} = - M_{XB} \quad .$$

$$M_{YLUG} = - M_{YB} \quad .$$

$$M_{ZLUG} = - M_{ZB} \quad .$$

(b) Phase 2 - Missile Flight After the
First Lug Clears Rail - Lug forces are:

$$F_{XLUG} = 0 \quad .$$

$$F_{YLUG} = \frac{m \left(d_{x2} \frac{M_{ZB}}{I_Z} \right) - (F_{YB} + mgC_{23})}{\left(1 + d_{x2}^2 \frac{m}{I_Z} \right)} \quad .$$

$$F_{ZLUG} = \frac{-m \left(\frac{d_{x2}}{I_Y} M_{YB} - Z_{RAIL} \right) - (F_{ZB} + mgC_{33})}{\left(1 + d_{x2}^2 \frac{m}{I_Y} \right)}$$

Lug moments are:

$$M_{XLUG} = - M_{XB}$$

$$M_{YLUG} = d_{x2} F_{ZLUG}$$

$$M_{ZLUG} = -d_{x2} F_{ZLUG} \quad .$$

(3) Total External Forces and Moments. The sum of all external forces and moments acting on the missile are:

a) Force components -

$$F_{XBA} = F_{AXB} + F_{TX} + F_{XLUG} \quad .$$

$$F_{YBA} = F_{AYB} + F_{TY} + F_{YLUG} \quad .$$

$$F_{ZBA} = F_{AZB} + F_{TZ} + F_{ZLUG} \quad .$$

b) Moment components -

$$M_{XBA} = M_{AXB} + M_{XTH} + M_{XLUG} + M_X \quad .$$

$$M_{YBA} = M_{AYB} + M_{YTH} + M_{YLUG} + \Delta M_Y + M_Y \quad .$$

$$M_{ZBA} = M_{AZB} + M_{ZTH} + M_{ZLUG} + \Delta M_Z + M_Z \quad .$$

c. Random Error Sources

(1) Launch Transient Model. The variables associated with the Monte Carlo launch transient models are given in Section III.B.2.e. An 8-card is used to select any one of these models (roll, pitch, or yaw) as a Monte Carlo variable. Roll is the only one of the three that requires specification of a probability distribution on the 8-card. The pitch and yaw models do require 8-cards; however, the probability distribution input fields are left blank because pitch and yaw are randomized indirectly, as explained in Reference 3.

A mean value of roll rate (WPTO) is input by 3-card. Mean values of pitch and yaw rate are not input, because the mean and distribution of these two variables are determined from solution of the forcing function, $F(t)$. However, the peak amplitude of pitch (AMP2) and yaw (AMP1) moments (due to helicopter vibration) must be input by 3-card. In addition, the flag, VIB, defined in Section III.B.2.e must be input equal to one.

(2) Pitch and Yaw Randomization Independent of Launch Transient Model. Pitch and yaw tipoff rates may be randomized from an input probability distribution by inputting the C-indices

of pitch and yaw rates on an 8-card. This capability was added as an option to directly randomize as opposed to indirectly randomizing pitch and yaw rates as previously mentioned. Use of this option will generate instantaneous changes in pitch and yaw rates at time of rear shoe rail exit. This option was added primarily to allow randomization of pitch and yaw rates for launch from a tower or ground vehicle in which there are no launcher vibrations. However, this option can be exercised simultaneously with the previously mentioned vibration model. Roll rate randomization previously described applies equally to helicopter or ground launchers.

d. Input/Output Variables and Cross Reference of C-Array

Tables 5 through 7 present the input/output variables and cross reference of the C-array of module A2.

TABLE 5. INPUT FROM DATA CARDS - MODULE A2

Fortran Symbol	Symbol Used in Text	C Index	Definition
RFAREA	S_A	1306	Aerodynamic cross section reference area (ft^2).
RFLGTH	S_L	1307	Aerodynamic reference length used to compute also moments (ft).
RLUG		1316	Spacing between the front and rear missile lugs (ft).
RAIL	RAIL	1317	Distance between rear of front lug and front of rail (ft).
AGRAV	g	1627	Acceleration due to gravity (ft/sec^2).
OPTN4		3504	Rail launcher dynamics and fire selector option switch: 0 - no rail dynamics - direct fire 1 - compute rail dynamics - direct fire 2 - compute rail dynamics - indirect fire.

TABLE 6. INPUT FROM OTHER MODULES - MODULE A2

Fortran Symbol	Symbol Used in Text	C Index	Definition
PDYNMC	P	203	Dynamic pressure (lb/ft^2)
VMACH	M	204	Mach number
VAIRSP	V_{MW}	207	Magnitude of velocity relative to the wind (ft/sec)
RANGO	$RANG_0$	380	Magnitude of separation distance between rail and missile (ft)
CX	C_X	1203	Aero axial force coefficient
CY	C_Y	1204	Aero side force coefficient
CZ	C_Z	1205	Aero normal force coefficient
CLP	C_{lp}	1206	Aero roll damping coefficient
CMQ	C_{mq}	1207	Aero pitch damping coefficient
CNR	C_{nr}	1208	Aero yaw damping coefficient
CL	C_l	1209	Aero rolling moment coefficient
CM	C_m	1210	Aero pitching moment coefficient
CN	C_n	1211	Aero yawing moment coefficient
FMX	M_X	1737	Components of rail moments caused by helicopter vibration (ft-lb)
FMY	M_Y	1741	
FMZ	M_Z	1745	
FMXTH	M_{XTH}	1320	Components of thrust misalignment moments about body axes (ft-lb)
FMYTH	M_{YTH}	1321	
FMZTH	M_{ZTH}	1322	
RLCG	ΔX_{CG}	1422	CG shift along X_B -axis (ft)

TABLE 6. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
FTHX	F_{TX}	1411	Thrust misalignment components along body axes (lb)
FTHY	F_{TY}	1412	
FTHZ	F_{TZ}	1413	
CFA23	C_{23}	1723	Element (2,3) of earth-to-body transformation matrix, M
WP	ω_P	1739	Roll rate about X_B -axis (deg/sec)
WQ	ω_Q	1743	Pitch rate about Y_B -axis (deg/sec)
WR	ω_R	1747	Yaw rate about Z_B -axis (deg/sec)
T	t	2000	Flight time (sec)
CFA33	C_{33}	1735	Element (3,3) of earth-to-body transformation matrix
WPTO	ω_{PTO}	1738	Tipoff roll rate (deg/sec)
AMP2	A_m	1742	Peak amplitude of pitch moment forcing function (ft/lb)
AMP1	A_m	1746	Peak amplitude of yaw moment forcing function (ft/lb)
VIB		626	Launch transient, vibration flag (pitch and yaw only): 0 - no vibration 1 - run with vibration

TABLE 7. OUTPUT - MODULE A2

Fortran Symbol	Symbol Used in Text	C Index	Definition
FXBA	F_{XB}	1300	X_B - component of all external forces acting on the missile (axial forces) (lb)
FYBA	F_{YB}	1301	Y_B - component of all external forces acting on the missile (side force) (lb)
FZBA	F_{ZB}	1302	Z_B - component of all external forces acting on the missile (normal forces) (lb)
FMXBA	M_{XB}	1303	X_B - component of all external moments acting on the missile (rolling moment) (ft-lb)
FMYBA	M_{YB}	1304	Y_B - component of all external moments acting on the missile (pitching moment) (ft-lb)
FMZBA	M_{ZB}	1305	Z_B - component of all external moments acting on the missile (yawing moment) (ft-lb)
FMH1	M_{H1}	1309	Hinge moment about aerodynamics control surface, fin No. 1 (ft-lb)
FMH2	M_{H2}	1310	Hinge moment about aerodynamics control surface, fin No. 2 (ft-lb)
FMH3	M_{H3}	1311	Hinge moment about aerodynamics control surface, fin No. 3 (ft-lb)
FMH4	M_{H4}	1312	Hinge moment about aerodynamics control surface, fin No. 4 (ft-lb)
FMXLUG	M_{XLUG}	1323	(1) X_B - component of moment counter-acted by the front and rear lugs when both lugs are on the rail (2) X_B - component of moment acting on the rear lug when the front lug has cleared the rail (rolling moment, ft-lb).

TABLE 7. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
FMYLUG	M_{XLUG}	1324	(1) Y_B - component of moment counter-acted by the front and rear lugs when both lugs are on the rail (2) Y_B - component of moment acting on the rear lug when the front lug has cleared the rail (pitching moment, ft-lb)
FMZLUG	M_{ZLUG}	1325	(1) Z_B - component of moment counter-acted by the front and rear lug when the lugs are on the rail (2) Z_B - component of moment acting on the rear lug when the front lug has cleared the rail (yawing moment, ft-lb)

e. Monte Carlo Input Variables and Cross Reference of C-Array

Table 8 presents the Monte Carlo input variables and cross reference of the C-array of module A2.

3. A3 - Engine Module

a. Function Description

The engine module calculates the total thrust (FTHRST) as a function of time, using a table look-up with linear interpolation between points. If the input engine misalignment switch, QNALGN, is greater than zero, the components of thrust (FTHX, FTHY, and FTHZ) along the body axes, X_B , Y_B , and Z_B , are calculated for use in determining translational accelerations. The corresponding moments (FMXTH, FMYTH, and FMZTH) are also calculated for use in determining rotational accelerations.

Regardless of the setting of the thrust misalignment switch, the engine module calculates instantaneous values for the time derivative of impulse (UIMPD), weight of burned propellant (UDWP), total vehicle mass (DMASS), change in CG offset due to burned propellant (RDELGC), moments of inertia (FMIX, FMIY, and FMIZ), and distance between the CG and rear lug (RLCG).

TABLE 8. MONTE CARLO INPUT - MODULE A2

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
WPTO	1738	A3I, A2		1738	Mean tipoff roll rate (deg/sec)
AMP2	1742	A3I, A2		1742	Peak amplitude of pitching moment forcing function (ft/lb)
AMP1	1746	A3I, A2		1746	Peak amplitude of yawing moment forcing function (ft/lb)
WQ	1743	A2		1743	Pitch rate (deg/sec)
WR	1747	A2		1747	Yaw rate (deg/sec)

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

A burnout switch (QBURN) is set to one when the first zero value is returned from the thrust table (indicating propellant burnout). After burnout, the engine module returns control to the calling routine without performing any calculations, and engine related variables retain their burnout values.

b. Equations

(1) Calculated when Thrust Misalignment Option is Selected (QNALGN > 0).

$$\left. \begin{aligned} FTHX &= (FTHRST) \cos (\alpha_T) \\ FTHY &= -(FTHRST) \sin (\alpha_T) \sin (\phi_T) \\ FTHZ &= (FTHRST) \sin (\alpha_T) \cos (\phi_T) \end{aligned} \right\} \begin{array}{l} \text{Thrust components along} \\ \text{body axes } (X_B, Y_B, Z_B) \end{array}$$

$$\left. \begin{aligned} FMXTH &= -(FTHY)(RFZCG) + (FTHZ)(RFYCG) \\ FMYTH &= (FTHX)(RFZCG) + (FTHZ)(RFXCG) \\ FMZTH &= -(FTHX)(RFYCG) - (FTHY)(RFXCG) \end{aligned} \right\} \begin{array}{l} \text{Moment components about} \\ X_B, Y_B, \text{ and } Z_B \text{ axes due} \\ \text{to thrust misalignment} \\ \text{and thrust displacement} \\ \text{from missile CG} \end{array}$$

where the terms on the right-hand side of the equations are defined in Figure 7.

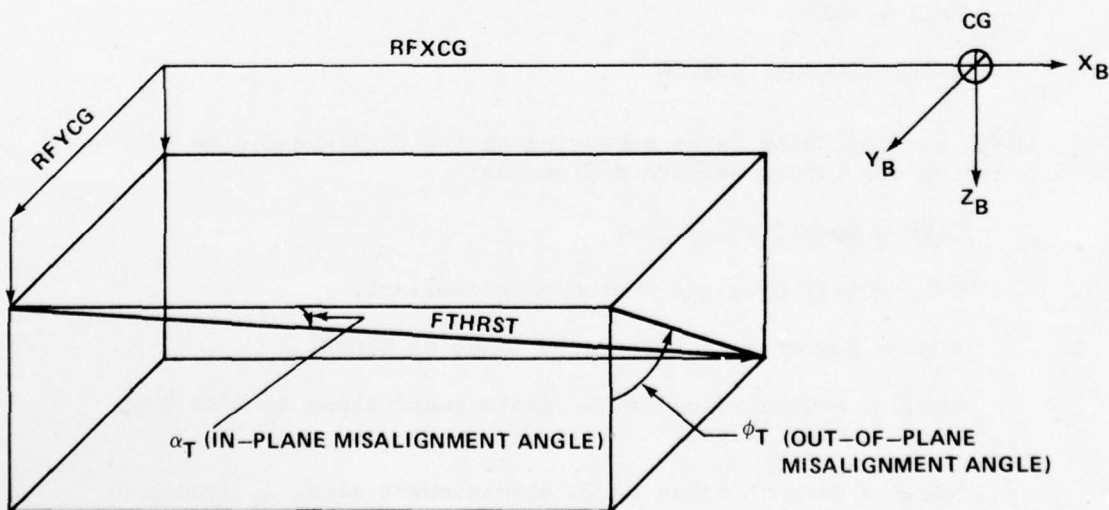


Figure 7. Thrust vector geometry.

Thus, the magnitude of the thrust vector is FTHRST, its direction is specified by the angles α_T and ϕ_T , and RFXCG, RFYCG, and RFZCG, are, respectively, the thrust application offsets from the missile CG along X_B , Y_B , and Z_B . Note the values of RFXCG, RFYCG, and RFZCG are to be input positive in the direction of the arrows shown in Figure 7 to obtain the correct sign for the moments.

(2) Calculated Regardless of the Thrust Misalignment Option.

$$UIMPD = FTHRST$$

$$UDWP = \frac{UIMP}{CISP}$$

$$DMASS = \frac{(DWT - UDWP)}{32.174}$$

$$RDEL CG = RDCGO - \frac{(RDCGO - RDCGF)(UDWP)}{DWP}$$

$$FMIX = \frac{FMIXO (DWT - UDWP)}{DWT}$$

$$FMIY = \frac{FMIYO (DWT - UDWP)}{DWT}$$

$$FMIZ = FMIY$$

$$RLCG = RL CGO + RDEL CG ,$$

where the following terms appearing on the right-hand side of the equation are inputs and are defined as:

CISP = Specific impulse.

DWT = Missile weight including propellant.

UIMP = Numerically integrated value of UIMPD.

RDCGO = Launch value of CG displacement along X_B from body axes origin.

RDCGF = Burnout value of CG displacement along X_B from body axes origin.

RLCGO = Distance between launch CG and rear lug.

$$\left. \begin{array}{l} \text{FMI XO} \\ \text{FMI YO} \\ \text{FMI ZO} \end{array} \right\} = \begin{array}{l} \text{Initial moments of inertia about } X_B, Y_B, \text{ and } Z_B \text{ axes,} \\ \text{respectively} \end{array} .$$

c. Assumptions

Although the instantaneous CG displacement from the body axes origin (RDEL CG) is calculated for use in the forces and moments module (A2), the CG shift is not used in the calculations for the instantaneous value of moments of inertia; the moments of inertia are modified only for the changing mass.

d. Initialization Subroutine

The engine module initialization subroutine (A3I) performs functions unrelated to the engine when the trajectory simulation initialization time is prior to engine burnout. Specifically, A3I initializes the angular body rates (ω_P , ω_Q , and ω_R) components of the angle of attack and roll angle (BALPHA, BALPHY, and BPHIP) to zero when simulation initiation is prior to burnout. The significance of these initialization actions is that angular rates and angles of attack will always be initially zero, regardless of the input values. This results from the fact that A3I is called after the input subroutine, OINPT1, and prior to the modules in the integration loop.

When simulation initiation is after engine burnout, A3I zeros all thrust components and sets moments of inertia, CG shifts, and vehicle mass to burnout values.

A3I also initializes several Monte Carlo variables. Thrust misalignment errors due to radial offset and nozzle misalignment are set.

A3I initializes the roll transient model used in conjunction with the optional optical contrast seeker described in Reference 3. Section III.B.3.g contains a list of all Monte Carlo variables initialized in A3I.

e. Random Error Sources - Thrust Misalignment/Offset

Thrust misalignment errors due to radial offset and nozzle misalignment, shown in Figure 8, are modeled in module A3. Monte Carlo values are generated in module A3I. Mean values of the thrust errors are set by input data cards.

When making runs that include thrust misalignment/offset errors, the program flag QNALGN must be set equal to one. If it is not, the logic to compute thrust component values from the Monte Carlo error values will be bypassed in module A3.

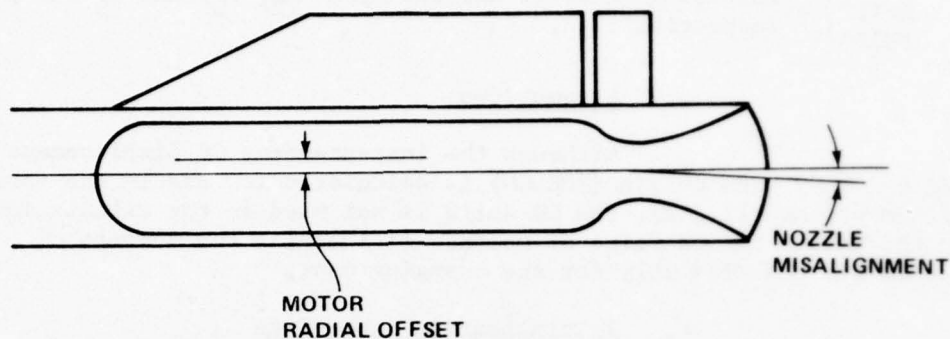


Figure 8. Thrust misalignment/offset error model.

The variables associated with the thrust misalignment/offset error model are given in Section III.B.3.g.

f. Input/Output Variables and Cross Reference of C-Array

Tables 9 and 10 present the input/output variables and cross reference of the C-array for module A3.

g. Monte Carlo Input Variables and Cross Reference of C-Array

Tables 11 and 12 present the Monte Carlo input variables and cross reference of C-array (launch transient and thrust misalignment variables, respectively).

4. C1 - Autopilot Module

a. Function Description

The autopilot, illustrated in the block diagram of Figure 9, provides pitch and yaw guidance signal shaping, short period rate damping, and navigation ratio mechanization required to implement the proportional navigation homing guidance technique. In addition, the autopilot maintains roll attitude by means of a roll control network. Pitch and yaw feedback is accomplished with rate gyros, while roll feedback is through a 2 DOF attitude gyro (modeled in G5). Gravity effects are continuously compensated for by the addition of a G_{BIAS} term. The autopilot has three modes of operation of the seeker. They are direct fire, direct fire-delayed guidance, and indirect fire.

TABLE 9. INPUT FROM DATA CARDS - MODULE A3

Fortran Symbol	Symbol Used in Text	C Index	Definition
RFXCG RFYCG RFZCG	RFXCG RFYCG RFZCG	1313 1314 1315	Thrust application point offset along X_B , Y_B , and Z_B body axes, from CG
BALPHT BPHIT	αT ϕT	1401 1402	
QNALGN	QNALGN	1403	
CISP	CISP	1414	Engine misalignment option switch (QNALGN > 0 selects engine misalignment)
DWT	DWT	1415	Specific impulse (sec)
DWP	DWP	1416	Missile weight (lb)
RDCGO	RDCGO	1417	Propellant weight (lb)
RDCGF	RDCGF	1418	Launch value of CG displacement along X-body axis (ft)
FMIXO FMIYO	FMIXO FMIYO	1419 1420	Burnout value of CG displacement along X-body axis (ft)
RLCGO	RLCGO	1421	Initial moments of inertia about X and Y body axes. (Due to assumed missile axial symmetry, FMIZF is taken to be equal to FMIYF) (slug-ft ²)
			Distance between launch CG and rear lug (ft).

TABLE 10. OUTPUTS - MODULE A3

Fortran Symbol	Symbol Used in Text	C Index	Definition
RDELCC	RDELCC	1308	Change in CG shift due to burned propellant (ft)
FMXTH FMYTH FMZTH	FMXTH FMYTH FMZTH	1320 1321 1322	Moment of force components about X, Y, and Z body axes due to engine misalignment and displacement of thrust point application from CG (ft-lb)

TABLE 10. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
FTHX FTHY FTHZ	FTHX FTHY FTHZ	1411 1412 1413	Translational thrust components along X, Y, and Z body axes (lb)
RLCG	RLCG	1422	
DMASS	DMASS	1628	
FMIX FMIY FMIZ	FMIX FMIY FMIZ	1748 1749 1750	Instantaneous values of moments of inertia about X, Y, and Z body axes (slug-ft ²)

TABLE 11. LAUNCH TRANSIENT MONTE CARLO VARIABLES

Program Variable Name of Error Source	C Index of Error Source	Program Module of Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
WPTO	1738	A3I, A2		1738	Mean tipoff roll rate (deg sec)
AMP2	1742	A3I, A2		1742	Peak amplitude of pitching moment forcing function (ft/lb)
AMP1	1746	A3I, A2		1746	Peak amplitude of yawing moment forcing function (ft/lb)

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

TABLE 12. THRUST MISALIGNMENT MONTE CARLO VARIABLES

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
RFXCG	1313	A3I	RFXCG	1313	Thrust X-offset (ft)
RFYCG	1314	A3I	RFYCG	1314	Thrust Y-offset (ft)
RFZCG	1315	A3I	RFZCG	1315	Thrust Z-offset (ft)
BALPHT	1401	A3I	BALPHT	1401	Thrust in-plane misalignment angle (deg)
BPHIT	1402	A3I	BPHIT	1402	Thrust out-of-plane misalignment angle (deg)

NOTE: See Figure 7 for pictorial illustration of these parameters.

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

(1) Direct Fire. In the direct fire mode, the seeker is locked on to the target ($OPTN4 < 1$, $TRKZY = 1$)* and the autopilot pitch and yaw channels receive guidance signals from the seeker. Normal terminal homing guidance is in effect. The pitch and yaw signals may be biased by input variables Q_{BIAS} and R_{BIAS} .

(2) Direct Fire-Delayed Guidance. In the direct fire-delayed guidance mode, the seeker is locked onto the target ($OPTN4 < 1$, $TRKZY = 1$, $TDY > 0$). However, the autopilot receives no guidance signal from the seeker until a specified flight time of TDY seconds has been reached. Preprogrammed guidance commands, Q_{BIAS} ,

*TRKZY is not a user input parameter. It is set in the seeker initialization module based upon the input value of OPNT4.

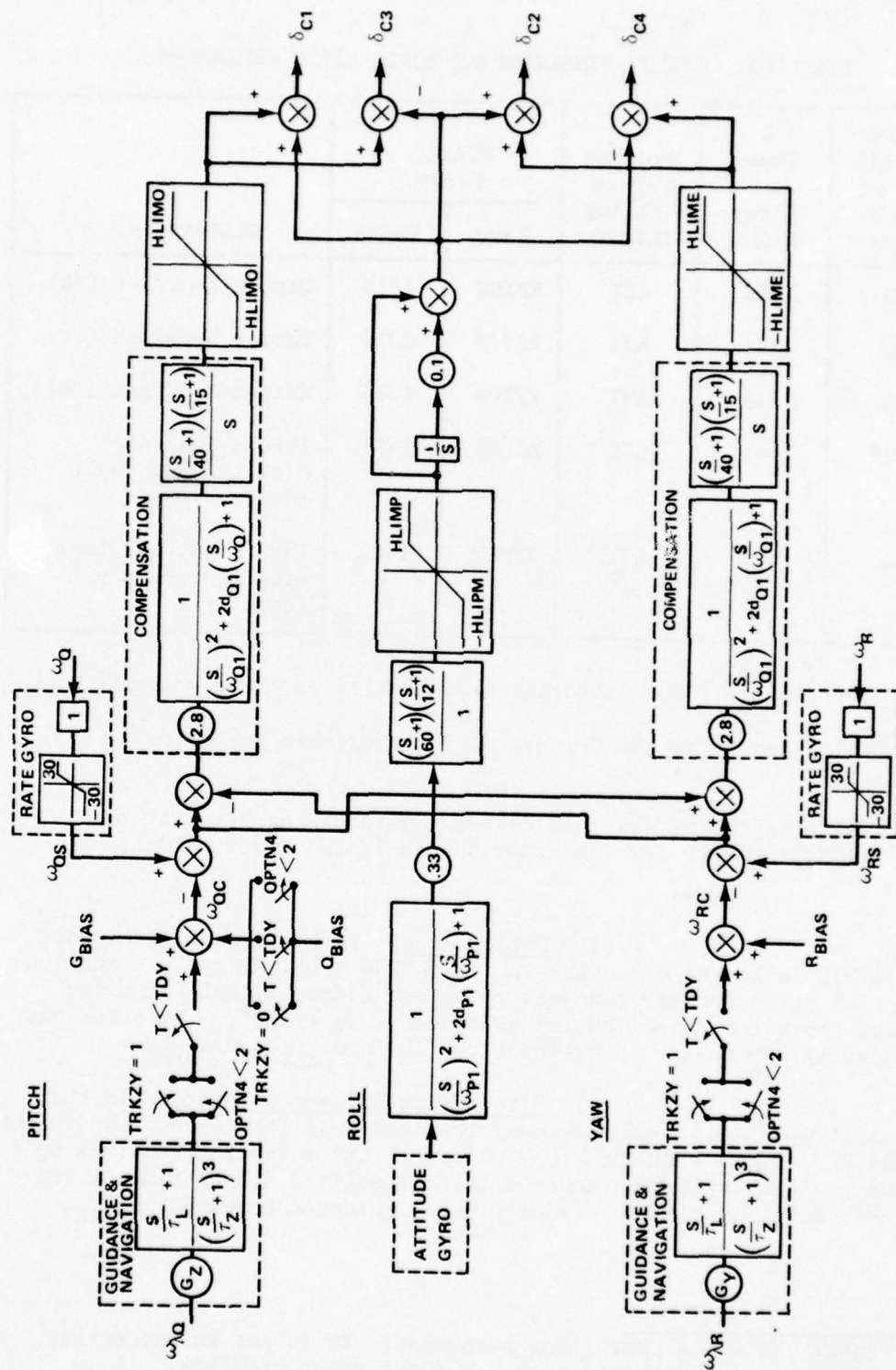


Figure 9. Autopilot block diagram.

R_{BIAS} , and the gravity compensation term G_{BIAS} are followed. At TDY seconds, the autopilot begins receiving guidance signals and normal terminal homing is in effect.

(3) Indirect Fire. If the seeker is in the indirect fire or caged mode ($OPTN4 = 2$, $TRKZY = 0$), then a preprogrammed flight profile is executed by using the Q_{BIAS} and R_{BIAS} terms to command pitch and yaw maneuvers. Following acquisition, the seeker is uncaged ($TRKZY$ is set to 1 in the seeker module), Q_{BIAS} is removed and normal terminal homing is in effect.

b. Equations

The first function of the autopilot is to perform appropriate guidance switching and signal shaping. If the seeker is in the direct fire mode ($OPTN4 < 1$, $TRKZY = 1$), the seeker output signals are smoothed and shaped by a lead-lag filter with one zero at τ_L and triple pole at τ_Y for yaw and τ_Z for pitch. Gravity effects are continuously compensated for by the addition of a G_{BIAS} term.

The commanded rate signals (ω_{QC} and ω_{RC}) are differenced with the sensed rate (ω_{QS} and ω_{RS}), the feedback signal. The resulting error signals are appropriately summed and differenced to produce the components in the missile's pitch and yaw axes. These signals are compensated by a lead-lag filter with real zeros at 40 and 15 rad/sec, and a complex pole pair with natural frequency ω_{Q1} and damping ratio d_{Q1} . Lastly, the signals are limited to keep the actuators from hitting their stops.

The roll control system attempts to maintain a zero roll attitude via a similar filter to that above with zeros at 60 and 12 rad/sec and poles at natural frequency ω_{p1} and damping d_{p1} . The pitch-roll and yaw-roll signals are summed and differenced in order to produce the appropriate reactions with the four actuators.

c. Initialization

The autopilot initialization subroutine, C4I, moves the indices of the C-array which contains derivatives utilized in the autopilot module into the array IPL(I). The array IPL(I) is used to point the numerical integration logic to the elements of the C-array which are to be numerically integrated.

C4I initializes the filters and integrators of the autopilot module. All initial conditions are set to zero.

C4I also contains the logic for randomizing autopilot error sources. These error sources are described in Section III.B.4.d.

d. Random Error Sources

(1) Pitch and Yaw Errors. The autopilot rate gyros can produce errors that perturb and bias the autopilot rate loops and degrade the sensitivity of the autopilot. Therefore, the primary errors sources of these rates gyros are included. Gyro errors (or more correctly, gyro error torques) can arise from a variety of different sources and are usually expressed as equivalent gyro drift rates.

Constant gyro drift rates result from uncompensated bias torques, L_e , and their magnitude is usually a measure of the gyro quality.

Acceleration sensitivity is primarily a function of the mass unbalance about the gyro output axis, i.e., the center of mass not coincident with the output axis. Linear accelerations, A , normal to the output axis produce gyro drift rates proportional to the accelerations.

The last gyro error source to be considered is a characteristic due to the inertia of the gyro float assembly. Angular accelerations about the output axis, $\dot{\omega}_{OA}$, cause gyro pickoff angle errors, which in turn torque the gyro through the electronic caging loop, resulting in a gyro drift rate. Thus, the total gyro error rate is

$$\omega_e = \frac{L_e}{H} + \frac{P}{H} A + \frac{J_{OA}}{H} \dot{\omega}_{OA},$$

where H is the angular momentum of the rotor, P is the pendulosity, and J_{OA} is the moment of inertia of the floated assembly about its output axis.

The autopilot has two stabilizing rate gyros mounted to sense inertial rates in the pitch and yaw axes. These rate gyros are mounted such that their output axes are aligned with the platform roll axis. Hence, the error rate for the pitch gyro is

$$\omega_{eQ} = K_{BQ} + K_{PQ} A + K_{OAQ} \dot{\omega}_P,$$

and for the yaw gyro

$$\omega_{eR} = K_{BR} + K_{PR} A + K_{OAR} \dot{\omega}_P.$$

The coefficients are user specified by their distribution functions. Since the gyro pendulosity, K_p , has an equal likelihood of occurring anywhere about the gyro output axis, its location is picked from a uniform distribution prior to each run.

(2) Roll Errors. Errors relating to the roll attitude gyro are uncaging errors at launch and drift. These error sources are described in Section III.B.6.d and modeled in subroutine G5.

e. Input/Output Variables and Cross Reference of C-Array

Tables 13, 14, and 15 present the input/output variables and cross reference of C-array for module C1.

f. Monte Carlo Input Variables

The variables associated with the Monte Carlo operation of the autopilot are given in Table 16. The mean values of these variables are input by 3-cards, and the probability distributions are input by 8-cards.

5. C4 - Actuator Module

a. Functional Description

The actuator system utilizes four independently controlled, pneumatically powered servos to position for four movable tail fins. Four commanded actuator fin position signals from the autopilot are summed with the negative feedback signals from the fin position potentiometers on the actuator mechanism. The resulting signals are used to pulse width modulate constant amplitude square wave signals. These signals control the on-off state of solenoid valves which are contained in the pneumatic system between the cold gas pressure source and the servos. An actuator position loop block diagram is depicted in Figure 10.

b. Equations

The actuator system shown in Figure 10 was reduced to the simple first order transfer function shown in Figure 11.

The 6 DOF simulation program actuator model is shown in Figure 12. This model is identical to that of Figure 11, with the exception of the rate and position limiters. As long as actuator operation is not saturated, the two models are identical.

TABLE 13. INPUT FROM DATA CARDS - MODULE C1

Fortran Symbol	Symbol Used in Text	C Index	Definition
TDY	TDY	866	Minimum time before trajectory pitch program will be switched to terminal homing guidance (sec)
GBIAS	G_{BIAS}	854	Gravity bias program (deg/sec)
HLIMO	H_{LIMO}	850	Pitch command limit (deg)
HLIME	H_{LIME}	851	Yaw command limit (deg)
QBIAS	Q_{BIAS}	852	Pitch rate-command bias (deg/sec)
RBIAS	R_{BIAS}	853	Yaw rate-command bias (deg/sec)
GZ	G_Z	867	Pitch navigation guidance filter gain
GY	G_Y	855	Yaw navigation guidance filter gain
WP1	W_{P1}	861	Complex pole of roll control filter (rad/sec)
DP1	d_{P1}	862	Damping coefficient of roll control filter
TAUZ	τ_Z	863	Pitch navigation filter pole (rad/sec)
TAUY	τ_Y	864	Yaw navigation filter pole (rad/sec)
HLIMP	H_{LIMP}	865	Roll command limit (deg)
WQ1	ω_{Q1}	871	Pitch and yaw compensation filter complex pole (rad/sec)
DQ1	d_{Q1}	872	Pitch and yaw compensation filter damping coefficient
TAUL	τ_L	877	Pitch and yaw navigation guidance filter zero (rad/sec)
OPTN4	OPTN4	3504	Fire control switch: 1 - direct fire 2 - indirect fire

TABLE 14. INPUTS FROM OTHER MODULES - MODULE C1

Fortran Symbol	Symbol Used in Text	C Index	Definition
EZ	ω_Z	403	Seeker output - pitch axis (deg/sec)
EY	ω_Y	407	Seeker output - yaw axis (deg/sec)
BPH1	ϕ_1	353	Missile roll attitude from roll gyro (deg).
WPD	$\ddot{\phi}_P$	1736	Missile roll acceleration (deg/sec ²)
ANGY	A	1677	Translational acceleration along Y _B -axis (g)
ANGZ	A	1678	Translational acceleration along Z _B -axis (g).
AKBQ	K _{BQ}	829	Pitch gimbal drift rate (deg/sec)
AKBR	K _{BR}	830	Yaw gimbal drift rate (deg/sec)
AKPQ	K _{PQ}	833	Pitch gimbal pendulosity coefficient (deg/sec/g)
AKPR	K _{PR}	834	Yaw gimbal drift rate (deg/sec/g)
AKOAQ	K _{OAQ}	837	Pitch gimbal output axis/roll coupling coefficient (sec)
AKOAR	K _{OAR}	838	Yaw gimbal output axis/roll coupling coefficient (sec)
TRKZY	TRKZY	464	Target acquisition switch: 0 - not acquired 1 - acquired
WQ	ω_Q	1743	Missile pitch rate (deg/sec)
WR	ω_R	1747	Missile yaw rate (deg/sec)
T	T	2000	Flight time (sec)

TABLE 15. OUTPUTS - MODULE C1

Fortran Symbol	Symbol Used in Text	C Index	Definition
BDELTC(1)	δ_{c1}	856	Commanded position, fin No. 1
BDELTC(2)	δ_{c2}	857	Commanded position, fin No. 2
BDELTC(3)	δ_{c3}	858	Commanded position, fin No. 3
BDELTC(4)	δ_{c4}	859	Commanded position, fin No. 4

TABLE 16. MONTE CARLO INPUT - MODULE C1

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
AKBQ	829	C1I		829	Pitch gimbal drift rate (deg/sec)
AKBR	830	C1I		830	Yaw gimbal drift rate (deg/sec)
AKPQ	833	C1I		833	Pitch gimbal pendulosity coefficient (deg/sec/g)
AKPR	834	C1I		834	Yaw gimbal drift rate (deg/sec/g)
AKO AQ	837	C1I		837	Pitch gimbal output axis/roll coupling coefficient (sec)
AKO AR	838	C1I		838	Yaw gimbal output axis/roll coupling coefficient (sec)

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

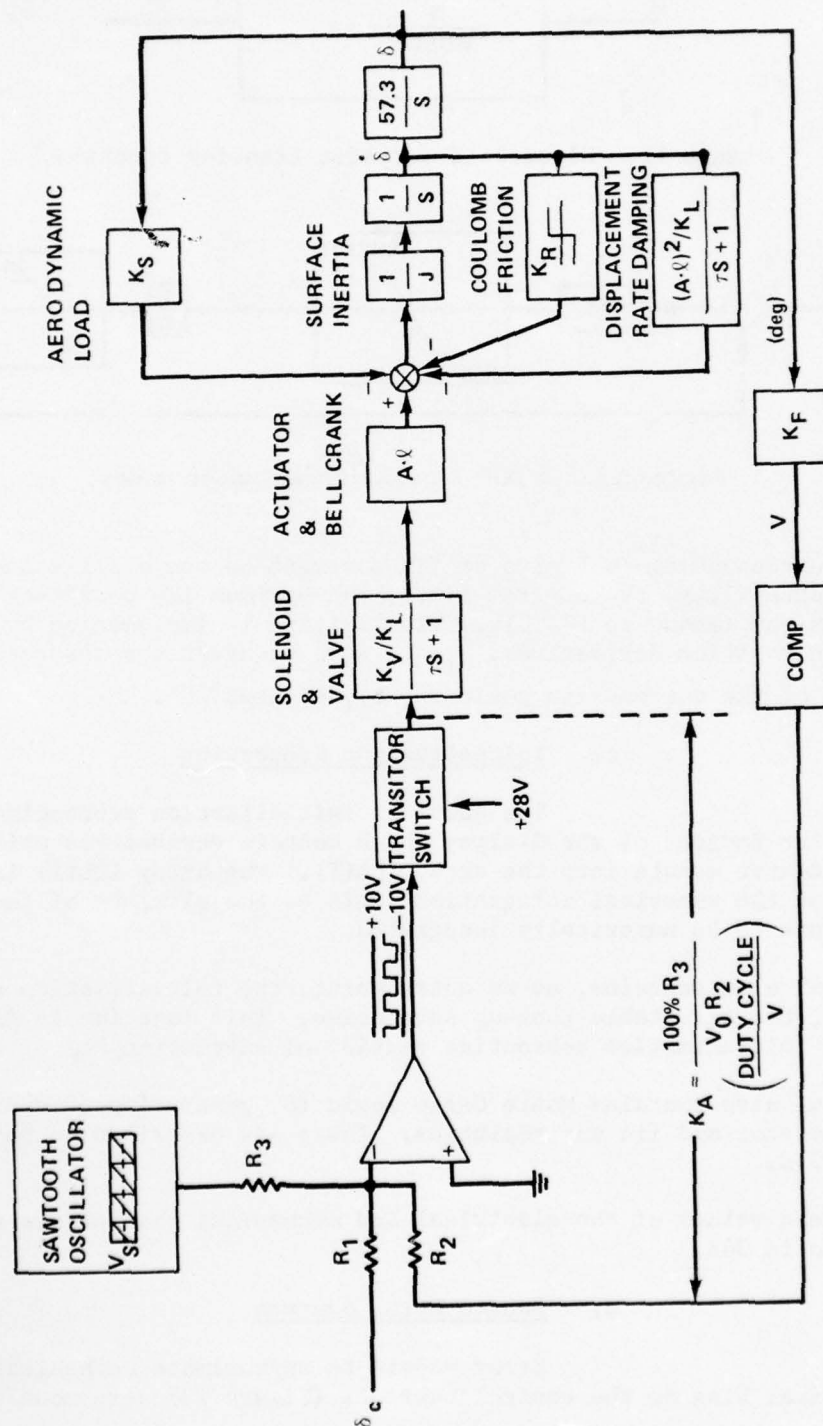


Figure 10. Actuator position loop.

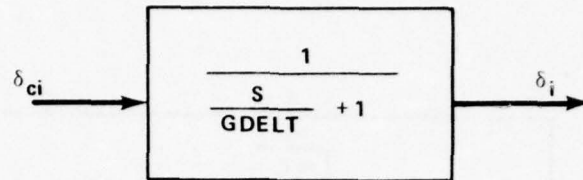


Figure 11. Linearized actuator transfer function.

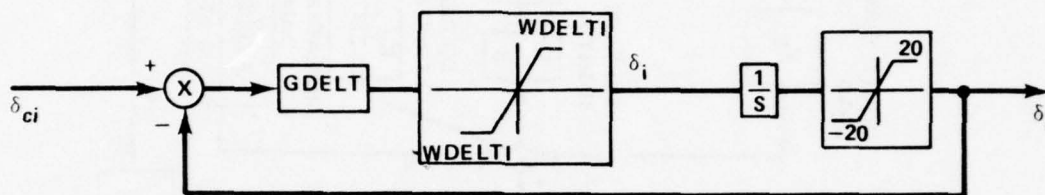


Figure 12. 6 DOF simulation actuator model.

Corresponding to limits of fin movement on the missile and torque motor capability, the program limits the maximum fin positions to $\pm 20^\circ$ and maximum torque to $\pm WDELTA$. Fin limiting is implemented by setting the fin position derivatives, δ_i , to zero whenever the absolute value of any of the current fin position, δ_i , exceeds 20° .

c. Initialization Subroutine

The actuator initialization subroutine, C4I, moves the indices of the C-array which contain derivatives utilized in the actuator module into the array IPL(I). The array IPL(I) is used to point the numerical integration logic to the elements of the C-array which are to be numerically integrated.

C4I also contains, as an entry point, the initialization routine for A1, the aero table look-up subroutine. This function is discussed in the initialization subroutine section of subroutine A1.

C4I also contains Monte Carlo logic for generation of random values for actuator and fin uncertainties. These are described in Section III.B.5.d.

Mean values of the electrical and mechanical bias errors are set to zero in C4I.

d. Random Error Sources

Error models to approximate mechanical and electrical bias on the control surfaces (Figure 13) were modeled

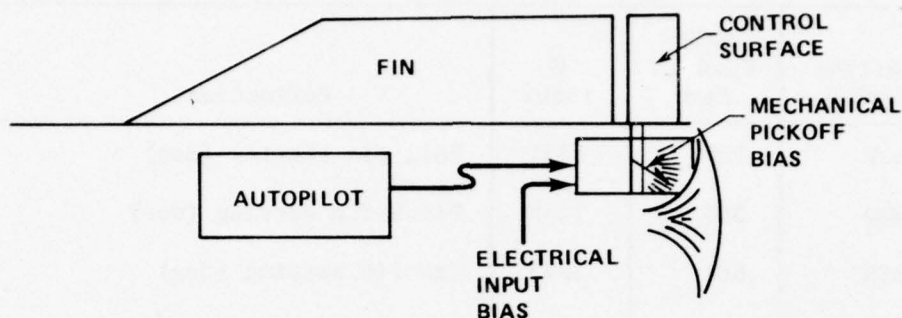


Figure 13. Control surface bias.

independently. Both the electrical and mechanical bias errors were assumed to be angular errors in the combined fin setting of roll, pitch, and/or yaw. Module C4I initializes the individual fin settings at time = 0 from input data cards for mean values of roll (BDP), pitch (BDQ), yaw (BDR), and Monte Carlo error values for the mechanical and electrical bias. The combined error values are:

$$\text{DELTB} = \text{FELECB} + \text{FMECHB} \text{ (roll setting error) } .$$

$$\text{DELTQB} = \text{FELECQB} + \text{FMECHQB} \text{ (pitch setting error) } .$$

$$\text{DELTRB} = \text{FELECRB} + \text{FMECHRB} \text{ (yaw setting error) } .$$

The individual fin settings, including the electrical and mechanical bias, are:

$$\text{BDELT1} = -(\text{BDP} + \text{DELTB}) + (\text{BDQ} + \text{DELTQB}) - (\text{BDR} + \text{DELTRB}) .$$

$$\text{BDELT2} = -(\text{BDP} + \text{DELTB}) + (\text{BDQ} + \text{DELTQB}) + (\text{BDR} + \text{DELTRB}) .$$

$$\text{BDELT3} = (\text{BDP} + \text{DELTB}) + (\text{BDQ} + \text{DELTQB}) - (\text{BDR} + \text{DELTRB}) .$$

$$\text{BDELT4} = (\text{BDP} + \text{DELTB}) + (\text{BDQ} + \text{DELTQB}) + (\text{BDR} + \text{DELTRB}) .$$

e. Input/Output Variables and Cross Reference of C-Array

Tables 17, 18, and 19 present the input/output variables and cross reference of C-array for module C4.

f. Monte Carlo Input Variables and Cross Reference of C-Array

Table 20 presents the Monte Carlo input variables and cross reference of C-array for module C4.

TABLE 17. INPUT FROM DATA CARDS - MODULE C4

Fortran Symbol	Symbol Used in Text	C Index	Definition
BDP	BDP	1231	Roll fin setting (deg)
BDQ	BDQ	1232	Pitch fin setting (deg)
BDR	BDR	1233	Yaw fin setting (deg)
WDELTL	W_{DELTL}	1143	Actuator rate limit (deg/sec)
GDELT	G_{DELT}	1144	Actuator pole (rad/sec)

TABLE 18. INPUT FROM OTHER MODULES - MODULE C4

Fortran Symbol	Symbol Used in Text	C Index	Definition
BDELTC(1)	δ_{c1}	856	Commanded fin position from autopilot, fin No. 1
BDELTC(2)	δ_{c2}	857	Commanded fin position from autopilot, fin No. 2
BDELTC(3)	δ_{c3}	858	Commanded fin position from autopilot, fin No. 3
BDELTC(4)	δ_{c4}	859	Commanded fin position from autopilot, fin No. 4
DELTB	DELTB	1254	Monte Carlo fin setting error in roll (deg)
DELTQB	DELTQB	1255	Monte Carlo fin setting error in pitch (deg)
DELTRB	DELTRB	1256	Monte Carlo fin setting error in yaw (deg)

TABLE 19. OUTPUTS - MODULE C4

Fortran Symbol	Symbol Used in Text	C Index	Definition
BDELT(1)	δ_1	1103	Actual fin position, fin No. 1
BDELT(2)	δ_2	1107	Actual fin position, fin No. 2
BDELT(3)	δ_3	1111	Actual fin position, fin No. 3
BDELT(4)	δ_4	1115	Actual fin position, fin No. 4

TABLE 20. MONTE CARLO INPUT - MODULE C4

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
DELTB	1254	C4I	FELECB	1101	Electrical bias in roll (deg)
DELTB	1254	C4I	FMECHB	1106	Mechanical bias in roll (deg)
DELTQB	1255	C4I	FELECBQ	1102	Electrical bias in pitch (deg)
DELTQB	1255	C4I	FMECHQB	1109	Mechanical bias in pitch (deg)
DELTRB	1256	C4I	FELECRB	1105	Electrical bias in yaw (deg)
DELTRB	1256	C4I	FMECHRB	1110	Mechanical bias in yaw (deg)

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

6. D1 - Translational Dynamics Module

a. Functional Description

The translation dynamics module calculates translational accelerations of the missile in both the earth and body coordinate systems, and moves the missile acceleration components to the velocity integrator locations in the C-array.

The missile velocity components obtained on the previous integration step are moved to the position integrator locations in the C-array. Missile g acceleration in body axes are obtained for information purposes. If the target motion option is selected on input (OPTARG > 0), target motion derivatives are also calculated based upon input values of linear acceleration and a turning term. The target acceleration and velocity components are moved to the target velocity and position locations in the C-array.

b. Equations

The following paragraphs give missile related and target motion equations.

(1) Missile Related Equations.

a) Total acceleration in body axes -

$$\begin{bmatrix} AXBA \\ AYBA \\ AZBA \end{bmatrix}_B = \frac{1}{DMASS} \begin{bmatrix} FXBA \\ FYBA \\ FZBA \end{bmatrix}_B$$

where FXBA, FYBA, and FZBA are calculated in the forces and moments module (A2) and represent the sum of the aerodynamic and thrust forces, and DMASS is the instantaneous total vehicle mass calculated in the engine module (A3).

b) Total acceleration in earth axes -

$$\begin{bmatrix} AXE \\ AYE \\ AZE \end{bmatrix}_E = M^T \begin{bmatrix} AXBA \\ AYBA \\ AZBA \end{bmatrix}_B$$

where M^T is the transpose of the earth-to-body transformation matrix, calculated in the rotational dynamics module (D2).

c) Earth axes velocity integrator values -

$$\begin{bmatrix} \text{VXED} \\ \text{VYED} \\ \text{VZED} \end{bmatrix} = \begin{bmatrix} \text{AXE} \\ \text{AYE} \\ \text{AZE} + \text{AGRAV} \end{bmatrix}$$

where AGRAV is the acceleration due to gravity. The "velocity integrator" locations in the C-array (equivalenced to VXED, VYED, and VZED in the translation dynamics module (DII) are the actual C locations which are used in the numerical integration routine AMRK.

d) Body axes velocity integrator values -

$$\begin{bmatrix} \text{VDXB} \\ \text{VDYB} \\ \text{VDZB} \end{bmatrix}_B = M \begin{bmatrix} \text{VXED} \\ \text{VYED} \\ \text{VZED} \end{bmatrix}_E .$$

e) g-acceleration in body axes -

$$\begin{bmatrix} \text{ANGX} \\ \text{ANGY} \\ \text{ANGZ} \end{bmatrix}_B = \frac{1}{g} \begin{bmatrix} \text{VDXB} \\ \text{VDYB} \\ \text{VDZB} \end{bmatrix}_B .$$

The body axes accelerations are calculated for information, and can be optionally printed.

f) Earth axes position integrator values -

$$\begin{bmatrix} \text{RXED} \\ \text{RYED} \\ \text{RZED} \end{bmatrix}_B = \begin{bmatrix} \text{VXE} \\ \text{VYE} \\ \text{VZE} \end{bmatrix}_B .$$

(2) Target Motion Equations. Several input parameters are available for specifying target motion during the simulation. One, ATHRST, represents simply the magnitude of the target acceleration vector. A second parameter, ATURNT, represents one variable in the calculation of the rate of change of the earth plane azimuth angle ($\dot{\psi}$) of the velocity vector, where the second variable in the calculation is the instantaneous magnitude of the velocity vector itself. The initial azimuth angle (ψ_0) can be input, as can an elevation angle (γ_0), where the sign convention of these angles is shown in Figure 14.

A summary of the kinds of target motion that can be achieved with the input target motion parameters is presented in Table 21.

TABLE 21. TARGET MOTION SUMMARY

ATHRST	ATURNT	VTARG	γ	ψ	Target Motion*
0	0	0	-	-	None
0	0	> 0	γ_0	ψ_0	Constant velocity of target away from origin in the direction specified by (γ_0, ψ_0) .
> 0	0	V_0	γ_0	ψ_0	Constant acceleration of target away from origin in the direction (γ_0, ψ_0) , with initial velocity V_0 .
0	> 0	$V_0 > 0$	γ_0	ψ_0	Constant magnitude of velocity, initially in the direction of (γ_0, ψ_0) , with direction of velocity vector changing at a constant rate determined by ATURNT and V_0 .
> 0	> 0	V_0	γ_0	ψ_0	Constantly accelerating target away from origin in initial direction of (γ_0, ψ_0) , but with increasing (at a decreasing rate) with time.

*Note all of the motions listed in Table 16 will automatically be initiated from the origin of the earth axes whenever $OPTN2 > 0$, because subroutine DII sets the target position coordinates to zero. Also, some combinations are not shown because they would not result in target motion due to the manner in which the equations are written. Thus, for example, the combination of $ATHRST = 0$, $ATURNT > 0$, $VTARG = 0$, (γ and ψ arbitrary) would result in no target motion.

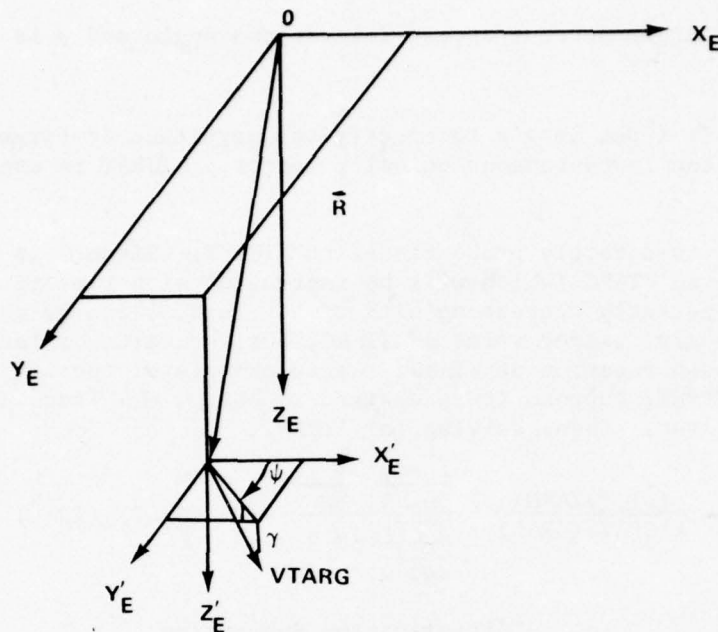


Figure 14. Target motion velocity vector*.

$$VTARGD = (ATHRST)(AGRAV),$$

where VTARG is the target velocity integrator position in the C-array, and ATHRST is the input value of target acceleration in g's.

$$\dot{\psi} = \frac{ATURN}{VTARGD} (AGRAV) (CRAD)$$

where $\dot{\psi}$ is the target velocity vector azimuth angle (Figure 14), ATURN is an input value (with units of g's) which partially determine the rate of change of the azimuth angle.

The components of the target velocity vector in the earth system are as follows:

$$VTXE = VTARG \cos(\gamma_0) \cos(\psi)$$

$$VTYE = VTARG \cos(\gamma_0) \sin(\psi)$$

$$VTZE = VTARG \sin(\gamma_0)$$

*NOTE: A system ($X_{E'}$, $Y_{E'}$, $Z_{E'}$), parallel to the earth axis system, has been defined at the terminal point of the radius vector to emphasize the fact that γ and ψ specify the instantaneous direction of the target velocity vector rather than the radius vector.

where γ_0 is target descent/ascent (elevation) angle and ψ is target azimuth.

ATHRST is input in g's to specify the magnitude of target acceleration along the instantaneous velocity vector. ATURNT is used in the equation for $\dot{\psi}$.

Thus, $\dot{\psi}$ is directly proportional to ATURNT. Since $\dot{\psi}$ is inversely proportional to VTARG (which will be increasing with time if ATHRST > 0) $\dot{\psi}$ will be constantly decreasing with time. Thus, $\dot{\psi}$ can be controlled on input for any desired value of VTARG, but the value of for all other times will be a function of VTARG. As an example of specifying an input value for ATURNT, suppose it is desired to have $\dot{\psi} = 1^\circ/\text{sec}$ when VTARG = 1 ft/sec. Then, solving for ATURNT,

$$\text{ATURNT} = \frac{(\dot{\psi}) (\text{VTARG})}{(\text{AGRAV}) (\text{CRAD})} = \frac{\frac{1 \text{ deg}}{\text{sec}} \frac{1 \text{ ft}}{\text{sec}}}{\frac{32 \text{ ft}}{\text{sec}^2} 57.3 \text{ deg}} \approx (5.47) (10^{-4}) \text{ g} .$$

c. Initialization Subroutine

The translational dynamics initialization subroutine (DLI) calculates initial missile position and velocity components according to one of seven combinations of input option switches OPTN2 and OPTN4. Table 22 depicts the input variables required for each option, where the variables are defined as:

RXE	}	Initial missile position and velocity coordinates in earth axes system.
RYE		
RZE		
VXE		
VYE		
VZE		
BPSIO	}	Euler angles orienting body axes with respect to the earth axes (see Figure C-1 in Appendix C).
BHTO		
BPHIO		
BHTG	}	Initial gimbal angles in pitch and yaw, respectively.
BPSIG		
RSLANT		Initial slant range from missile to target.

TABLE 22. INPUT DATA OPTIONS FOR INITIAL VALUES

	Unrestricted Inputs	Restricted Inputs					
		No Rail Dynamics		Rail Dynamics Included			
		Direct Fire		Direct Fire		Indirect Fire	
OPTN4	0	0	0	1	1	2	2
OPTN2	0	1	2	1	2	1	2
RXE	X	I	X	I	X	I	X
RYE	X	0	0	0	0	0	0
RZE	X	I	X	I	X	I	X
VXE	X	I	I	I	I	I	I
VYE	X	I	I	I	I	I	I
VZE	X	I	I	I	I	I	I
RTXE	X	0	0	0	0	0	0
RTYE	X	0	0	0	0	0	0
RTZE	X	0	0	0	0	0	0
BPSIO	X	I	I	X	X	X	X
BTHTO	X	I	I	X	X	X	X
BPHIO	X	0	0	0	0	0	0
BHTTG	X	X	X	I	I	X	X
BPSIG	X	X	X	I	I	X	X
RSLANT		X	I	X	I	X	I
BSLOV		X		X		X	
VWXE		X	X	X	X	X	X
VWYE		X	X	X	X	X	X
VWZE		X	X	X	X	X	X
(VMACH)* (VMWTE)		X	X	X	X	X	X

X - denotes variables that must be specified by input data.

I - denotes variables that are computed internally.

0 - denotes variables that are either set to zero initially or will be computed as zero.

*Input YMACH if OPTN6 = 0; input VMWTE if OPTN6 = 1.

BLOS	Angle between line-of-sight and earth plane. (Sign convention: BSLOV > 0 when line-of-sight is above the earth plane.)
VWYE } VWZE }	Wind velocity components in earth axes.
VMACH	Initial missile Mach number.

d. Random Error Sources

DII contains three Monte Carlo error sources. Only one of these error sources, missile launch attitude, is directly related to the function of DI, that is, translational dynamics computation. The other two, roll gyro attitude error and roll gyro drift rates appear here because the error values are required in the initialization of the transformation matrix $[A_0]$ and the initial position of the roll gyro (X_{BO1} , Y_{BO1} , Y_{BO}) that are used in subroutine G5.

(1) Missile Launch Attitude. Missile launch attitude, illustrated in Figure 15 is modeled in the initialization module DII. The attitude angles BTHTO, TPHIO, and BPSIO are the mean error sources for attitude randomization. BTHTO and BPSIO mean values are input quantities, while the mean value of BPHIO is set to zero in DII.

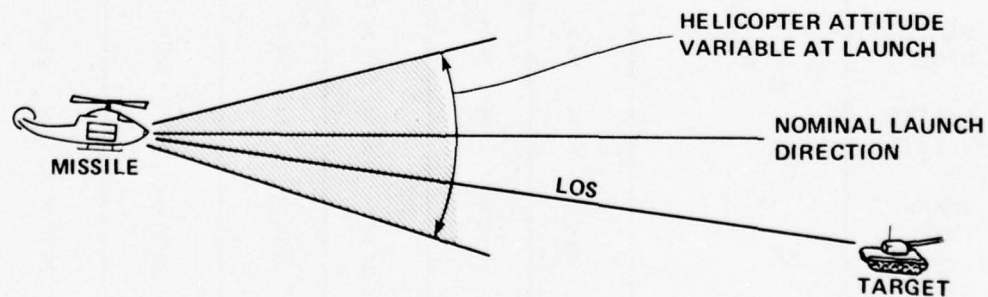


Figure 15. Missile launch attitude.

(2) Autopilot Gyros. Autopilot roll attitude gyro errors are made up of an inertial misalignment at uncaging and drift. The inertial misalignment due to uncertainties in helicopter attitude also cause missile launch attitude errors (Figure 16); therefore, it should be remembered that the probability distributions for these two error sources (launch attitude and gyro misalignment) should be the same.

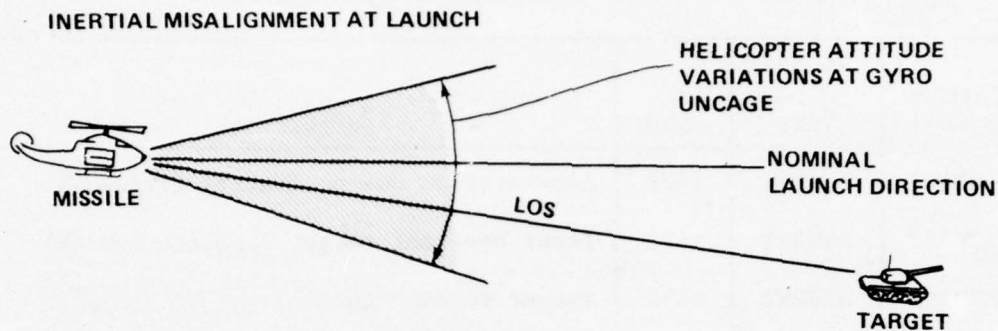


Figure 16. Autopilot gyro uncertainties.

The mean error sources for the autopilot gyro misalignment angles are the missile launch attitude angles BPHIO and BPSIO. The mean values of these launch attitude angles are set by input data card. The mean error sources for the gyro drift components are P_1 and R_1 . The mean values of these variables are set to zero in module DII.

Gyro drift has two components due to the construction of the autopilot gyro. The gyro is a 2 DOF gyro; thus, it rotates independently about two axes. The rotational axes are yaw (R_1) and roll (P_1). The dynamical equations for gyro drift rate are presented in Section III.B.11.c.

e. Input/Output Variables and Cross Reference of C-Array

Tables 23, 24, and 25 present the input/output variables and cross reference of C-array for module D1.

f. Monte Carlo Input Variables and Cross Reference of C-Array

The Monte Carlo input variables and cross reference of C-array of module D1 is presented in Table 26.

7. D2 - Rotational Dynamics Module

a. Functional Description

The rotational dynamics module calculates the numerical values for the derivatives of the vehicle rotational rates (ω_P , ω_Q , and ω_R), and the elements (C_{ij} , $i, j = 1, 2, 3$) of the earth-to-body axis transformation matrix, M .

TABLE 23. INPUT FROM DATA CARDS - MODULE D1

Fortran Symbol	Symbol Used in Text	C Index	Definition
AGRAV	AGRAV	1627	Acceleration due to gravity (ft/sec ²)
ATHRST	ATHRST	1629	Input constant target acceleration (g)
ATURNT	ATURNT	1630	Target turning term
BGAMT	γ	1631	
OPTARG	OPTARG	1639	Target motion option switch (OPTARG > 0 for target motion)
CRAD	CRAD	1751	Radians to degrees conversion
BPSIT	γ	1647	Target azimuth
RXE	RXE	1615	Components of missile position in earth fixed coordinate system (ft)
RYE	RYE	1619	
RZE	RZE	1620	
VXE	VXE	1603	Components of missile velocity in earth fixed coordinate system (ft/sec)
VYE	VYE	1607	
VZE	VZE	1611	
BPSIO	BPSIO	1754	Autopilot gyro yaw angle (deg)
BTHTO	BTHTO	1753	Autopilot gyro pitch angle (deg)
BPHIO	BPHIO	1752	Autopilot gyro roll angle (deg)
RSLANT	RSLANT	1667	Initial slant range from missile to target (ft)
BSLOV	BSLOV	1666	Angle between line-of-sight and earth plane (Sign convention: BSLOV > 0 when line-of- sight is above earth plane) (deg)
VWXE	VWXE	100	Wind velocity components in earth axes (ft/sec)
VWYE	VWYE	101	
VWZE	VWZE	102	

TABLE 24. INPUT FROM OTHER MODULES - MODULE D1

Fortran Symbol	Symbol Used in Text	C Index	Definition
FXBA	FXBA	1300	Components of total forces acting on missile in body coordinate system (lb)
FYBA	FYBA	1301	
FZBA	FZBA	1302	
CFA11	CFA11	1703	Elements of the earth-to-body transformation matrix, M
CFA12	CFA12	1707	
CFA13	CFA13	1711	
CFA21	CFA21	1715	
CFA22	CFA22	1719	
CFA23	CFA23	1723	
CFA31	CFA31	1727	
CFA32	CFA32	1731	
CFA33	CFA33	1735	

TABLE 25. OUTPUT - MODULE D1

Fortran Symbol	Symbol Used in Text	C Index	Definition
VXE	VXE	1603	Components of missile velocity in earth fixed coordinate system (ft/sec)
VYE	VYE	1607	
VZE	VZE	1611	
RXE Q	RXE	1615	Components of missile position in earth fixed coordinate system (ft)
RYE	RYE	1619	
RZE	RZE	1620	
AXBA	AXBA	1624	Components of total missile acceleration in the body axes (ft/sec ²)
AYBA	AYBA	1625	
AZBA	AZBA	1626	
VTXE	VTXE	1660	Components of target velocity in the earth system (ft/sec)
VTYE	VTYE	1661	
VTZE	VTZE	1662	
VDXB	VDXB	1663	Body axes acceleration (ft/sec ²)
VDYB	VDYB	1664	
VDZB	VDZB	1665	
ANGX	ANGX	1676	g-accelerations in body axes
ANGY	ANGY	1677	
ANGZ	ANGZ	1678	

TABLE 26. MONTE CARLO INPUTS - MODULE D1

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
BTHTO	1753	D1I	BTHTO	1753	Initial pitch angle (deg)
BPHIO	1752	D1I	BPHIER	360	Autopilot gyro roll error (deg)
BPSIO	1754	D1I	BPSIER	362	Autopilot gyro yaw error (deg)
P1	1764	D1I	P1	1764	Roll rate about gyro inner gimbal (deg/sec)
R1	1765	D1I	R1	1765	Yaw rate about gyro outer gimbal (deg/sec)

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

b. Equations

The rotational derivatives of the vehicle are calculated from values of the respective moments [calculated in the forces and moments module (A2)] and input values of the moments of inertia. The equations are:

$$\dot{\omega}_P = \frac{M_X}{I_{XX}} \text{ (roll)}$$

$$\dot{\omega}_Q = \frac{M_Y + (I_Z - I_X) (\omega_P) (\omega_R)}{I_{YY}} \text{ (pitch)}$$

$$\dot{\omega}_R = \frac{M_Z + (I_X - I_Y) (\omega_P) (\omega_Q)}{I_{ZZ}} \text{ (yaw)}$$

where M_α , $\alpha = X, Y, Z$, denotes the moment of force about X, Y, and Z body axes, respectively; $I_{\alpha\alpha}$, $\alpha = X, Y, Z$, denotes the moment of inertia about the X, Y, and Z body axes, respectively; and ω_P , ω_Q , and ω_R are in rad/sec.*

If $OPTN3 > 0$ [input roll option switch, C(3503)], the calculation of $\dot{\omega}_P$ is not accomplished, and missile roll is not simulated (a constant roll rate is maintained).

The derivatives (\dot{C}_{ij} , $i, j = 1, 2, 3$) of the elements of the earth to body transformation matrix, M, are calculated using the following equations:

$$\dot{C}_{11} = (C_{21}) (\omega_R) - (C_{31}) (\omega_Q) \quad .$$

$$\dot{C}_{12} = (C_{22}) (\omega_R) - (C_{32}) (\omega_Q) \quad .$$

$$\dot{C}_{13} = (C_{23}) (\omega_R) - (C_{33}) (\omega_Q) \quad .$$

$$\dot{C}_{21} = (C_{31}) (\omega_P) - (C_{11}) (\omega_R) \quad .$$

$$\dot{C}_{22} = (C_{32}) (\omega_P) - (C_{12}) (\omega_R) \quad .$$

*Note that in the 6 DOF simulation program, ω_P , ω_Q , and ω_R are in deg/sec, so the factor CRAD = 57.295778 appears where appropriate.

$$\begin{aligned}\dot{C}_{23} &= (C_{33}) (\omega_P) - (C_{13}) (\omega_R) \quad . \\ \dot{C}_{31} &= (C_{11}) (\omega_Q) - (C_{21}) (\omega_P) \quad . \\ \dot{C}_{32} &= (C_{12}) (\omega_Q) - (C_{22}) (\omega_P) \quad . \\ \dot{C}_{33} &= (C_{13}) (\omega_Q) - (C_{23}) (\omega_P) \quad .\end{aligned}$$

c. Assumptions

The derivation of $\dot{\omega}_P$, $\dot{\omega}_Q$, and $\dot{\omega}_R$ requires the assumptions that (1) the products of inertia (I_{XY} , I_{XZ} , I_{YZ} , etc.) are zero, and (2) the time derivatives of the principal moments of inertia (\dot{I}_{XX} , \dot{I}_{YY} , \dot{I}_{ZZ}) are zero. The point at which these assumptions are required in deriving these equations is discussed in Appendix A.

A derivation of the matrix element derivations, (\dot{C}_{ij}) , is accomplished in Appendix B. No limiting assumptions, other than that the earth fixed coordinate system is inertial, are required in the derivation.

d. Initialization Subroutines

A rotational dynamics initialization subroutine, (D2I), calculates the initial earth to body axis transformation matrix, M, from the input initial Euler angles ψ , θ , and ϕ , which are defined as follows:

- 1) A positive rotation (toward Y_E from X_E) of ψ (degrees) about the Z_E axis, giving a system e' (X' , Y' , Z').
- 2) A negative rotation (the X' axis up from the plane of the earth axis system) of θ about the Y' axis, giving a system e'' (X'' , Y'' , Z'').
- 3) A positive rotation (toward Z'' from Y'') of ϕ degrees about the X'' axis, given the body axis system $E_B(X_B, Y_B, Z_B)$.

The angles are depicted in Figure 17 where (X_E, Y_E, Z_E) and (X_B, Y_B, Z_B) represent the earth and body axes, respectively.

The resulting transformation, M, from the earth axis system to the body axis system is given by the following equation.

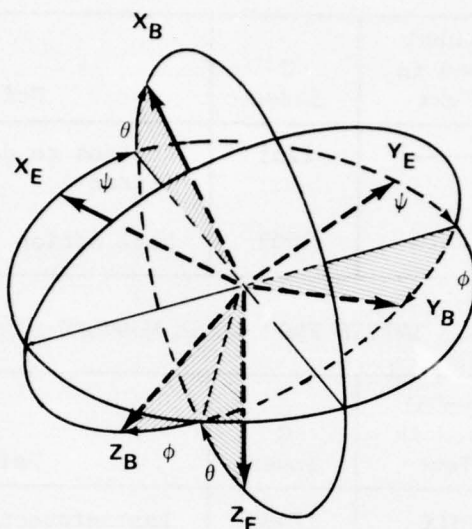


Figure 17. Euler angle geometry.

$$M = \begin{bmatrix} \cos \psi \cos \theta & \sin \psi \cos \theta & -\sin \theta \\ \cos \psi \sin \theta \sin \phi & \cos \psi \cos \phi & \cos \theta \sin \phi \\ -\sin \psi \cos \phi & +\sin \psi \sin \theta \sin \phi & \\ \cos \psi \sin \theta \cos \phi & \sin \psi \sin \theta \cos \phi & \cos \theta \cos \phi \\ +\sin \psi \sin \phi & -\cos \psi \sin \phi & \end{bmatrix} .$$

Thus, a vector \bar{V}_E expressed in the earth axis system is given in the body axis system as $\bar{V}_B = M\bar{V}_E$. The transformation is derived for reference in Appendix C.

e. Input/Output Variables and Cross Reference of C-Array

Tables 27, 28, and 29 present the input/output variables and cross reference of C-array for module D2.

8. G2 - Winds Module

a. Functional Description

Subroutine G2 models the time varying (gusts) component of the winds module. If the Monte Carlo time varying component of the wind has not been selected, then G2 is a dummy routine and nothing

TABLE 27. INPUT FROM DATA CARDS - MODULE D2

Fortran Symbol	Symbol Used in Text	C Index	Definition
CRAD	-----	1751	Radians to degrees conversion factor
OPTN3	-----	3503	Roll option switch

TABLE 28. INPUTS FROM OTHER MODULES - MODULE D2

Fortran Symbol	Symbol Used in Text	C Index	Definition
FMIX	FMIX	1748	Instantaneous values of moments of inertia (slug-ft ²)
FMIY	FMIY	1749	
FMIZ	FMIZ	1750	
FMXBA	FMXBA	1303	Components of the total moments of force about the body coordinate system (ft-lb)
FMYBA	FMYBA	1304	
FMZBA	FMZBA	1305	

is computed. For the deterministic mode or the Monte Carlo steady state mode, the one time wind calculations are made in G2I. The wind velocity components are referenced to the earth fixed coordinate system.

b. Equations

The time varying wind component is simulated by passing white noise through the first order filter shown in Figure 18. The time varying output of the filter is added to the steady state wind component to get the total wind velocity.

The wind gust model contains frequency components that are both a function of distance and time. The time component represents a time varying wind at a fixed point in space while the distance component represents the variation in the steady state component with range. Figure 19 illustrates the nature of the range dependent steady state wind.

The filter constants and the standard deviation of the output are dependent on the missile and quasi-steady state wind velocities and on a parameter referred to as the scale length, L_u . From an

TABLE 29. OUTPUT - MODULE D2

Fortran Symbol	Symbol Used in Text	C Index	Definition
CFA11	C_{11}	1703	Elements of the earth-to-body transformation matrix, M
CFA12	C_{12}	1707	
CFA13	C_{13}	1711	
CFA21	C_{21}	1715	
CFA22	C_{22}	1719	
CFA23	C_{23}	1723	
CFA31	C_{31}	1727	
CFA32	C_{32}	1731	
CFA33	C_{33}	1735	
WP	ω_P	1739	Roll rate about X_B -axis (deg/sec)
WQ	ω_Q	1743	Pitch rate about Y_B -axis (deg/sec)
WR	ω_R	1747	Yaw rate about Z_B -axis (deg/sec)

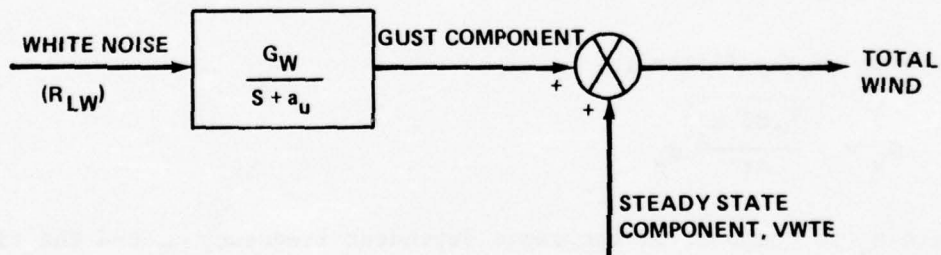


Figure 18. Wind gusts filter.

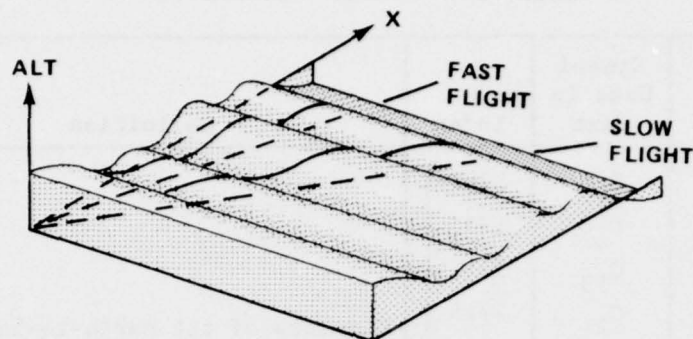


Figure 19. Space dependent wind field model.

examination of the wind profile shown in Figure 19, it can be seen why missile velocity and direction relative to the wind field are important. The velocity and direction determine the frequency at which the crests in the wind field are struck by the missile as it flies downrange. The scale length, L_u , represents roughly the longest distance that two points in the wind field can be separated before correlation between their velocities becomes zero.

The differential equation of the filter is

$$\dot{X} + a_u X = R_{LW} \quad .$$

The gain of the filter is

$$G_w = \sqrt{\frac{1.89 a_u}{\Delta t}} \sigma_u$$

where a_u is composed of the range dependent frequency ω_R and the time dependent frequency ω_T , or

$$a_u = \omega_R + \omega_T \quad .$$

The range dependent frequency ω_R is

$$\omega_R = \frac{u}{L_u} \quad ,$$

where u is the projection of missile velocity (\bar{V}_{MSLE}) onto the wind velocity, or

$$u = \bar{V}_{MSLE} \cdot \frac{\overline{VWTE}}{|\overline{VWTE}|} .$$

The scale length, L_u , (an empirically determined quantity) is

$$L_u = -12.1 \sigma_u + 475 .$$

The time dependent frequency, ω_T , is

$$\omega_T = \frac{|\overline{VWTE}|}{VWTEM} ,$$

where $VWTEM$ is the mean value of the probability distribution (Figure 20) from which the steady state wind (\overline{VWTE}) is initialized for each run of a run set if the steady state wind is to be randomly selected. If however, \overline{VWTE} is not randomly selected, but instead is computed from the standard deviation of the gusts via the equation $VWTE = 2.9 \sigma_u$, then

$$\omega_T = 1 \text{ rad/sec} .$$

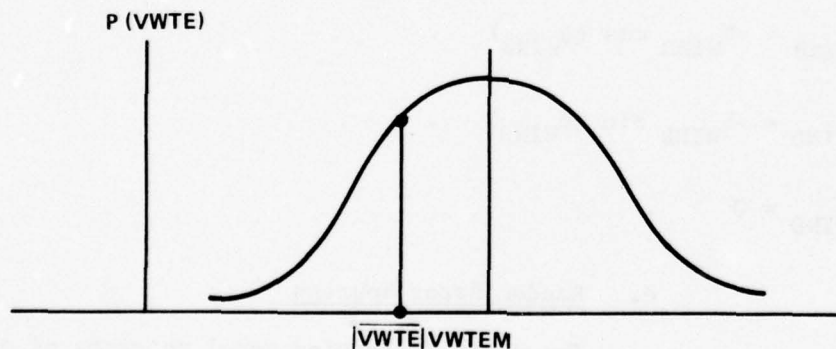


Figure 20. Steady state wind distribution.

The expected standard deviation, σ_u , of the wind gusts model is directly proportional to the steady state wind component $|\overline{VWTE}|$ by

$$\sigma_u = \frac{|\overline{VWTE}|}{2.9} .$$

The option to compute σ_u from the previously mentioned equation or the option to compute $|\overline{VWTE}|$ from

$$|\overline{VWTE}| = 2.9 \sigma_u$$

is left to the user.

c. Initialization Subroutine

The steady state wind magnitude VWTE and direction BPSIW (Figure 21) are modeled in module G2I as Monte Carlo variables. The mean of the steady state wind is the value of VWTE input by type 3 data card, and the mean of the wind direction is the input value of BPSIW input on a type 3 data card. In the deterministic mode, the velocity components of the wind are computed based on input values of wind velocity, V_{WIND} , and wind direction, ψ_{WIND} , as shown in Figure 22. G2I also computes the Monte Carlo initial value of the time series wind gusts.

$$V_{XWIND} = -V_{WIND} \cos (\psi_{WIND}) .$$

$$V_{YWIND} = -V_{WIND} \sin (\psi_{WIND}) .$$

$$V_{ZWIND} = 0 .$$

d. Random Error Sources

The Monte Carlo wind model consists of a steady state wind component and a time varying (gusts) component. Either component of the model may be randomized independently of the other. However, when exercising the time varying model, consideration must be made concerning the relationship between the steady state wind magnitude VWTE and the expected standard deviation SIGU (σ_u) of the time varying component. This relationship was given in Section III.B.8.b. Input combinations of the steady state wind and the time varying wind is given

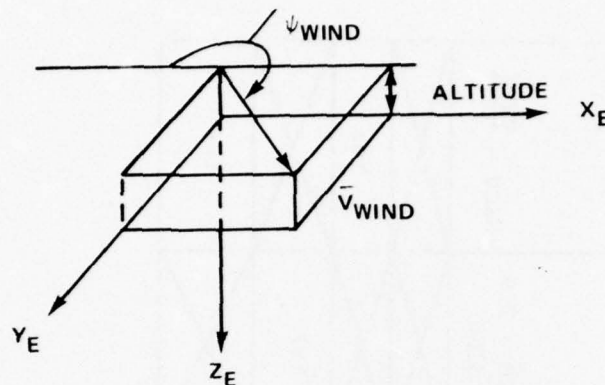


Figure 21. Wind components.

in Table 30. An explanation of each combination follows the table. The type 3 and type 8 input cards referred to in Table 30 are explained in Section IV.A , "Input Card Types."

(1) Monte Carlo Steady State Wind Only. The steady state wind magnitude and direction are randomly selected for each run of the run set from user specified probability distributions. The type 3 card input values of VWTE and BPSIW are the mean values for the probability distributions.

(2) Monte Carlo - Both Steady State and Time Varying Wind. The steady state wind magnitude and direction are randomly selected for each run of the run set from user specified probability distributions. The type 3 card input values of VWTE and BPSIW are the mean values for the probability distributions. The time varying wind component will be randomly generated from MCARLO white noise. The expected standard deviation SIGU will be computed internally from the Monte Carlo value of VWTE for each run of the run set.

(3) Monte Carlo Time Varying Wind Only - Input SIGU. The time varying wind component will be randomly generated from MCARLO white noise. The expected standard deviation SIGU is input via type 3 data card. The steady state wind magnitude VWTE is not randomly selected, but the wind direction BPSIW is. VWTE is computed internally from SIGU. It should be noted that VWTE = 0 must be input via type 3 data card.

(4) Monte Carlo Time Varying Wind Only - Compute SIGU. The time varying wind component will be randomly generated from MCARLO white noise. The expected standard deviation is not input, but is computed internally from VWTE. The steady state wind magnitude VWTE is not randomly selected, but is input via type 3 data card. The

TABLE 30. WIND INPUT COMBINATIONS

	Type 8 Card Input			Type 3 Card Input			Compute Internally	
	1	2	3	4	5	6	7	8
	Wind Gust Flag GVWTE C(70)	Steady State Flag VWTE C(52)	Wind Direction Flag BPSIW C(51)	SIGU (σ_u) C(54)	Mean Steady State Value VWTE C(52)	Mean Wind Direction BPSIW C(51)	VWTE = 2.9 SIGU	SIGU = $\frac{VWTE}{2.9}$
1	No	Yes	Yes	No	Yes	Yes		
2	Yes	Yes	Yes	No	Yes	Yes		Yes
3	Yes	No	Yes	Yes	Yes VWTE = 0	Yes	Yes	
4	Yes	No	Yes	No	Yes VWTE \neq 0	Yes		Yes

wind direction BPSIW is randomly selected from a user specified probability distribution. An example output of combination (3) is given in Figure 22.

e. Input/Output Variables and Cross Reference of C-Array

Tables 31, 32, and 33 present the input/output variables and cross reference of C-array for module G2.

TABLE 31. INPUT FROM DATA CARDS - MODULE G2

Fortran Symbol	Symbol Used in Text	C Index	Definition
OPTNW		50	Wind option selector: 0 - no winds 1 - include steady winds
BPSIW	ψ_{WIND}	51	Wind direction: angle between wind velocity vector and the negative X-axis (deg)
VWTE	V_{WIND}	52	Wind speed with respect to the ground (ft/sec)

TABLE 32. INPUT FROM OTHER MODULES - MODULE G2

Fortran Symbol	Symbol Used in Text	C Index	Definition
BLU	L_u	56	Scale length
WNDWO	ω_T	58	Time dependent frequency
SLWD	\dot{X}	59	Filter variable
RLW	R_{LW}	60	White noise
SLW	X	62	Filter variable
CBPSIW	$\cos(\psi_{WIND})$	65	X-component of wind direction
SBPSIW	$\sin(\psi_{WIND})$	66	Y-component of wind direction
GSIGU	-	69	Temporary variable = $\sigma_u \sqrt{\frac{1.89}{\Delta t}}$

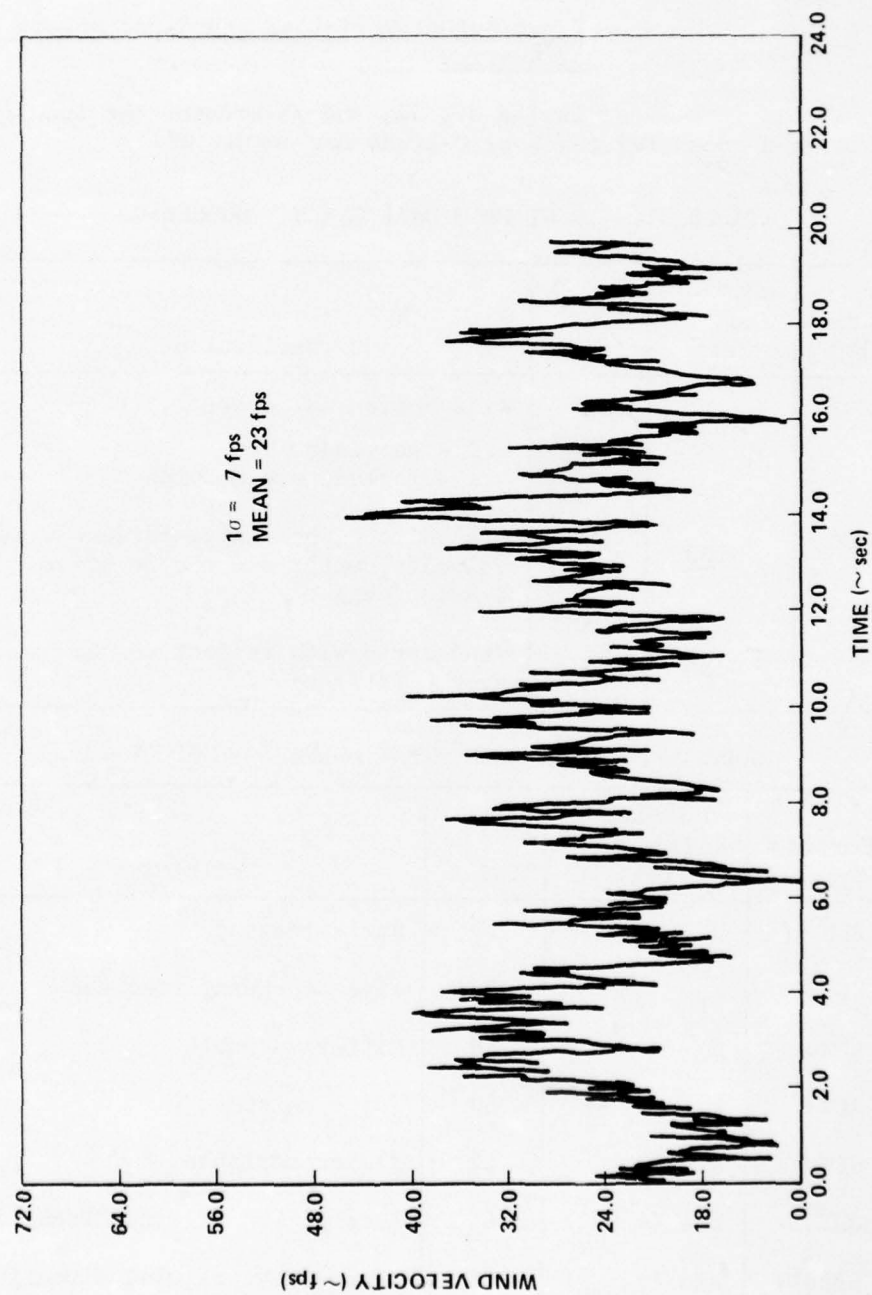


Figure 22. Typical wind gusts output.

TABLE 33. OUTPUT - MODULE G2

Fortran Symbol	Symbol Used in Text	C Index	Definition
VWXE	V _{XWIND}	100	Components of the wind velocity relative to the earth fixed coordinate system (ft/sec)
VWYE	V _{YWIND}	101	
VWZE	V _{ZWIND}	102	

f. Wind Monte Carlo Variables

The variables associated with the Monte Carlo wind model are given in Table 34.

TABLE 34. MONTE CARLO INPUTS - MODULE G2

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
BPSIW	51	G2I	BPSIW	51	Wind direction (deg)
VWTE	52	G2I	VWTE	52	Steady state wind magnitude (ft/sec)
GVWTE	70	(G2I) (G2)	GVWTE	70	Total wind magnitude, steady state plus time varying
SIGU	54	-	-	-	Time varying wind standard deviation (ft/sec). Input by type 3 data card

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

9. G3 - Air Data

a. Functional Description

Subroutine G3 computes the missile velocity with respect to the wind, and two atmospheric properties, density and speed of sound. The magnitude of the missile velocity, the atmospheric density and speed of sound are then used to compute Mach number and dynamic pressure.

b. Equations

- 1) Missile velocity with respect to wind -

$$\bar{V}_{MW} = \bar{V}_{MISSILE} - \bar{V}_{WIND} \quad .$$

- 2) Missile altitude -

$$h = -R_{ZE} + R_{ZO}$$

where

R_{ZE} = Z-component of missile position in earth coordinates

R_{ZO} = Altitude of earth coordinate system above ground.

- 3) Atmospheric density -

$$\rho = \frac{\rho_0}{1 + kh + k_1 h^3}$$

where

$$\rho_0 = 0.076475$$

$$k = 0.3325 \times 10^{-4}$$

$$k_1 = 0.02315 \times 10^{-12} \quad .$$

- 4) Atmospheric speed of sound -

$$a = k_2 h + a_0$$

where

$$a_0 = 1117.3$$

$$k_2 = -0.00392 \quad .$$

5) Dynamic pressure -

$$P = \frac{1}{2} \rho \frac{|\bar{V}_{MW}|^2}{g_0} \quad .$$

6) Mach number -

$$M = \frac{|\bar{V}_{MW}|}{a} \quad .$$

c. Input/Output Variables and Cross Reference of C-Array

Tables 35, 36, and 37 present input/output variables and cross reference of C-array for module G3.

TABLE 35. INPUT FROM DATA CARDS - MODULE G3

Fortran Symbol	Symbol Used in Text	C Index	Definition
RHZRO	R_{ZO}	208	Altitude of earth fixed coordinate system above ground (ft)

TABLE 36. INPUT FROM OTHER MODULES - MODULE G3

Fortran Symbol	Symbol Used in Text	C Index	Definition
VWXE } VWYE } VWZE }	\bar{V}_{WIND}	100 } 101 } 102 }	Wind velocity components in earth fixed coordinate system (ft/sec)
VXE } VYE } VZE }	$\bar{V}_{MISSILE}$	1603 } 1607 } 1611 }	Velocity components of missile in earth fixed coordinate system (ft/sec)
RZE	R_{ZE}	1623	Z-component of missile position in earth fixed coordinate system (ft)

TABLE 37. OUTPUT - MODULE G3

Fortran Symbol	Symbol Used in Text	C Index	Definition
VMWXE } VMWYE } VMWZE }	\bar{V}_{MW}	200 } 201 } 202 }	Components of missile velocity relative to the wind in the earth fixed coordinate system (ft/sec)
PDYNMC	P	203	Dynamic pressure (lb/ft ²)
VMACH	M	204	Mach number
DRHO		205	Atmospheric density (lb/ft ³)
VSOUND	a	206	Atmospheric speed of sound (ft/sec)
VAIRSP	$ \bar{V}_{MW} $	207	Magnitude of missile velocity relative to wind (airspeed) (ft/sec)
RH	h	209	Altitude of missile above ground (ft)

10. G4 - Terminal Geometry

a. Functional Description

This subroutine monitors the line-of-sight vector $\bar{\Delta R}(t)$ at the end of each integration step to determine if the point of closest approach (target plane intersection) to the target has been passed. If the closest approach point has been passed, integration is halted and the time of closest approach (t_0), the position of the target with respect to the missile ($\bar{\Delta R}_0$), and the miss distance (RMIS) are computed. After computation of the miss distance, two optional sets of data are also computed at this point. If there are any "type 10" input cards (IMVCT > 0), then the mean and standard deviation for the specified "type 10" parameters are computed. Also, if any time series Monte Carlo variables are present (ITCT > 0), then several laser spot jitter parameters are computed and printed. These include the maximum deviation of the laser spot jitter components and the mean and mean square values of the spot jitter components. After these computations, LCONV is set to 2 to flag subroutine STGE3 that the trajectory computation is to be terminated.

The time and position at closest approach are computed by linear interpolating the time (t_1) and position ($\overline{\Delta R}_1$) values just prior to closest approach and the time (t_2) and position ($\overline{\Delta R}_2$) values following closest approach (Figure 23). The time and position values following closest approach exist as current values of time (t) and position ($\overline{\Delta R}$) on the trajectory, while the time (t_1) and position ($\overline{\Delta R}_1$) just prior to closest approach were saved on the previous pass through this subroutine.

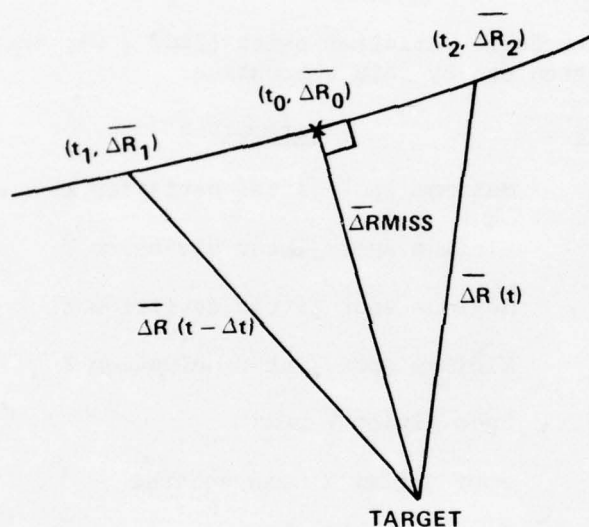


Figure 23. Point of closest approach.

G4 also monitors the altitude (RDELZ) of the missile relative to the target. If the altitude becomes negative, it is assumed that ground impact has occurred. If ground impact does occur, the run termination switch, LCONV, is set to 2 to flag STGE3 to terminate trajectory computation.

After bracketing the closest approach point and interpolation for the time and position, the following parameters are output via this subroutine:

<u>Parameter</u>	<u>Definition</u>
RMISS	Miss distance (ft)
t_0	Flight time at closest approach (sec)

<u>Parameter</u>	<u>Definition</u>
RDELX(ΔX) RDELY(ΔY) RDELZ(ΔZ)	Position components of the target with respect to the missile in the system centered at the missile and parallel to the earth fixed frame (ft)
RYFP(YFP) RZFP(ZFP)	Position components of the target in the flight plane frame (the X-component is not output since it is assumed to be zero) (ft)

If time series Monte Carlo variables exist (ITCT > 0), then the following parameters are written out by this subroutine:

<u>Parameter</u>	<u>Definition</u>
C(1567)	Maximum spot jitter deviation Y
C(1568)	Minimum spot jitter deviation Y
C(1577)	Maximum spot jitter deviation Z
C(1578)	Minimum spot jitter deviation Z
YMC	Spot jitter Y mean
YMC2	Spot jitter Y mean squared
ZMC	Spot jitter Z mean
ZMC2	Spot jitter Z mean squared
XMCSPT	Spot jitter radial root mean squared

b. Equations

To monitor the line-of-sight vector, the position of the target is first transformed into a flight path coordinate system aligned with missile velocity by

$$\overline{RFP} = [M] \overline{\Delta R},$$

where

$$\overline{\Delta R} = \begin{bmatrix} \Delta X \\ \Delta Y \\ \Delta Z \end{bmatrix} \quad \begin{array}{l} \text{Position of target with respect to missile in a} \\ \text{system parallel to the earth fixed coordinate} \\ \text{system} \end{array}$$

$$\overline{\text{RFP}} = \begin{bmatrix} \text{XFP} \\ \text{YFP} \\ \text{ZFP} \end{bmatrix} \quad \text{Position of target with respect to missile in flight plane coordinate system}$$

and

$$M = \begin{bmatrix} \cos \gamma_H \cos \gamma_V & \sin \gamma_H \cos \gamma_V & -\sin \gamma_V \\ -\sin \gamma_H & \cos \gamma_H & 0 \\ \cos \gamma_H \sin \gamma_V & \sin \gamma_H \sin \gamma_V & \cos \gamma_V \end{bmatrix} \quad .$$

The previously mentioned transformation involves a rotation from the earth fixed axes through the heading angle γ_H and the flight path angle γ_V to the flight plane coordinate system as shown in Figure 24.

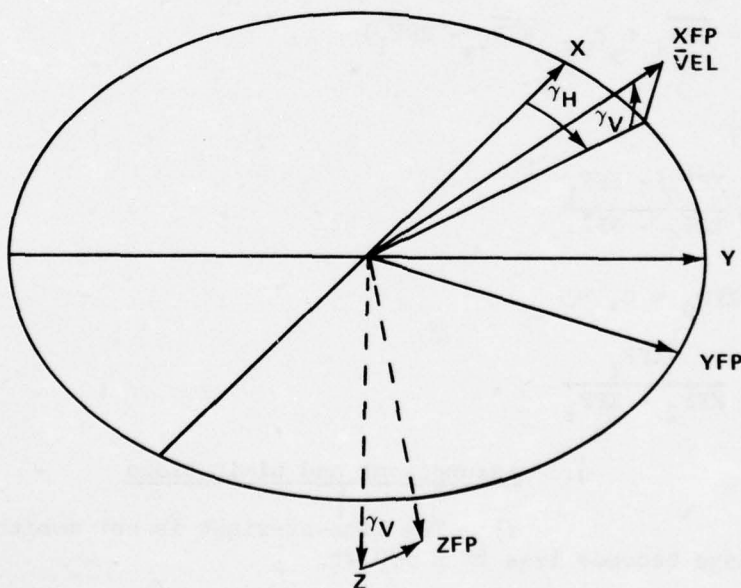


Figure 24. Flight plane coordinate system.

Transforming the line-of-sight vector into the flight plane coordinate system simplifies the determination of closest approach passage, because the X-component (XFP) of the line-of-sight will be

zero at closest approach. This condition exists because the X-axis (XFP) is coincident with the velocity vector and the line-of-sight is normal to the velocity at the closest approach point.

To determine closest approach passage, the value of XFP is monitored. A positive XFP means the target lies ahead of the missile. A negative XFP means the target lies behind the missile. When the value of XFP changes sign from one integration step to the next, closest approach has been bracketed. At this time, integration is halted and the time (t_0) and position ($\overline{\Delta R}_0$) of closest approach is computed by interpolation. Interpolation is performed using XFP as the independent variable. Thus,

$$t_0 = t_1 + P_{CT} (t_2 - t_1)$$

$$\overline{\Delta R}_0 = \overline{\Delta R}_1 + P_{CT} (\overline{\Delta R}_2 - \overline{\Delta R}_1)$$

and

$$\overline{RFP}_0 = \overline{RFP}_1 + P_{CT} (\overline{RFP}_2 - \overline{RFP}_1) ,$$

where

$$P_{CT} = \frac{XFP_0 - XFP_1}{XFP_2 - XFP_1} ;$$

and since $XFP_0 = 0$,

$$P_{CT} = \frac{-XFP_1}{XFP_2 - XFP_1} .$$

c. Assumptions and Limitations

1) The line-of-sight is not monitored until a slant range becomes less than 500 ft.

2) For a slant range greater than 500 ft, the Z-component (RDELZ) of the target with respect to the missile is monitored to determine ground impact.

3) The flight plans coordinate system is aligned with the missile earth fixed velocity vector. If appreciable target motion exists, then the condition that the X-component (XFP) of RFP is equal to zero at the point of closest approach to the target is not precisely true.

d. Input/Output Variables and Cross Reference of C-Array

Tables 38 and 39 present the input/output variables and cross reference of C-array for module G4.

TABLE 38. INPUT FROM OTHER MODULES - MODULE G4

Fortran Symbol	Symbol Used in Text	C Index	Definition
BGAMH	γ_H	357	Horizontal flight path angle (heading) (deg)
BGAMV	γ_V	358	Vertical flight path angle (deg)
RANGE		371	Distance from target (ft)
RDELX	ΔX	1635	Position components of target (line-of-sight) with respect to the missile in earth fixed coordinate system (ft)
RDELY	ΔY	1636	
RDELZ	ΔZ	1637	
T	t	2000	Flight time (sec)
ITCT	ITCT	3721	Total number "type 8" parameters
IMVCT	IMVCT	3030	Total number "type 10" parameters
IMVNDX		3020	The mean, standard deviation variable C-index that appears on the "type 10" card
YMC	YMC	1564	Spot jitter Y mean
YMC2	YMC2	1565	Spot jitter Y mean squared
ZMC	ZMC	1574	Spot jitter Z mean
ZMC2	ZMC2	1575	Spot jitter Z mean squared

11. G5 - Coordinate Conversion Module

a. Functional Description

G5 computes all the angles pertaining to the position and velocity of the vehicle (the proportional navigation angles and look vector angles) and makes three coordinate transformations.

TABLE 39. OUTPUT - MODULE G4

Fortran Symbol	Symbol Used in Text	C Index	Definition
LCONV	LCONV	2020	Integration termination switch
RMISS	RMISS	300	Miss distance (measured in target plane)
RXF	YFP	301	Position components of target with respect to missile in the flight plane coordinate system (ft)
RYF	YFP	302	
RZF	ZFP	303	
VSD		3000	"Type 10" parameter standard deviation
VMEAN		3010	"Type 10" parameter mean

The components of the spin axis of the 2-DOF gyro (inertial platform for roll attitude stabilization) is computed in the earth fixed coordinate system along with the two Euler angles defining the orientation of the gyro relative to the body coordinate system. The angles computed and the transformations made in this subroutine are:

- 1) Euler angles of the body coordinate system relative to the earth-fixed coordinate system.
- 2) Inertial platform gyro spin axis position components and Euler angles.
- 3) Target position with respect to the missile, missile total velocity, and missile position with respect to the moving rail launcher.
- 4) Transformation of missile line-of-sight from earth fixed coordinate system into the body coordinate system.
- 5) Vertical and horizontal line-of-sight angles.
- 6) Vertical and horizontal proportional navigation angles.
- 7) Vertical and horizontal flight path angles of the missile with respect to the earth fixed axes.
- 8) Transformation of the velocity relative to the air from the earth fixed coordinate system into the body coordinate system.
- 9) Angle of attack with respect to the wind.
 - a) Vertical (α) and horizontal (β) angles of attack.
 - b) Alpha prime (α' - absolute angle of attack) and phi prime (ϕ' - aerodynamic roll angle with respect to wind) angles (wind tunnel axes).

b. Equations

(1) Euler Angles of the Body Coordinate

System. The three Euler angles (γ, θ, ϕ) are computed from elements of the earth-to-body transformation matrix, $[M]$. The matrix is computed in D2, the rotational dynamics subroutine, and passed into this subroutine by the COMMON BLOCK C. The matrix is defined as

$$M = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix} .$$

The relationship between each element value and the three Euler angles is given in Appendix C. It can be seen from these relationships that

$$\phi = \tan^{-1} \frac{C_{23}}{C_{33}} \quad (\text{Euler roll})$$

$$\theta = \tan^{-1} \frac{-C_{13}}{\sqrt{C_{11}^2 + C_{12}^2}} \quad (\text{Euler pitch})$$

$$\psi = \tan^{-1} \frac{C_{12}}{C_{11}} \quad (\text{Euler yaw}) .$$

(2) Inertial Platform Position Components

and Euler Angles. The inertial platform is a 2 DOF gyro. The gyro is oriented with its spin axis aligned with the initial Y-body axis of the vehicle as shown in Figure 25. The outer gimbal is aligned with the roll axis of the missile, and the inner gimbal is aligned with the yaw axis as shown in Figure 26.

Gyro initial orientation matrices are set in D2I, the rotational dynamics initialization subroutine. The gyro matrix is defined as:

$$A0 = \begin{bmatrix} A0_{11} & A0_{12} & A0_{13} \\ A0_{21} & A0_{22} & A0_{23} \\ A0_{31} & A0_{32} & A0_{33} \end{bmatrix} ,$$

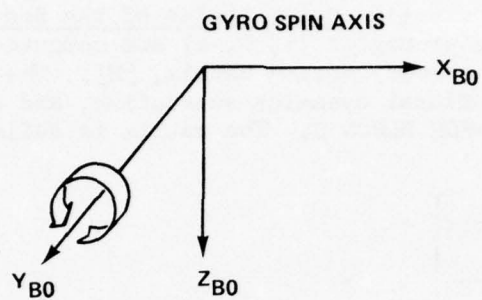


Figure 25. Initial orientation of the 2 DOF gyro.

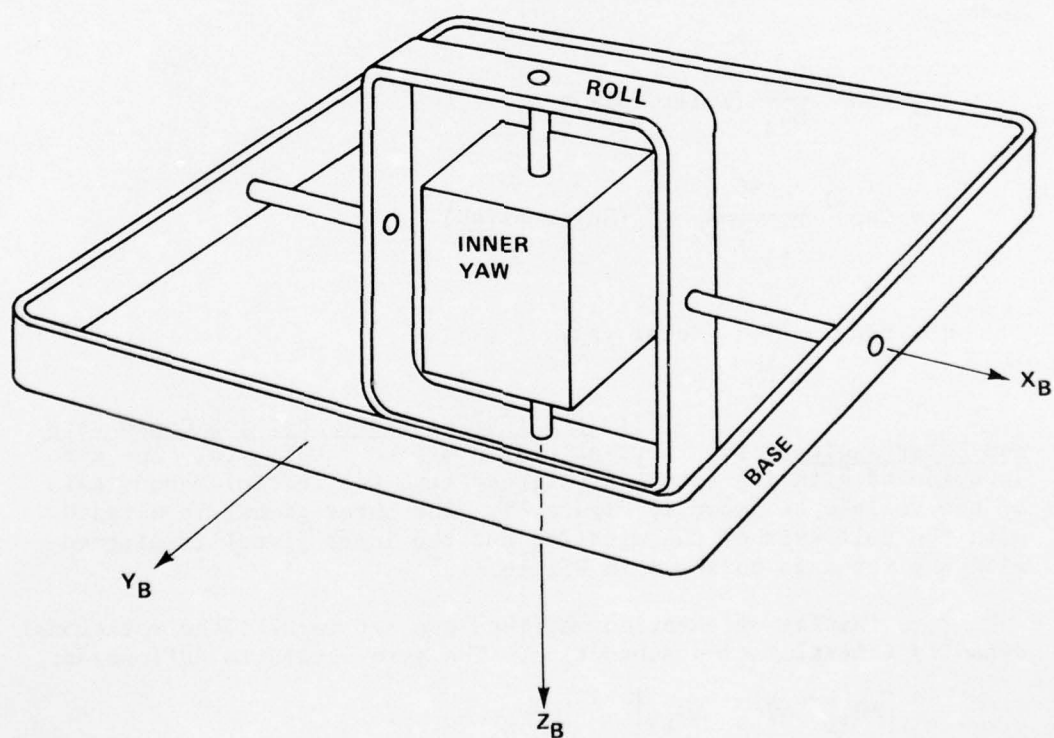


Figure 26. Roll gyro orientation.

where

$$\begin{bmatrix} A0_{11} & A0_{12} & A0_{13} \\ A0_{21} & A0_{22} & A0_{23} \\ A0_{31} & A0_{32} & A0_{33} \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix} \text{ at } t = 0 .$$

The elements are taken from the earth-to-body coordinate system transformation matrix M computed at the initial time point or, $[A0] = [M]$ at $t = 0$. This subroutine (G5) transforms the axes of the gyro from the initial body coordinate system through the earth fixed system to the current body coordinate system and then computes the roll angle detected by the gyro. Thus,

$$\begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}_{\text{GYRO}} = [M] [A0]^T \begin{bmatrix} X_{B0} \\ Y_{B0} \\ Z_{B0} \end{bmatrix}_{\text{GYRO}} .$$

Substituting the components of the gyro ($X_{B0} = 0$, $Y_{B0} = 1$, $Z_{B0} = 0$) into the previously mentioned equation gives,

$$\begin{bmatrix} X_B \\ Y_B \\ Z_E \end{bmatrix}_1 = \begin{bmatrix} C_{11}A0_{21} + C_{12}A0_{22} + C_{13}A0_{23} \\ C_{21}A0_{21} + C_{22}A0_{22} + C_{23}A0_{23} \\ C_{31}A0_{21} + C_{32}A0_{22} + C_{33}A0_{23} \end{bmatrix} .$$

The roll angle is shown in Figure 27 and is computed by

$$\phi_1 = \tan^{-1} \left(\frac{Z_{B1}}{Y_{B1}} \right) .$$

(3) Target Position (Line-of-Sight Vector) with Respect to the Missile, Missile Total Velocity, and Missile Position with Respect to the Moving Rail Launcher. The missile total velocity in the earth fixed coordinate system is

$$V_{\text{TOTE}} = \sqrt{V_{\text{XE}}^2 + V_{\text{YE}}^2 + V_{\text{ZE}}^2} .$$

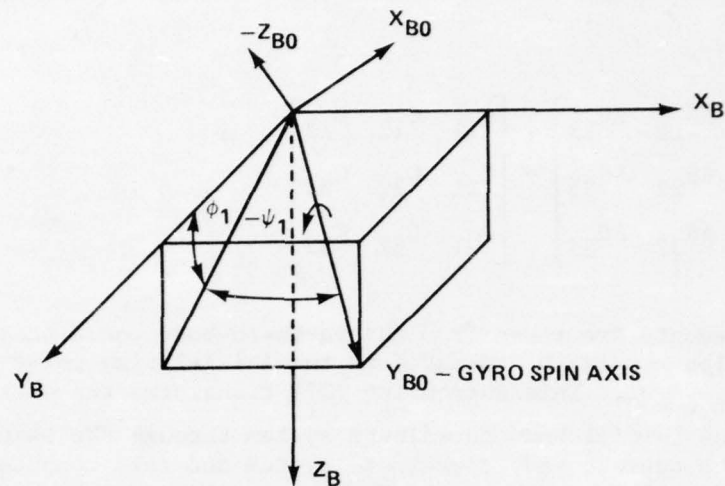


Figure 27. Gyro Euler angles.

The target position (line-of-sight vector) with respect to the missile (Figure 28) is

$$\bar{R}_{\nabla} = \bar{R}_T - \bar{R}_E \quad (\text{line-of-sight vector})$$

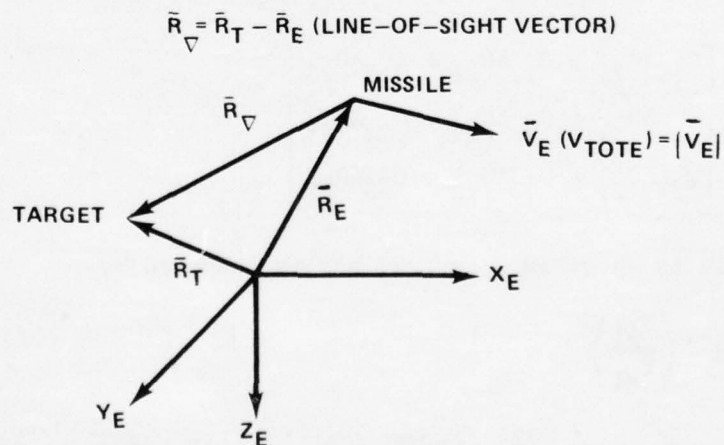


Figure 28. Earth fixed coordinate system.

To determine missile separation from the launch rail, the position and motion of the rail is required along with the position and motion of the missile. The motion of the rail is assumed to be composed of a constant linear velocity with respect to the earth (\bar{V}_0 , the missile initial velocity, Figure 29).

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JUL 76 C L LEWIS, W R HOOKER, A W LEE
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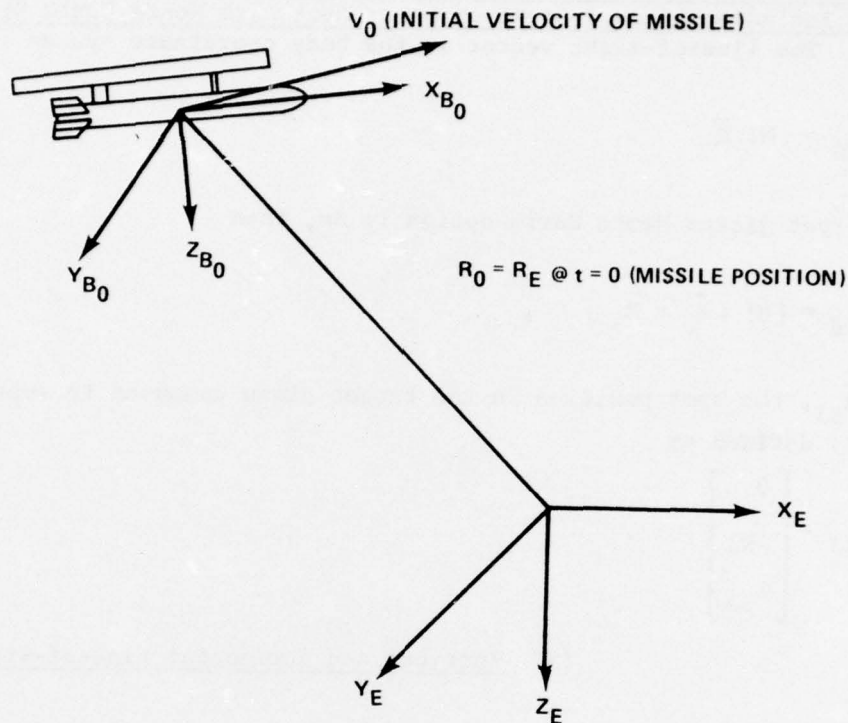


Figure 29. Launcher initial position and velocity.

The initial position of the rail is assumed to be \bar{R}_0 , the initial position of the missile. Thus, the position of the launcher as a function of time in the earth fixed coordinate system is

$$\bar{R}_L = \bar{R}_E + \bar{V}_0 t \quad .$$

Missile position with respect to the launcher then becomes

$$\Delta \bar{R}_{ML} = \bar{R}_E - \bar{R}_L \quad ,$$

with the magnitude of the separation being

$$R_{ANGO} = \sqrt{\Delta X_{ML}^2 + \Delta Y_{ML}^2 + \Delta Z_{ML}^2} \quad .$$

(4) Transformation of the Missile Line-of-Sight from the Earth Fixed Coordinate System into the Body Coordinate System, Including Line-of-Sight of Laser Spot with Monte Carlo Spot Jitter. The line-of-sight vector in the body coordinate system is

$$\bar{R}_{TB} = [M] \bar{R}_{\nabla} .$$

If the spot jitter Monte Carlo option is on, then

$$\bar{R}_{TB} = [M] [\bar{R}_{\nabla} + \bar{R}_{SJ}] ,$$

where \bar{R}_{SJ} , the spot position in the target plane computed in subroutine SPOT, is defined as

$$\bar{R}_{SJ} = \begin{bmatrix} 0 \\ Y_{SJ} \\ Z_{SJ} \end{bmatrix} .$$

(5) Vertical and Horizontal Line-of-Sight Angles.

$$\gamma_H = \tan^{-1} \frac{-\Delta Y_{LOS}}{\Delta X_{LOS}}$$

$$\gamma_V = \tan^{-1} \frac{-\Delta Z_{LOS}}{\sqrt{\Delta X_{LOS}^2 + \Delta Y_{LOS}^2}}$$

The slant range from missile to the target is given as

$$RANGE = \sqrt{\Delta X_{LOS}^2 + \Delta Y_{LOS}^2 + \Delta Z_{LOS}^2} ,$$

where

$$\begin{bmatrix} \Delta X_{LOS} \\ \Delta Y_{LOS} \\ \Delta Z_{LOS} \end{bmatrix} = \bar{R}_{\nabla} . \quad (\text{See Figure 30}).$$

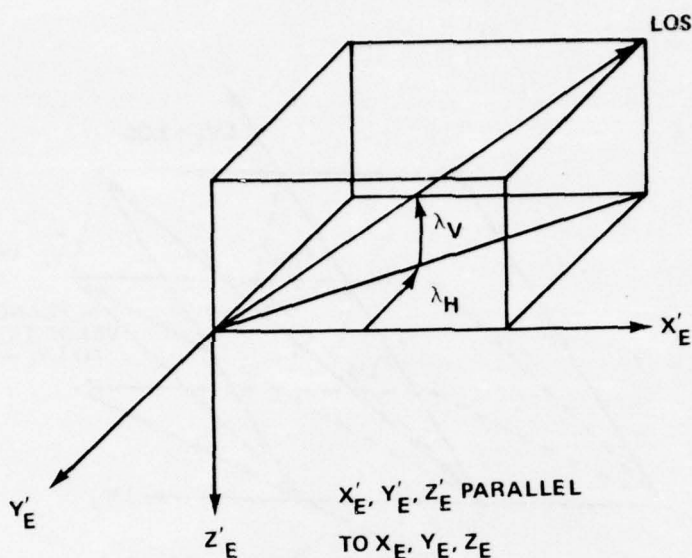


Figure 30. Vertical and horizontal line-of-sight angles.

(6) Vertical and Horizontal Proportional Navigation. Vertical and horizontal proportional navigation angles are defined in the coordinate system shown in Figure 31. The vertical and horizontal proportional navigation angles gives the orientation of the missile velocity vector relative to the line-of-sight vector. In deriving these angles, the assumption is made that the velocity of the target is negligible with respect to the missile velocity.

This coordinate system is established with the line-of-sight vector as the \overline{LV}_1 -axis; \hat{LV}_2 is normal to the line-of-sight vector and lying in a horizontal plane; and \overline{LV}_3 completes a right-handed system. The proportional navigation angles are the angles defining the orientation of the missile velocity with respect to the line-of-sight. These angles are shown in Figure 31.

The line-of-sight coordinate system is established by

$$\begin{aligned}\overline{LV}_1 &= \overline{\Delta R}_{LOS} \\ \hat{LV}_2 &= \frac{(\hat{k}_E \times \overline{LV}_1)}{|\hat{k}_E \times \overline{LV}_1|} *\end{aligned}$$

* \hat{k}_E is a unit vector along the Z_E -axis, and \times represents a cross product.

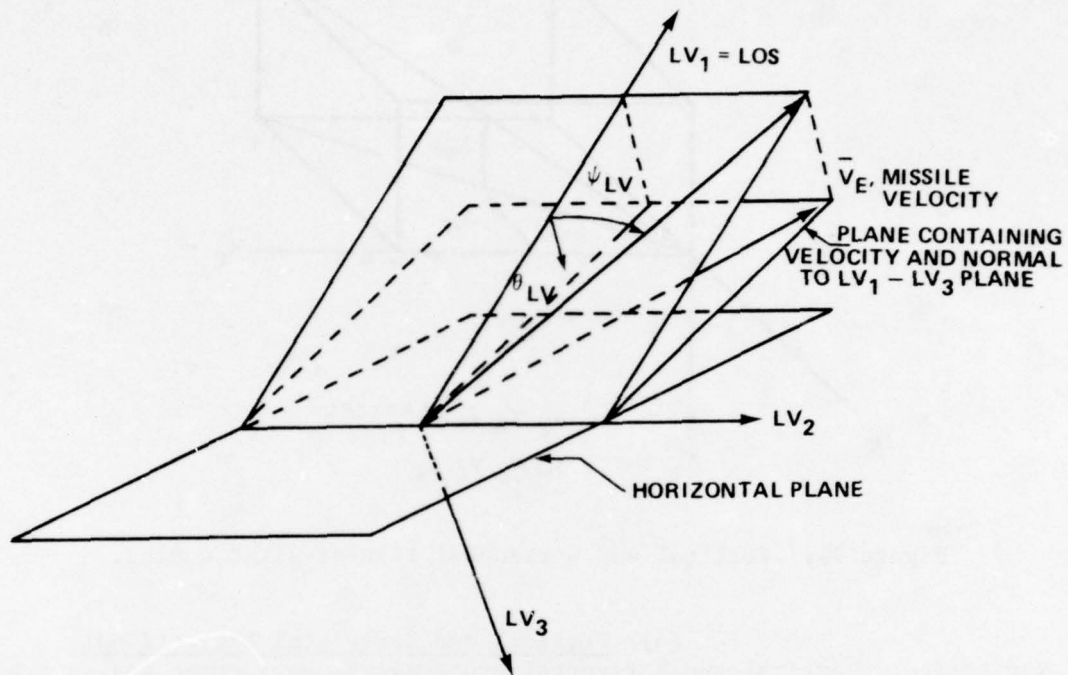


Figure 31. Proportional navigation angles.

and

$$\overline{LV}_3 = \overline{LV}_1 \times \hat{LV}_2 \quad .$$

The magnitude of $\hat{k}'_E \times \overline{LV}_1$ may be found by considering that

$$\hat{k}_E \times \overline{LV}_1 = \hat{k}_E \times \overline{\Delta R}_{LOS}$$

and that

$$\hat{k}_E \times \overline{\Delta R}_{LOS} = (\Delta R \sin \beta) \hat{\gamma} \quad .$$

Now, $\Delta R \sin \beta$ is simply the projection of ΔR into the $X_E - Y_E$ plane.

Thus,

$$\Delta R \sin \beta = \sqrt{\Delta X_{LOS}^2 + \Delta Y_{LOS}^2} \quad .$$

Therefore,

$$\hat{LV}_2 = \frac{(\hat{k}_E \times \overline{LV}_1)}{\sqrt{\Delta X_{LOS}^2 + \Delta Y_{LOS}^2}} \quad .$$

To determine the navigation angles, the missile velocity is projected onto each axis of the LV coordinate system. This produces the components of the velocity in this system. Thus, the angles are computed by

$$\theta_{LV} = \tan^{-1} \frac{\overline{V}_E \cdot \hat{LV}_3}{\overline{V}_E \cdot \hat{LV}_1} \quad *$$

and

$$\psi_{LV} = \tan^{-1} \frac{\overline{V}_E \cdot \hat{LV}_2}{\overline{V}_E \cdot \hat{LV}_1} \quad .$$

(7) Vertical and Horizontal Flight Path Angles in the Earth Fixed Coordinate System.

$$\gamma_V = \tan^{-1} \left(\frac{-V_{ZE}}{\sqrt{V_{XE}^2 + V_{YE}^2}} \right)$$

and

$$\gamma_H = \tan^{-1} \left(\frac{V_{YE}}{V_{XE}} \right) \quad (\text{see Figure 32}) \quad .$$

(8) Transformation of the Velocity Relative to the Wind from the Earth Fixed Coordinate System into the Body Coordinate System. The velocity of the missile with respect to the wind, calculated in subroutine G3, is transformed into the body axes by

*The dot "." represents a dot product.

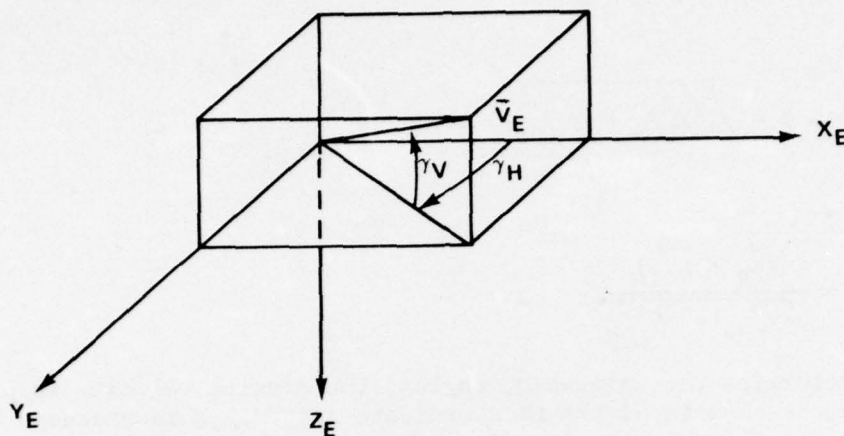


Figure 32. Vertical (γ_V) and horizontal (γ_H) flight path angles.

$$\bar{V}_{MWB} = [M] \bar{V}_{MWE} ,$$

where

$$\bar{V}_{MWB} = \begin{bmatrix} V_{MWU} \\ V_{MWV} \\ V_{MWW} \end{bmatrix} .$$

(9) Angle of Attack with Respect to Wind Axes. The geometry relating to the angles of attack of the missile with respect to the wind is illustrated in Figure 3 of Section III.B.1 and Figure 33. The calculation of these angles is bypassed if the engine is thrusting (Flag QBURN \leq 0) and the missile is still on the launch rail (RANGO \leq RAIL).

The vertical angle of attack (α) and the horizontal angle of attack (β) is given in the following equations:

$$\alpha = \tan^{-1} \left(\frac{V_{MWW}}{V_{MWU}} \right)$$

and

$$\beta = \tan^{-1} \left(\frac{V_{MWV}}{V_{MWU}} \right) . \quad (\text{See Figure 33})$$

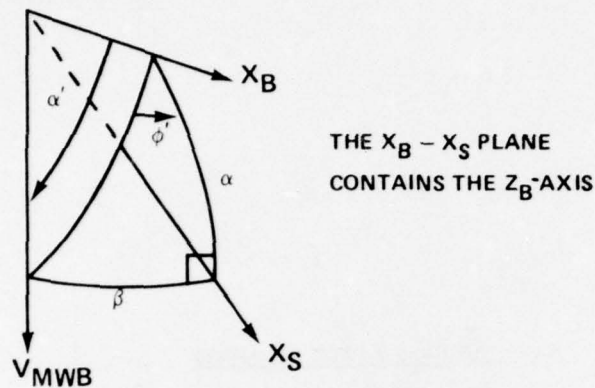


Figure 33. Angles of attack.

From spherical trigonometry and assuming a small angle of sideslip, β , (the small angle β allows a right triangle to be formed by the chords of the angles α , β , and α') the absolute angle of attack, α' , and the roll angle of the missile with respect to the wind axes, ϕ' , may be computed based on small angle approximations by

$$\alpha'^2 = \alpha^2 + \beta^2$$

and

$$\phi' = \tan^{-1} \frac{\alpha}{\beta} .$$

Conventionally, small angle approximations limits the angle magnitudes to approximately 10° . However, in the derivation of the previously mentioned equations, half angles ($\alpha/2$, $\beta/2$) appear in the formulas that are simplified through the small angle approximation. Thus, since

$$\frac{\alpha}{2} \leq 10^\circ$$

and

$$\frac{\beta}{2} \leq 10^\circ ,$$

then

$$\alpha \leq 20^\circ$$

and

$$\beta \leq 20^\circ$$

is allowed.

c. Random Error Sources

G5 contains logic for the computation of one Monte Carlo error source, the roll attitude gyro drift. D11 sets the initial value for this error source.

(1) Roll Gyro Drift. The roll gyro is a 2 DOF gyro and is assumed to have drift in both axes. The drift rates, P_1 and R_1 , about the roll and yaw axes, respectively, are selected randomly in D11. The effect of these drift rates are transformed to the position coordinates of the gyro by

$$\dot{X}_1 = R_1 Z_{B01}$$

$$\dot{Y}_1 = P_1 Z_{B01}$$

$$\dot{Z}_1 = (P_1 Y_{B01} - R_1 X_{B01})$$

Since the rates are assumed to be constant, gyro position can be determined by direct integration. Thus,

$$X_1 = \dot{X}_{B01} t$$

$$Y_1 = \dot{Y}_{B01} t + 1$$

$$Z_1 = \dot{Z}_{B01} t$$

(The integration constants for the position coordinates are 0, 1, 0 as stated in Section III.B.11.b).

d. Input/Output Variables and Cross Reference of C-Array

Tables 40 and 41 present the input/output variables and cross reference of C-array for module G5.

TABLE 40. INPUTS FROM OTHER MODULES - MODULE G5

Fortran Symbol	Symbol Used in Text	C Index	Definition
VMWXE } VMWYE } VMWZE }	\bar{V}_{MWE}	200 } 201 } 202 }	Components of missile velocity relative to the wind in earth fixed system (ft/sec)
VAIRSP		207	Velocity magnitude of missile relative to wind (ft/sec)
QBURN		1405	Engine burnout switch (1 = burnout)
VXE } VYE } VZE }	V_{XE} V_{YE} V_{ZE}	1603 } 1607 } 1611 }	Components of missile velocity in earth fixed coordinate (ft/sec)
RXE } RYE } RZE }	\bar{R}_E	1615 } 1619 } 1623 }	Position components of missile in earth fixed coordinate system (ft)
RTXE } RTYE } RTZE }	\bar{R}_T	1651 } 1655 } 1659 }	Position components of target in earth fixed coordinate system (ft)
R XO } R YO } R ZO }	\bar{R}_O	1668 } 1669 } 1670 }	Initial position components of missile and rail in fixed system (ft)
V XO } V YO } V ZO }	\bar{V}_O	1671 } 1672 } 1673 }	Initial velocity - components of missile and rail in earth fixed system (ft/sec)

TABLE 40. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
CFA11	C_{11}	1703	Elements of the earth-to-body transformation matrix, M
CFA12	C_{12}	1707	
CFA13	C_{13}	1711	
CFA21	C_{21}	1715	
CFA22	C_{22}	1719	
CFA23	C_{23}	1723	
CFA31	C_{31}	1727	
CFA32	C_{32}	1731	
CFA33	C_{33}	1735	
A021	$A0_{21}$	1755	Position components of gyro 1 (inertial platform) spin axis unit vector in earth fixed coordinate system
A022	$A0_{22}$	1756	
A023	$A0_{23}$	1757	
A031	$A0_{31}$	1758	Position components of gyro 2 (inertial platform) spin axis unit vector in earth fixed coordinate system
A032	$A0_{32}$	1759	
A033	$A0_{33}$	1760	
T	t	2000	Flight time (sec)
RSJYMC	Y_{SJ}	1680	Y-component actual spot location
RSJZMC	Z_{SJ}	1681	Z-component actual spot location
RSPOTX		1682	Target position components in earth fixed system with spot jitter added
RSPOTY		1683	
RSPOTZ		1684	
P1	P_1	1764	Roll gyro roll drift rate (deg/sec)
R1	R_1	1765	Roll gyro yaw drift rate (deg/sec)

TABLE 41. OUTPUT - MODULE G5

Fortran Symbol	Symbol Used in Text	C Index	Definition
BTHT	θ	350	Euler pitch angle of body system (deg)
BPSI	ψ	351	Euler yaw angle of body system (deg)
BPHI	ϕ	352	Euler roll angle of body system (deg)
BPH1	ϕ_1	353	Euler roll angle of inertial platform (gyro 1) with respect to the body system (deg)
BTH2	θ_2	354	Euler pitch angle of inertial platform (gyro 2) with respect to the body system (deg)
BPS1	ψ_1	355	Euler yaw angle of the inertial platform (gyro 1) with respect to the body system (deg)
BPH2	ϕ_2	393	Euler roll angle of inertial platform (gyro 2) with respect to the body system (deg)
VTOTE	V_{TOTE}	356	Missile total velocity magnitude in the earth fixed frame (ft/sec)
BGAMH	γ_H	357	Horizontal flight path angle (heading) measured clockwise from X_E -axis (deg)
BGAMV	ψ_V	358	Vertical flight path angle measured positive up from the local horizontal (deg)
BTHLV	θ_{LV}	363	Vertical proportional navigation angle, measured positive downward from the line-of-sight vector to the projection of the missile velocity into the vertical plane that contains the line-of-sight vector (deg)
BPSLV	ψ_{LV}	364	Horizontal proportional navigation angle measured positive clockwise from the line-of-sight vector to the projection of the missile velocity into the plane containing the line-of-sight vector and normal to the vertical plane (deg)

TABLE 41. (Continued)

Fortran Symbol	Symbol Used in Text	C Index	Definition
BLAMV	λ_V	365	Vertical line-of-sight angle, measured from the local horizontal to the line-of-sight vector (deg)
BLAMH	λ_H	366	Horizontal line-of-sight angle, measured from X_E -axis to the projection of the line-of-sight vector into local horizontal plane (deg)
BALPHA	α	367	Vertical angle of attack, measured from the projection of the missile velocity with respect to the wind into the $X_B - Z_B$ plane and the X_B -axis (deg)
BALPHY	β	368	Horizontal angle of attack (sideslip) measured from the projection of the missile velocity with respect to the wind into the $X_B - Z_B$ plane and the velocity relative to the wind (deg)
BALPHP	α'	369	Total angle of attack between vehicle X_B -body axis and the velocity relative to the wind (deg)
BPHIP	ϕ'	370	Aerodynamic roll angle between the plane containing the $Z_B - X_B$ axes and the plane containing X_B velocity relative to the wind (deg)
RANGE	RANGE	371	Slant range from missile to the target (ft)
RXBA	ΔX_{BLOS}	372	X-component of missile line-of-sight (ΔR_{BLOS}) in body coordinates (ft)
RYBA	ΔY_{BLOS}	373	Y-component of missile line-of-sight (ΔR_{BLOS}) in body coordinates (ft)
RZBA	ΔZ_{BLOS}	374	Z-component of missile line-of-sight (ΔR_{BLOS}) in body coordinates (ft)

TABLE 41. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
RANGO	R_{ANGO}	380	Magnitude of the separation distance between the rail launcher and the missile. (Measured from rear end of launcher to the rear lug of missile) (ft)
RXL	ΔX_{ML}	390	X-component of the missile position with respect to the launcher (ft)
RYL	ΔY_{ML}	391	Y-component of the missile relative to the launcher in the earth fixed coordinate frame (ft)
RZL	ΔZ_{ML}	392	Z-component of the missile relative to the launcher in the earth fixed coordinate frame (ft)
RDELX	ΔX_{LOS}	1635	X-component of missile line-of-sight ($\Delta \bar{R}_{\text{LOS}}$) in earth fixed coordinate system (ft)
RDELY	ΔY_{LOS}	1636	Y-component of missile line-of-sight ($\Delta \bar{R}_{\text{LOS}}$) in earth fixed coordinate system (ft)
RDELZ	ΔZ_{LOS}	1637	Z-component of missile line-of-sight ($\Delta \bar{R}_{\text{LOS}}$) in earth fixed coordinate system (ft)

e. Monte Carlo Input Variables and Cross Reference of C-Array

Table 42 presents the Monte Carlo input variables and cross reference of C-array for module G5.

12. S1 - Seeker Module

The seeker module, S1, currently used in the 6 DOF simulation program models a quadrant (laser) tracker. Two other seekers, a digital/linear laser seeker and an optical contrast seeker, are available as options as explained in Section III.B.12.h.

TABLE 42. MONTE CARLO INPUT - MODULE G5

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
P1	1764	D1I	P1	1764	Roll gyro roll drift rate
R1	1765	D1I	R1	1765	Roll gyro yaw drift rate

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

a. Functional Description

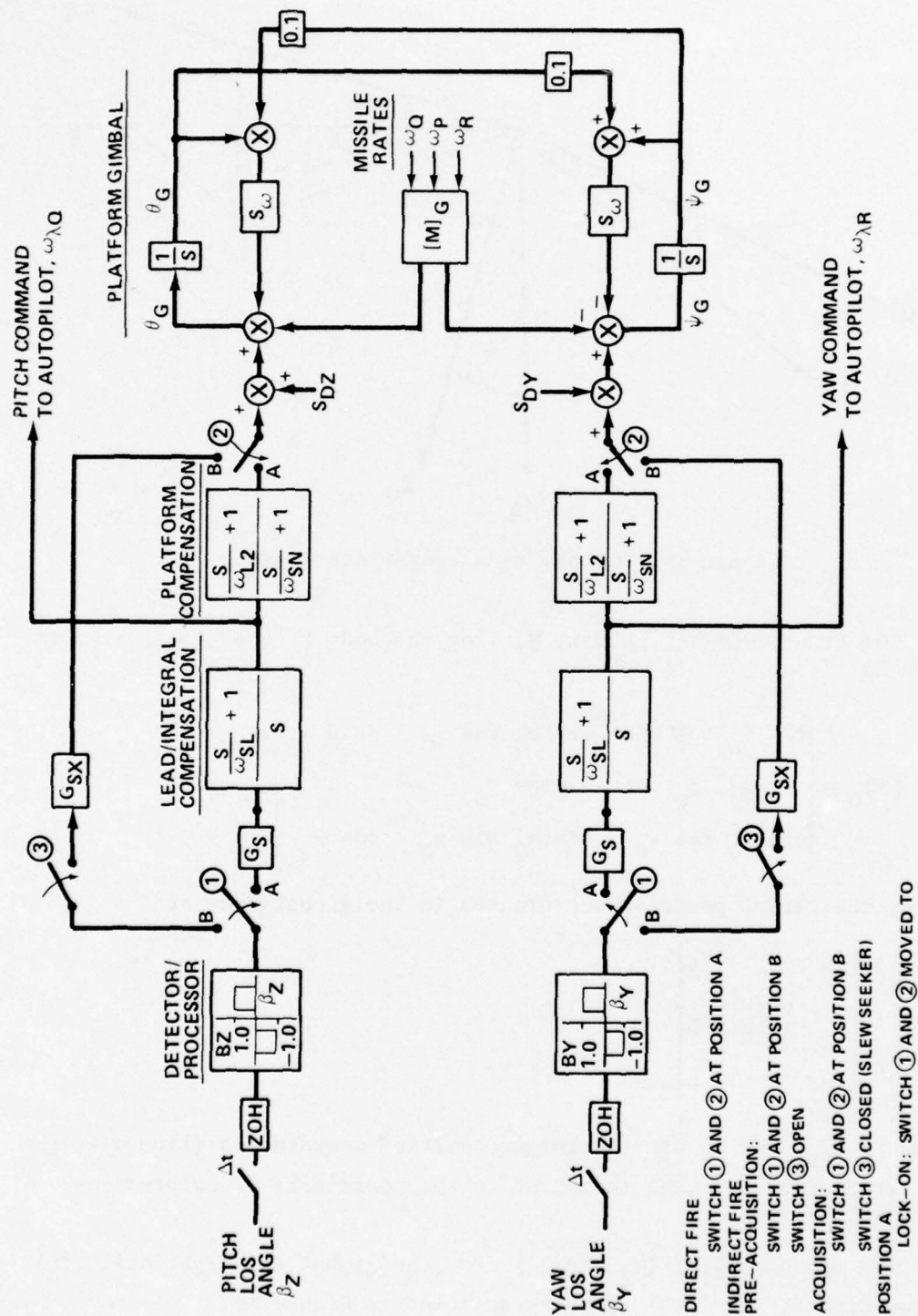
Figure 34 is the block diagram representation of the laser seeker as it is implemented in the 6 DOF simulation program. The transfer functions given in each of the blocks were transformed by use of the M-method into state variable format for solution by numerical integration.

There are options in module S1 for bypassing the lead integral compensation and platform compensation that are not shown in this block diagram. However, these options are dealt with in detail in the following sections.

b. Equations

(1) Line-of-Sight Calculation. The initial portion of the module logic determines target position (modeled as a point source) in the gimbal axes. This operation consists of transforming the X, Y, and Z components of target position from the body axes to the gimbal axes, then calculating the angular offsets (from the gimbal boresight axis) in pitch and yaw.

As is depicted in Figure 35, the gimbal axes, (X_G, Y_G, Z_G) , orientation with respect to the body axes, (X_B, Y_B, Z_B) , is specified by two rotations; the first through an angle of ψ_G about the Z_B -axis, and the second through an angle of θ_G about Y_G (the sign of the angles following the right-hand rule convention).



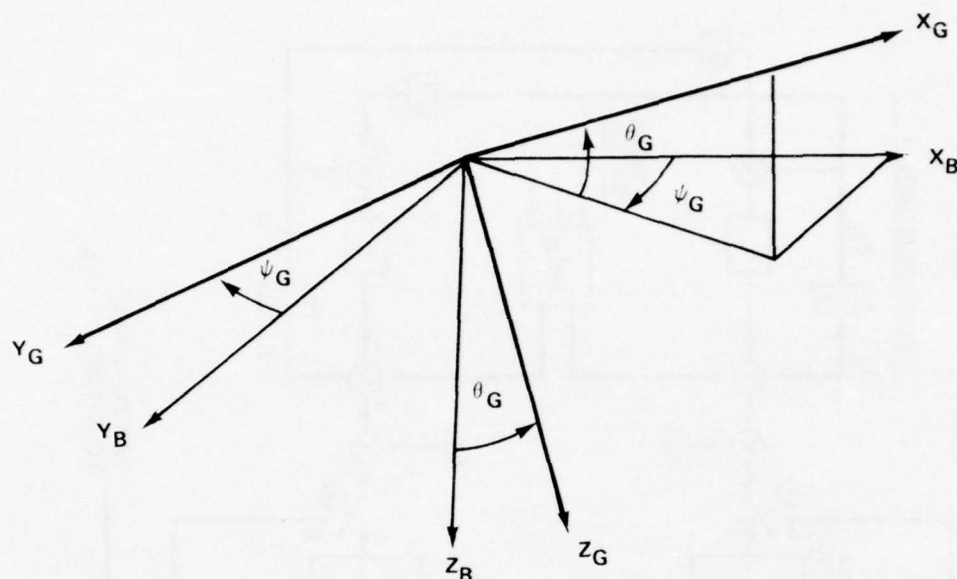


Figure 35. Gimbal axes coordinate system.

The transformation matrix, M , from the body to the gimbal axes is given by

$$[M]_G = \begin{bmatrix} \cos \theta_G \cos \psi_G & \sin \psi_G \cos \theta_G & -\sin \theta_G \\ -\sin \psi_G & \cos \psi_G & 0 \\ \sin \theta_G \cos \psi_G & \sin \theta_G \sin \psi_G & \cos \theta_G \end{bmatrix} .$$

Hence, the target position coordinates in the gimbal axes are

$$\begin{bmatrix} X_G \\ Y_G \\ Z_G \end{bmatrix}_G = [M]_G \begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}_B ,$$

where X_B , Y_B , and Z_B are the target position coordinates (line-of-sight vector) in the body axes (computed in the coordinate transformation module, G5).

The offset angles (β_Z and β_Y) from the gimbal boresight axis (X_G) follow directly from the geometry depicted in Figure 36.

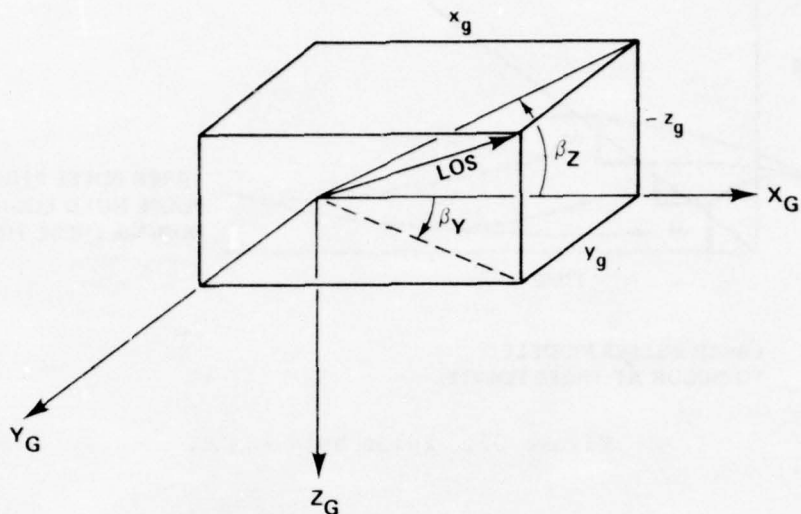


Figure 36. Angular offset of line-of-sight from seeker boresight axis (X_G).

Thus,

$$\beta_z = \tan^{-1} \frac{-z_g}{x_g}$$

and

$$\beta_y = \tan^{-1} \frac{y_g}{x_g} .$$

(2) Pulse Hold Logic. The sampler and zero order hold (ZOH) represents the pulsed nature of the received laser energy. Modeling of these events is done by holding the last detector pulse Δt seconds, at which time a new laser pulse is received. Thus, the seeker detector time function will appear as shown in Figure 37.

(3) Seeker Detector/Processor. The laser seeker assembly, mounted on a two axis, momentum stabilized platform, contains a quadrant detector for sensing of laser energy reflected from the target and focused into a fixed diameter spot. The detector output, Figure 38, is processed by electronics into a signal of constant amplitude that changes in sign as the spot moves from quadrant to quadrant. Thus, the detector output signal in pitch and yaw is

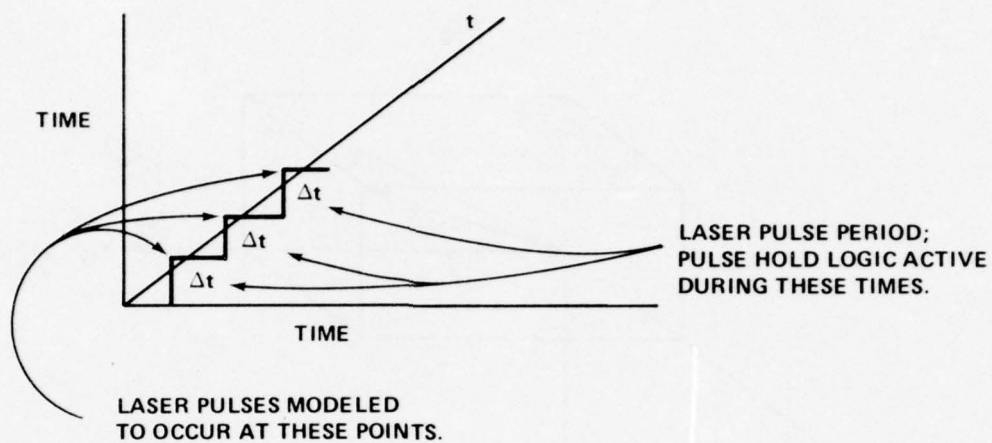


Figure 37. Pulse hold logic.

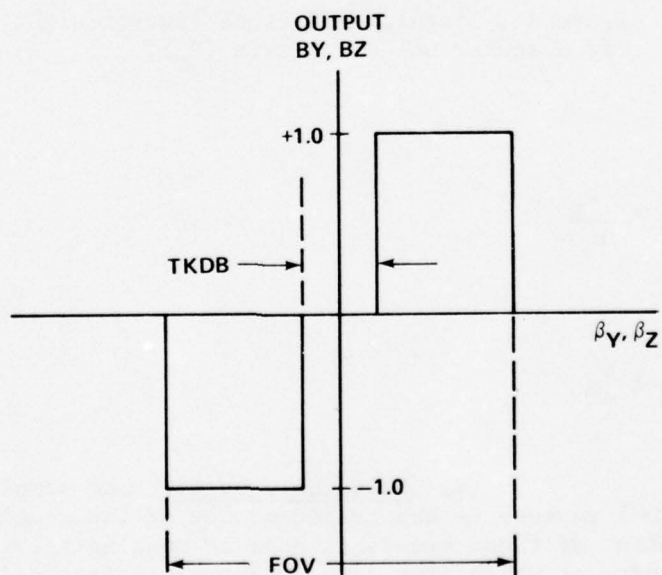


Figure 38. Processor output.

$$BZ = \begin{cases} +1, & \text{if } \beta_Z > 0 \\ -1, & \text{if } \beta_Z < 0 \end{cases} \quad (\text{pitch})$$

$$BY = \begin{cases} +1, & \text{if } \beta_Y > 0 \\ -1, & \text{if } \beta_Y < 0 \end{cases} \quad (\text{pitch})$$

In addition to the ± 1 output, two instances of zero output are possible. One is due to tracker deadband and the other is due to target moving out of field-of-view limits.

(a) Range Dependent Deadband

Determination - Range dependent deadband determination is found using the following equation:

$$TKDB = \left(\frac{BDB}{2} \right) \left(\frac{RANGE}{32810} \right)^2 ,$$

where TKDB is one-half the total range dependent deadband, BDB is the input total deadband normalized to 10 km (32,810 ft), and RANGE is the missile to target slant range. A rationale for computing deadband in this manner is, the reflected laser energy will vary as $1/(RANGE)^2$, so the photoelectric current differential between the four quadrants will also vary as a function of $1/(RANGE)^2$. Since the photoelectric current differential also varies by the amount of image center offset from the detector center, there will be a minimum detectable image offset due to detector and amplifier noise. Therefore, if $(|\beta_Z| < TKDB)$ $BZ = 0$ and if $(|\beta_Y| < TKDB)$ $BY = 0$, set pitch or yaw detector outputs to zero if target angular offset in pitch or yaw are within the deadband.

(b) Target In or Out of Field-of-View

Determination - The target is out of the elliptical field-of-view defined by ϕ_Y and ϕ_Z , if

$$\frac{\beta_Y^2}{\phi_Y^2} + \frac{\beta_Z^2}{\phi_Z^2} > 1 .$$

The geometry of this determination is shown in Figure 39.

From Figure 39, using small angle approximations (specifically, the Y and Z coordinates of field-of-view and target position are taken to be the arc lengths, e.g., $Y_{FOV} \approx r \phi_Y / 57.3$, with angles in degrees), the equation for the field-of-view ellipse boundary is

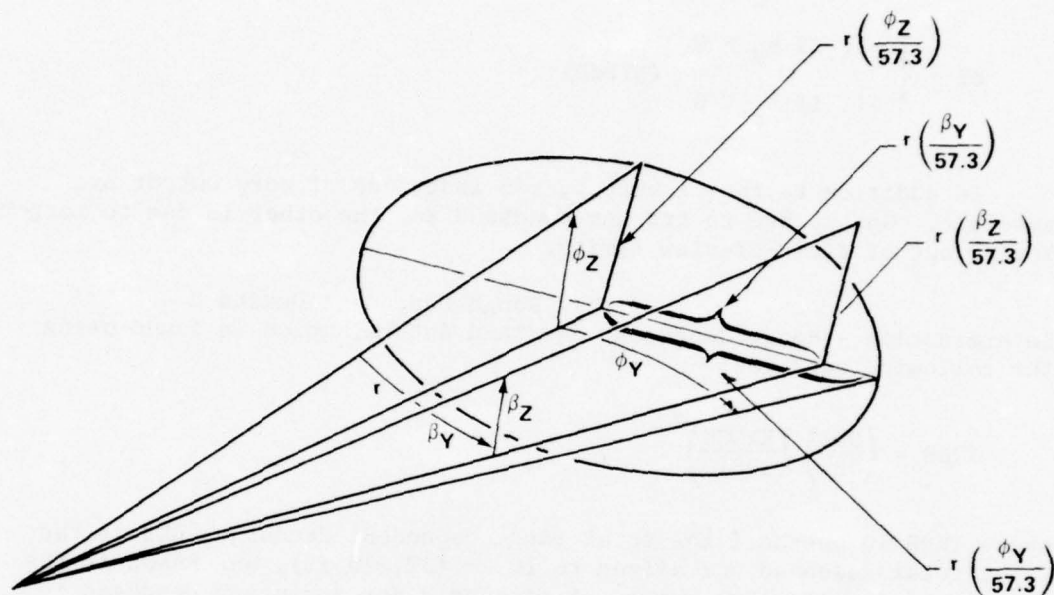


Figure 39. Target in or out of field of view determination.

$$\frac{Y^2}{r^2 \frac{\phi_Y}{57.3}} + \frac{Z^2}{r^2 \frac{\phi_Z}{57.3}} = 1$$

If the point (Y, Z) is such that the left hand side is greater than 1, then (Y, Z) is outside the field-of-view ellipse. Replacing Y and Z with the target components, $r \beta_Y/57.3$ and $r \beta_Z/57.3$, and cancelling the r's and the 57.3, yields

$$\frac{\beta_Y^2}{2} + \frac{\beta_Z^2}{2} > 1$$

the condition for the target being outside the field-of-view.

(4) Direct Fire: Prelaunch Lock-on to Target (OPTN4 = 1). There are two seeker model options for calculating autopilot and seeker gimbal torque error signals. One option directly outputs the detector error signal times a gain factor. The second integrates the detector gain and permits a seeker signal shaping term

and a response time factor to be input (lead integral compensation). In both of these options, the same signals are used for both the autopilot and the seeker gimbal torque. A third option (platform compensation, which can be exercised only if the second of the previously discussed two options is used) allows the response of the seeker gimbal torque signal to be controlled by input independently of the autopilot signal.

(a) Detector Error Signal Times a Gain Output Directly - Detector error signal times a gain output directly is found using the following equations:

$$\omega_{\lambda Q} = G_s \beta_Z$$

$$\omega_{\lambda R} = G_s \beta_Y$$

$$\omega_{QP} = \omega_{\lambda Q}$$

and

$$\omega_{RP} = \omega_{\lambda R} ,$$

where $\omega_{\lambda Q}$ and $\omega_{\lambda R}$ are the pitch and yaw commands to the autopilot, and ω_{QP} and ω_{RP} are seeker torque commands.

(b) Detector Error Signal Lead Integral Compensation - Detector error signal lead/integral compensation is found using the following equations:

$$\omega_{\lambda Q} = \frac{G_s \beta_Z + \Phi}{\omega_{SL}} + \int_0^t G_s \beta_Z + \Phi \, dt$$

$$\omega_{\lambda R} = \frac{G_s \beta_Y + \Phi}{\omega_{SL}} + \int_0^t G_s \beta_Y + \Phi \, dt$$

$$\omega_{QP} = \omega_{\lambda Q}$$

and

$$\omega_{RP} = \omega_{\lambda R} ,$$

where Φ is an input term which can be used to change the operating level of the detector error signal*, and ω_{SL} is an input seeker signal lead factor.

The block diagram for $\omega_{\lambda Q}$ transformed by the M-method, is shown in Figure 40. An analogous block represents β_Y .

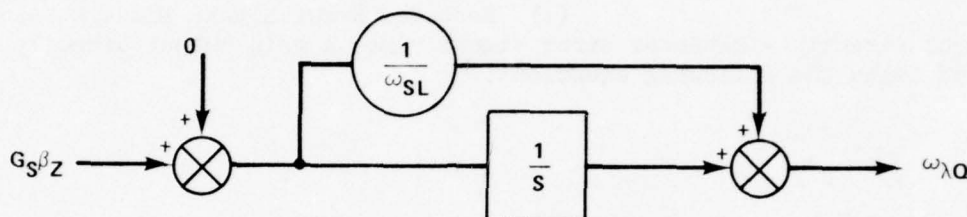


Figure 40. Error signal processing when $\omega_{SL} > 0$.

The pulse hold logic causes β_Z and β_Y to behave as a positive or negative unit step function, depending upon whether the point source target is in the upper or lower two quadrants of the detector. Consequently, the term

$$\frac{G_S \beta_Z + \Phi}{\omega_{SL}}$$

is a step function with amplitude $\pm G_S$, when $\Phi = 0$, $\omega_{SL} = 1$. The integrated term is a ramp function with slope $\pm G_S$. The quantity contributed by the term $G_S \beta_Z + \Phi/\omega_{SL}$, superimposed on the ramp function, provides the output signal $\omega_{\lambda Q}$ with a faster response to a detector error signal change than would be obtained with only the integrated term.

(c) Platform Compensation (Utilized Only When $\omega_{SN} > 0$) - An additional seeker signal compensation network following the lead integral compensation is optional. The equations for the compensation network are

$$\dot{\omega}_{LQS} = \omega_{SN} (\omega_{\lambda Q} - \omega_{LQS})$$

*A positive input value of Φ , for example, would cause the detector output signal to ride on the value of $\Phi > 0$, which would positive bias the pitch and yaw error signals to the autopilot. To simulate gyro drift, Φ can be used.

$$\dot{\omega}_{LRS} = \omega_{SN} (\omega_{\lambda R} - \omega_{LRS})$$

and

$$\omega_{QP} = \frac{\dot{\omega}_{LQS}}{\omega_{L2}} + \omega_{LQS}$$

$$\omega_{RP} = \frac{\dot{\omega}_{LRS}}{\omega_{L2}} + \omega_{LRS}$$

The block diagram for the seeker gimbal torque signals is shown in Figure 41 for the pitch channel (an analogous block can be drawn for the yaw-channel).

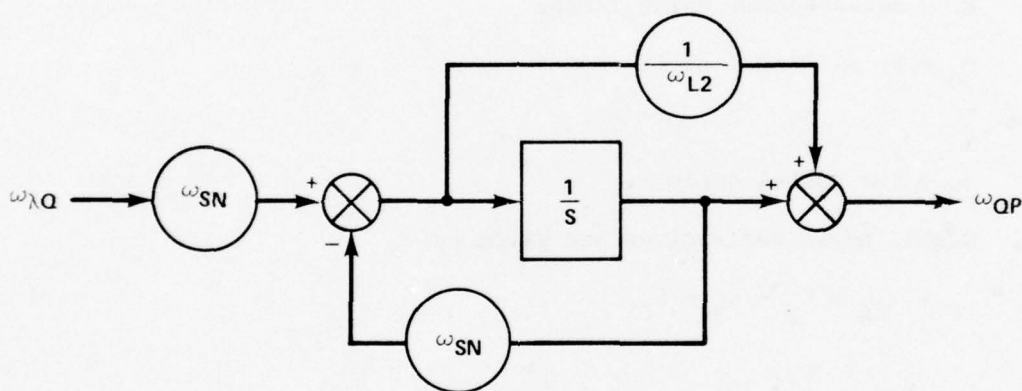


Figure 41. Platform compensation by M-method transformation ($\omega_{SN} > 0$).

(d) Seeker Gimbal Dynamics - After calculation of the seeker error signals for autopilot and seeker gyro gimbal torques, the seeker module transforms missile body rates to the seeker gimbal axes and calculates seeker gimbal angle derivatives. Only first order seeker dynamics such as seeker drift rate and gimbal coupling are considered.

In order to transform missile body rates to seeker gimbal axes

$$\begin{bmatrix} \omega_X \\ \omega_Y \\ \omega_Z \end{bmatrix}_{\text{Gimbal Axes}} = [M]_G \begin{bmatrix} \omega_P \\ \omega_Q \\ \omega_R \end{bmatrix}_{\text{Body Axes}},$$

where $[M]_G$ is the body axes to seeker gimbal axes transformation matrix. Because the seeker is not gimballed about the X_B -axis, the ω_X -component is not calculated.

Gimbal coupling terms are given by

$$U_{ZK} = S_{\omega} (-\theta_G + 0.1 \psi_G) ,$$

and

$$U_{YK} = S_{\omega} (-\psi_G - 0.1 \theta_G) ,$$

where

S_{ω} = Autoerection drift factor

θ_G = Pitch gimbal angle

and

ψ_G = Yaw gimbal angle .

Gimbal angle derivatives are given by

$$\dot{\theta}_G = \omega_{QP} + C_Z - \omega_Y + S_{DZ}$$

$$\dot{\psi}_G = \omega_{RP} + C_Y - \frac{\omega_Z}{\alpha_{33}} + S_{DY} ,$$

where

S_{DZ}, S_{DY} = Seeker drift rates

α_{33} = The (3,3) element of the body to seeker gimbal axes transformation matrix, M_G .

(5) Indirect Fire: Launch without Lock-on to Target (OPTN4 > 1). In the indirect fire mode, the missile is launched prior to target lock-on. The seeker is caged along the missile longitudinal axis (CAGE = 0), and no signals are processed for output to the autopilot. Thus, the autopilot operates open loop with respect to the seeker. However, the autopilot does operate closed loop about the rate sensor gyros of the autopilot in order to maintain a controlled flight until target acquisition and seeker lock-on. Target acquisition in this case refers to the time that the target comes into the field-of-view, but prior to the time that it crosses the midpoint of the field-of-view in pitch and yaw.

Two events must occur for target acquisition. One, the target must be close enough so that the reflected laser energy is detectable by the seeker. And, two, the target must lie within the field-of-view of the seeker.

When both of these events occur, the acquisition phase is entered. The seeker is then slewed toward the target at a constant rate based on detector output of ± 1 and a high gain, G_{SX} . Thus, pitch and yaw seeker commands are

$$\omega_{QP} = G_{SX} B_Z$$

and

$$\omega_{RP} = G_{SX} B_Y \quad .$$

When the target crosses the centerline of the seeker detector, the slew commands are switched out, the seeker is locked on, and normal tracker operation is begun. At this point, all conditions of direct fire are in effect.

While the seeker is being slewed toward the target, the autopilot remains open loop to the seeker. No autopilot guidance commands are initiated until the target crosses the seeker centerline. When this occurs, the switch TRKZY is set to line to flag the autopilot to commence proportional navigation guidance.

c. Assumptions and Limitations

The following assumptions are made in the 6 DOF seeker model:

- 1) The target is modeled as a point source.
- 2) The point source may include motion due to laser designator jitter.
- 3) The seeker 2 DOF gyro is modeled without second order dynamics.
- 4) Reflected pulses are always present at the input PRF and are always detected when in the field-of-view.
- 5) Detector image resolution deadband is a function of range only.
- 6) The seeker pitch to yaw and yaw to pitch coupling terms assume an inertially stabilized platform.
- 7) Seeker gimbal angle limiting is not modeled.

8) Numerical integration must be synchronized with sample period [4] (τ at ZOH) in order to insure accurate integration. Logic is built into the seeker subroutines to insure that integration and sample period are synchronized. This is accomplished by

$$\Delta t = \frac{\tau}{\left[\text{AINT} \left(\frac{\tau}{\Delta t_{\text{INPUT}}} \right) \right]}$$

where

τ = ZOH sample period (sec)

Δt_{INPUT} = Input integration stepsize (sec)

$\text{AINT}(X)$ = Computer function that integerizes the argument (X)

Δt = Integration stepsize that the program will use.

The above function will always compute an integration stepsize that is equal to or greater than the input stepsize. Since there is an upper bound on the stepsize that can be used to integrate the differential equations in this simulation program, there is the possibility that a stepsize larger than the upper bound will be computed. (Upper bound is approximately 12.5 msec, with the exception of the optical contrast seeker model S2 which has an upper bound of approximately 0.5 msec). Therefore, one should insure that a reasonable stepsize is input and verify that a reasonable stepsize is computed. For example, if the sample period is 16.7 msec, then a stepsize of 8.35 msec or less must be input to insure that the computed stepsize is 12.5 msec or less.

The first assumption results in all of the seeker optics and detector characteristics (such as image resolution, saturation, signal-to-noise, etc.) being ignored. The implications of the third assumption are essentially self-explanatory; the simulated gyro behaves as a perfect gyro (with the exception of the coupling terms and drift). The fourth and fifth assumptions ignore the possibility of lost pulses, attenuation of reflected signals due to atmospheric conditions, designator malfunction, countermeasures, etc. The sixth assumption is not strictly true in a gyro which is processed to follow the line-of-sight. However, the assumption would not be severely violated with a relatively stabilized line-of-sight seeker boresight angle. If the 6 DOF model is to be used to evaluate candidate seekers components (e.g., seekers) however, more precise models may be required.

d. Initialization Subroutine

The seeker initialization subroutine, SII, enters the indices of the elements of the C-array which contain seeker module generated derivatives into successive locations in the IPL array. The IPL-array points the numerical integration logic to the elements of the C-array which are to be numerically integrated. SII initializes the IPL-array with the indices of all potentially utilized seeker related derivatives, despite the fact that the number of derivatives actually used by the seeker module depends upon whether the input values of the variables ω_{SL} and ω_{SN} are zero or positive. The only potentially detrimental effect of this is to cause unnecessary numerical integrations to occur.

SII initializes the cage-uncage switches used in S1 as a function of the setting of the input option switch, OPTN4. Specifically, if $OPTN4 \leq 1$ (signifying that simulation is for direct fire, lock-on before launch), the seeker gyro caging switches are set to the uncaged value (CAGE, TKRY, TKRZ, and TRKZY all equal to 1), reflecting the fact that the gyro is uncaged before direct fire launch. If $OPTN4 > 1$ (an indirect fire mode simulation), the seeker gyro caging switches are set to the cage value, zero.

SII also provides initial values for several Monte Carlo variables including seeker output starting values BY and BZ, seeker starting time ST, seeker pointing error θ_{ERR} and ψ_{ERR} , and seeker drift S_{DY} and S_{DZ} .

e. Random Error Sources

(1) Seeker Pulse Train. The seeker output signal starting time (ST) and initial output value in the pitch (BZ) and yaw (BY) channels are initialized through calls to MCARLO in the seeker initialization module, SII.

The seeker output is a bang-bang signal similar to that shown in Figure 42. Therefore, the absolute magnitude of this signal does not change the probability distribution for the initial value of the seeker signal represents only the probability of the sign of the signal. Thus, initial values of BY and BZ are determined from a distribution according to the sign of the random number.

(2) Seeker Pointing Error. The seeker gimbal yaw angle ψ_G and the seeker gimbal pitch angle θ_G are initialized through calls to MCARLO in the seeker initialization module, SII.

(3) Seeker Drift. Two elements of seeker drift are modeled. They are on-axis and autoerection drift. The equation for these drift elements, in the yaw and pitch channels, are

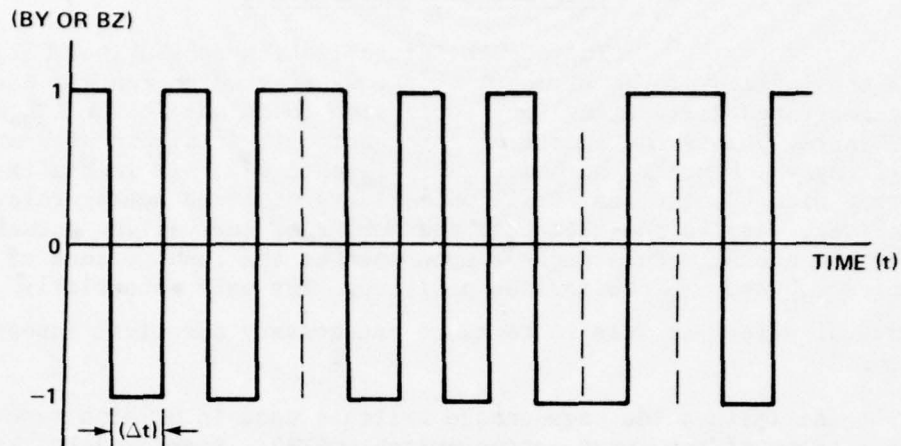


Figure 42. Seeker pulse train.

$$U_{ZK} = S_{\omega} (-\theta_G + 0.1 \psi_G) + S_{DZ}$$

and

$$U_{YK} = S_{\omega} (-\psi_G - 0.1 \theta_G) + S_{DY} ,$$

where

S_{ω} = Autoerection drift coefficient

S_{DY} = On axis drift in yaw

S_{DZ} = On axis drift in pitch.

f. Input/Output Variables and Cross Reference of C-Array

The input/output variables and cross reference of C-array for module S1 are presented in Tables 43, 44, and 45.

g. Monte Carlo Input Variables and Cross Reference of C-Array

The Monte Carlo input variables and cross reference of C-array for module S1 are presented in Table 46.

h. Other Available Seeker Models

Three optional seeker models are available to the Monte Carlo 6 DOF program. They are obtained by dropping the S1

TABLE 43. INPUT FROM DATA CARDS - MODULE S1

Fortran Symbol	Symbol Used in Text	C Index	Definition
RLOCK	RLOCK	445	Maximum quadrant tracker acquisition range (ft)
DT	Δt	446	Laser designator pulse repetition time (sec)
BDB	BDB	447	Tracker deadband (deg) at 10 km
CFOVZ	ϕ_Z	448	Total seeker field-of-view in pitch (deg)
CFOVY	ϕ_V	449	Total seeker field-of-view in yaw (deg)
GSX	G_{SX}	450	Seeker acquisition slew command rate (deg/sec)
SEPS	ϕ	451	Integration shift rate
SWP	S_ω	452	Autoerection drift
GS	G_S	456	Detector output gain (deg/sec)
WSL	ω_{SL}	457	Lead integral compensation zero (rad/sec)
WSN	ω_{SN}	458	Platform compensation pole (rad/sec)
WL2	ω_{L2}	459	Platform compensation zero (rad/sec)

type 2 input card and adding a new type 2 card for the desired seeker model. The three models are listed as follows:

- 1) Optical contrast seeker - S2 module [2].
- 2) Optical contrast seeker, low frequencies only - S3 module [2].
- 3) Digital/linear laser seeker - S4 module [5].

Each of the three modules has a module number to be punched right-adjusted in column 25 of its type 2 card. They are S2-29, S3-30, and S4-31. These numbers control which module is called.

TABLE 44. INPUT FROM OTHER MODULES - MODULE S1

Fortran Symbol	Symbol Used in Text	C Index	Definition
RANGE	RANGE	371	Missile to target slant range (line-of-sight vector magnitude) (ft)
RXBA	X_B	372	X-component of slant range (in body axes) (ft)
RYBA	Y_B	373	Y-component of slant range (in body axes) (ft)
RZBA	Z_B	374	Z-component of slant range (in body axes) (ft)
WP	ω_P	1739	Missile roll rate (in body axes) (deg/sec)
WQ	ω_Q	1737	Missile pitch rate (in body axes) (deg/sec)
WR	ω_R	1747	Missile yaw rate (in body axes) (deg/sec)
SDY	S_{DY}	465	Yaw on axes drift rate (deg/sec)
SDZ	S_{DZ}	466	Pitch on axes drift rate (deg/sec)

TABLE 45. OUTPUTS - MODULE S1

Fortran Symbol	Symbol Used in Text	C Index	Definition
WLAMQ	$\omega_{\lambda Q}$	403	Seeker pitch error signal to autopilot
WLAMR	$\omega_{\lambda R}$	407	Seeker yaw error signal to autopilot
CAGE	CAGE	461	Seeker gyro cage-uncage switch
TKRZ	-	462	Acquisition switch for pitch
TKRY	-	463	Acquisition switch for yaw
TRKZY	-	464	Acquisition switch for autopilot

TABLE 45. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
BY	BY	11	Seeker processor output value in yaw (deg)
BZ	BZ	12	Seeker processor output value in pitch (deg)
BEPSZ	B_Z	435	Boresight angle in pitch (deg)
BEPSY	B_Y	436	Boresight angle in yaw (deg)
WZ	ω_Z	437	Missile body rates in gimbal axes
WY	ω_Y	438	
BCDEFL		439	Total deflection of gimbals
WLQD		408	Seeker state variables
WLZ		411	
WLRD		412	
WLR		415	
WLQDS		416	
WLQS		419	
WLRSD		420	
WLRS		423	
BTHTGD	$\dot{\theta}_G$	424	Pitch gimbal angle rate (deg/sec)
BHTG	θ_G	427	Pitch gimbal angle (deg)
BPSIGD	$\dot{\psi}_G$	428	Yaw gimbal angle rate (deg/sec)
BPSIG	ψ_G	431	Yaw gimbal angle (deg)

Included in Sections III.B.12.i , III.B.12.j , and III.B.12.k are the random error sources, input/output variables, and Monte Carlo input variables for each model. Complete documentation of each seeker model can be found in the references [1-9].

i. Random Error Sources

(1) S2 and S3 Module Optical Contrast Seeker.
Initial condition random error sources specified as probability distributions unique to the optical contrast seeker or impacting the operation of the optical contrast seeker are listed as follows.

TABLE 46. MONTE CARLO INPUT - MODULE S1

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
ST	460	S1I	ST	460	Seeker starting time
BY	11	S1I	BY	11	Seeker output initial value in yaw
BZ	12	S1I	BZ	12	Seeker output initial value in pitch
UYK		S1I	SWP	452	Autoerection drift
UZK		S1I	SWP	452	Autoerection drift
UYK		S1I	SDY	465	On-axis drift
UZK		S1I	SDZ	466	On-axis drift
BTGERR	470	S1I	BTGERR	470	Yaw gimbal angle pointing error
BPGERR	471	S1I	BPGERR	471	Pitch gimbal angle pointing error

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

- a) Seeker platform mass unbalance -
 - (1) Outer gimbal.
 - (2) Inner gimbal.
- b) Seeker rate gyro errors -
 - (1) Drift.
 - (2) Mass unbalance.
 - (3) Output axis/missile roll coupling.
- c) Launch transient rate distributions -
 - (1) Pitch and yaw rate.
 - (2) Roll rate.

(2) S4 Module Digital/Linear Laser Seeker.

Initial condition and time varying error sources specified as probability distributions relating to the digital/linear seeker are as follows:

- a) Seeker drift.
- b) Seeker pulse train.
- c) Laser designator spot jitter.
- d) S/T ratio uncertainties.
- e) Seeker gain variations.

j. Input Variables and Cross-Reference of C-Array

(1) Optical Contrast Seeker, Module S2 and S3

Input Variable Description. Tables 47 and 48 identify all variables of the optical contrast seeker subroutines (S2 and S3) that can be input by 3-cards. Variable names beginning with K are the gains. Variable names beginning with W are the frequency components.

TABLE 47. INPUT FROM DATA CARDS - MODULE S2 AND S3
(OPTICAL CONTRAST SEEKER)

Fortran Symbol	Symbol Used in Text	C Index	Definition
WTQ1		573	Pitch channel frequencies
WTQ2		575	
WQ1		577	
WQ3		581	
WQ4		583	
WQ5		585	
WQ6		587	
WRQ2		591	
WRQ4		595	
WTR1		574	Yaw channel frequencies
WTR2		576	
WGR1		578	
WGR3		582	
WGR4		584	
WGR5		586	
WGR6		588	
WRR2		592	
WRR4		596	
RCL		597	Rate command limit in pitch and yaw
TCLQ		598	Torque command limit in pitch

TABLE 47. (Continued)

Fortran Symbol	Symbol Used in Text	C Index	Definition
TCLR		599	Torque command limit in yaw
JI		565	Moment of inertia of inner gimbal
JO		566	Moment of inertia of outer gimbal
GEOCS		497	Rate gyro gain to autopilot, pitch and yaw
FRI		567	Inner gimbal friction coefficient (in.-oz)
FRO		568	Outer gimbal friction coefficient (in.-oz)
FFOV		604	Blind range decimal percent field-of-view
TARHT		601	Target height (ft)
TARWD		602	Target width (ft)
TAU		600	Seeker sample period (sec)
TLAG		606	Optical contrast seeker transport lag (sec)
KQ1		545	Pitch channel gains
KQ2		547	
KQ3		549	
KQ6		553	
KQ7		555	
KQ8		557	
KQ10		559	
KQ11		561	
KQ12		563	
KR1		546	Pitch channel gains
KR2		548	
KR3		550	
KR5		552	
KR6		554	
KR7		556	
KR8		558	
KR10		560	
KR11		562	
KR12		564	

TABLE 47. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
WPTO		1738	Tipoff roll rate (deg/sec)
AMP2		1742	Peak amplitude of pitch moment forcing function (ft/lb)
AMP1		1746	Peak amplitude of yaw moment forcing function (ft/lb)
VIB		626	Launch transient vibration flag (pitch and yaw only): 0 - no vibration 1 - run with vibration

TABLE 48. INPUT FROM DATA CARDS - MODULE S4
(DIGITAL/LINEAR LASER SEEKER)

Fortran Symbol	Symbol Used in Text	C Index	Definition
DT		446	Laser designator pulse repetition rate (sec)
GS		456	Detector output gain
SEPS		451	
SWP		452	Spring restraining torque constant
WSL		457	Lead integral compensation zero (rad/sec)
WSN		458	Platform compensation pole (rad/sec)
WL2		459	Platform compensation zero (rad/sec)
CROSS		506	Gimbal cross coupling coefficient
BLUR		519	Diameter of laser spot on seeker detector (deg)
CKNULL		523	Proportionality constant of θ null

TABLE 48. (Concluded)

Fortran Symbol	Symbol Used in Text	C Index	Definition
STOTSW		524	Digital to linear switching point
STOTMX		525	Detector output limiter (deg/sec)
RDES		526	Designator range (ft)
HDES		527	Designator altitude (ft)
RVIS		529	Visibility (statute mi)
CPT		530	Target reflectivity
ETHR		531	Threshold energy density at seeker aperture (J/km^2)
EDES		532	Laser designator energy (J)
WCZ		500	Guidance filter natural frequency (rad/sec)
WF		502	
BF		505	
CZETA		507	Guidance filter damping coefficient
SGBIAS		509	Seeker g-bias (deg/sec)
WCN		518	Guidance filter pole (rad/sec)
WCL		510	Guidance filter zero (rad/sec)
SGSTOT		511	Standard deviation of S/T ratio (dB)
GSLIM		539	Seeker output rate limits for linear operation

k. Monte Carlo Input Variables and Cross Reference of C-Array

(1) Optical Contrast Seeker Monte Carlo Input Variables. The variables associated with the Monte Carlo seeker models are given in Table 49. The mean values of these variables are input by 3-cards and the probability distributions are input by 8-cards.

(a) Launch Transient Monte Carlo Input Variables, Optical Contrast Seeker Modules - An 8-card is used to select any one of these models (roll, pitch, or yaw) as a Monte Carlo variable. Roll is the only one of the three that requires specification of a probability distribution on the 8-card. The pitch and yaw models do require 8-cards; however, the probability distribution input fields are left blank because pitch and yaw are randomized indirectly.

A mean value of roll rate (WPT0) is input by 3-card. Mean values of pitch and yaw rate are not input because the mean and distribution of these two variables are determined from solution of the forcing function, $F(t)$ [2]. However, the peak amplitude of pitch (AMP2) and yaw (AMP1) moment (due to helicopter vibration) must be input by 3-card. In addition, the flag, VIB, must be input equal to 1.

(b) Pitch and Yaw Randomization Independent of Launch Transient Model - Pitch and yaw tipoff rates may be randomized from an input probability distribution via the C-indices of pitch and yaw rate on an 8-card. This capability was added as an option to directly randomize as opposed to indirectly randomizing pitch and yaw rates as previously mentioned. Use of this option will generate instantaneous changes in pitch and yaw rate at time of rear shoe rail exit. This option was added primarily to allow randomization of pitch and yaw rates for launch from a tower or ground vehicle in which there are not launcher vibrations. However, this option can be exercised simultaneously with the previously mentioned vibration model. The roll rate randomization previously described applies equally to helicopter or ground launchers.

(2) Digital/Linear Laser Seeker Monte Carlo Inputs. Table 50 presents the digital/linear laser seeker Monte Carlo inputs for module S4.

13. SPOT - Laser Designator Spot Jitter

a. Functional Description

The spot jitter module computes the Y and Z components of the laser designator spot motion (jitter) on the target plane. It also sets up the spot jitter derivatives to be integrated for the next time step.

TABLE 49. MONTE CARLO INPUT - MODULES S2 AND S3
(OPTICAL CONTRAST SEEKER)

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
KUO	611	S2I		611	Outer gimbal mass unbalance (in.-oz/g)
KUI	612	S2I		612	Inner gimbal mass unbalance (in.-oz/g)
KBO	613	S2I		613	Outer gimbal drift rate (deg/sec)
KBI	614	S2I		614	Inner gimbal drift rate (deg/sec)
KOAO	617	S2I		617	Outer gimbal output axis/roll coupling coefficient (sec)
KOAI	618	S2I		618	Inner gimbal output axis/roll coupling coefficient (sec)
WPTO	1738	A3I, A2		1738	Mean tipoff roll rate (deg/sec)
AMP2	1742	A3I, A2		1742	Peak amplitude of pitching moment forcing function (ft/lb)
AMP1	1746	A3I, A2		1746	Peak amplitude of yawing moment forcing function (ft/lb)
WQ	1743	A2		1743	Pitch rate (deg/sec)
WR	1747	A2		1747	Yaw rate (deg/sec)

*MCARLO is flagged by the C-index of this variable in the
calling module.

When MCARLO is flagged by this C-index, a random number will be
returned from MCARLO for the error source in the first column.

TABLE 50. MONTE CARLO INPUT - MODULE S4 (DIGITAL/LINEAR LASER SEEKER)

Program Variable Name of Error Source	Program Module Containing Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
UYK	S4	S4I	SWP	452	Autoerection drift
UZK					
UYK	S4	S4I	SDY	465	On-axis drift
UZK	S4	S4I	SDZ	466	On-axis drift
ST	S4	S4I	ST	460	Seeker starting time
BEPSY	S4	S4I	BEPSY	436	Seeker initial pointing error in yaw
BEPSZ	S4	S4I	BEPSZ	435	Seeker initial pointing error in pitch
GS	S4	S4, S4I	GS	456	Seeker output gain
GSLIM	S4	S4, S4I	SGLIM	539	Seeker output rate limit

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

b. Equations

To simulate designator jitter, white noise is passed through the second order filter shown in Figure 43. The result is a correlated output that closely approximates involuntary human movement. The damping factor, ζ , and the natural frequency, ω_0 , are chosen such that the output of the filter matches that movement. These values are built into the model. The gain G of the filter is selected by the user to control the standard deviation of the output.

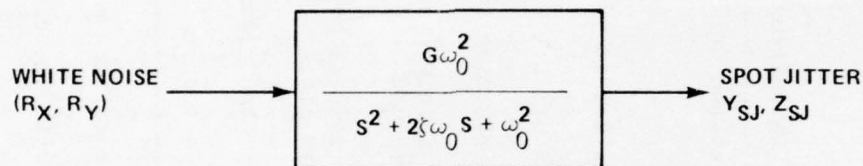


Figure 43. Spot jitter filter.

The spot motion is assumed to be in the target plane as shown in Figure 44 and is composed of two parallel but independently computed components in Y and Z . Two identical filters are used to compute these two components. The output of these two filters at any instant in time is different because a different white noise signal is input to each.

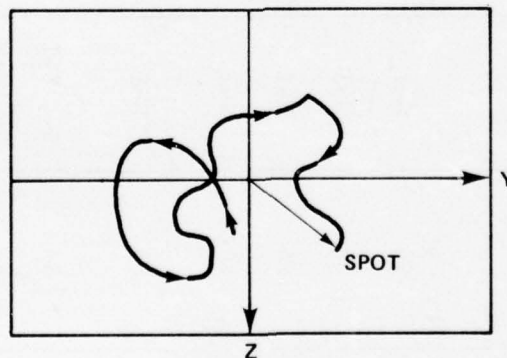


Figure 44. Spot trace in target plane.

The differential equation derived from the transform (Figure 43) to be numerically integrated is

$$\ddot{X} + 2\zeta\omega_0\dot{X} + \omega_0^2 X = \omega_0^2 R_X \quad .$$

The actual spot position Y-component (similarly for Z) is:

$$Y = GX$$

where the gain G is

$$G = 0.707 \frac{\sigma_{\text{SPOT}}}{\sqrt{\frac{\omega_0 \Delta t}{4\zeta}}}$$

The parameters in the previously mentioned equations are

ζ = Damping factor (0.745 data statement in SPOTI)

ω_0 = Natural frequency (3.94 data statement in SPOTI)

R_X = White noise input to Y-component filter

σ_{SPOT} = Expected standard deviation of RSS output of both Y and Z component filters (the 0.707 appears because σ_{SPOT} is the RSS standard deviation)

Δt = Random number calling sequence (normally the integration stepsize)*.

The filter integration constants are all initialized to zero on the first run of a run set. On all subsequent runs of that run set, the filter is not reinitialized, but instead remains charged with the final values that occurred on the preceding run. This means that the time series output is a continuously varying function interrupted by neither reinitialization of all deterministic parameters nor randomization of the stochastic parameters. For example, assume a seven run set in which the flight time of each run is 2 sec. The combined run set flight is then 14 sec. If a plot of the spot jitter were made versus the combined flight time. It would appear as shown in Figure 45. Each 2-sec time slice would represent the spot motion that occurred in each individual run of the run set.

*The statistical properties of the output filter will vary $\pm 10\%$ when the integration step is varied from 0.01 to 0.0125 sec. Therefore, care must be exercised in changing the integration stepsize when performing sensitivity studies.

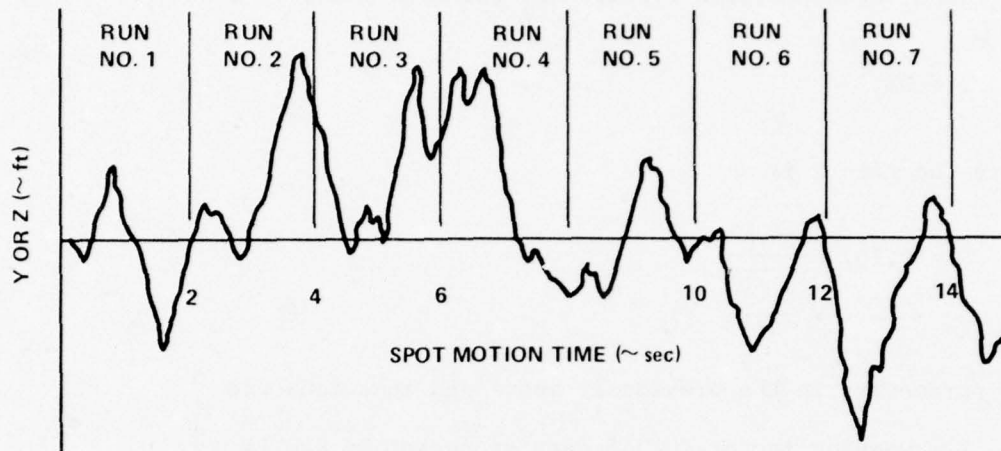


Figure 45. Spot jitter time history.

The reason for handling spot jitter in this manner was to eliminate the transient response of the spot from all runs after the first. The transients die down in approximately 3 to 4 sec. Thought was also given concerning the running of the spot jitter filters for a period of 10 to 15 sec prior to beginning the first run of the set to eliminate the transients from all runs. However, since the minimum spot motion run time for a 25 Monte Carlo run set is approximately 90 sec (3.5 sec per run for a 1-km missile range), the transient response of the filter did not last long enough nor did it appear serious enough to warrant consideration.

A final word about MCARLO and its treatment of spot jitter. This particular error source is handled such that the missile guides on the spot, but calculates miss distance from the target. This was accomplished by adding the spot position to the seeker line-of-sight vector (in G5) so that it guides on the spot.

c. Initialization Subroutine

SPOTI is the initialization subroutine for SPOT. The components of spot jitter (Y_{SJ} , Z_{SJ}) and the spot jitter scale factors (GSPOTY and GSPOTZ) are initialized in SPOTI. Also, the logic to add the spot jitter differential equations to the array (IPL) of the 6 DOF program is contained therein. IPL is the array of variables to be integrated each time step.

d. Random Error Sources

Spot jitter Y and Z components are the only random error sources in SPOT.

e. Input/Output Variables and Cross Reference of the C-Array

Tables 51, 52, and 53 present the input/output variables and cross reference of the C-array for module SPOT.

TABLE 51. INPUT FROM DATA CARDS - MODULE SPOT

Fortran Symbol	Symbol Used in Text	C Index	Definition
SIGSPOT	T_{SPOT}	1581	Expected standard deviation of spot jitter RSS value in Y and Z) (ft)
ZETA	ζ	1579	Spot jitter filter damping rates
WO	ω_0	1580	Spot jitter filter natural frequency (rad/sec)

TABLE 52. INPUT FROM OTHER MODULES - MODULE SPOT

Fortran Symbol	Symbol Used in Text	C Index	Definition
ITNDX		3753	Array of Monte Carlo C-indices input on 8-cards
ITCT		3721	Total number of time series error sources
RX	R_X	1561	White noise input to Y-component filter
RY	R_Y	1571	White noise input to Z-component filter
GSPOTY	G	1562	Spot jitter Y-component scale factor
GSPOTZ	G	1572	Spot jitter Z-component scale factor

f. Monte Carlo Input Variables and Cross-Reference of C-Array

Table 54 presents the Monte Carlo input variables and cross reference of C-array for module SPOT.

TABLE 53. OUTPUT MODULE SPOT

Fortran Symbol	Symbol Used in Text	C Index	Definition
SXPDD	\ddot{X}	1560	Spot jitter differential equation variables
SYPDD	\ddot{Y}	1570	
SXPD	\dot{X}	1563	
SYPD	\dot{Y}	1573	
SXP	X	1566	
SYP	Y	1576	
RSJYMC	$Y_{S\sigma}$	1680	Y-component of spot in target plane (ft)
RSJZMC	$Z_{S\sigma}$	1681	Z-component of spot in target plane (ft)

TABLE 54. MONTE CARLO INPUT - MODULE SPOT

Program Variable Name of Error Source	C Index of Error Source	Program Module Calling MCARLO	MCARLO Flag*		Definition
			Name	Index	
RSJYMC	1680	SPOT SPOTI	RSJYMC	1680	Y-component of spot jitter
RSJZMC	1681	SPOT SPOTI	RSJZMC	1681	Z-component of spot jitter
SIGSPOT	1581				Expected standard deviation of spot jitter. Must be input on type 3 data card

*MCARLO is flagged by the C-index of this variable in the calling module.

When MCARLO is flagged by this C-index, a random number will be returned from MCARLO for the error source in the first column.

C. MCARLO-Monte Carlo Control Subroutine

1. Introduction

A Monte Carlo approach was developed for generating CEP related information for the THAD program. This approach consists of executing a specified number of runs* using the MICOM 6 DOF simulation program, where both initialization error conditions and time varying error conditions for each simulation run will be randomly generated from input error probability distributions. The resulting miss distance coordinates from each run are then subjected to an automated statistical analysis using the CEP Analysis System (CEPAS) program, Section III. D to obtain CEP information.

The composite simulation tool that evolved from the Monte Carlo approach is a stochastic 6 DOF model consisting of the MICOM 6 DOF deterministic simulation program, a Monte Carlo control subroutine (MCARLO), and the CEPAS program.

Statistical data are input on distinct data card types (type 8 cards). In the absence of statistical data inputs, the operation of the 6 DOF program reverts to that of the deterministic version of the program.

The Monte Carlo approach takes advantage of the dual mode operation of the 6 DOF program. The initialization modules call MCARLO to randomize all initial condition error sources. Then in the flight execution module, MCARLO is called to generate time series random conditions.

2. Monte Carlo Control Subroutine - MCARLO

The Monte Carlo control subroutine MCARLO is structured according to error source type and error source probability distribution. There are two error source types. They are initial condition error sources and time varying error sources. There are three error source distributions. They are normal, uniform, and correlated normal. The error source distributions are subcategories of both error source types as shown in Figure 46 with the one exception of correlated normal which is unique to time series error sources.

If no stochastic input data cards are read on input, the local error source logic which calls MCARLO (necessarily located at the point of application of the error source in the 6 DOF program) is step up so that the call is not executed.

*A run is defined as the numerical integration of a missile trajectory from launch to target plane intercept.

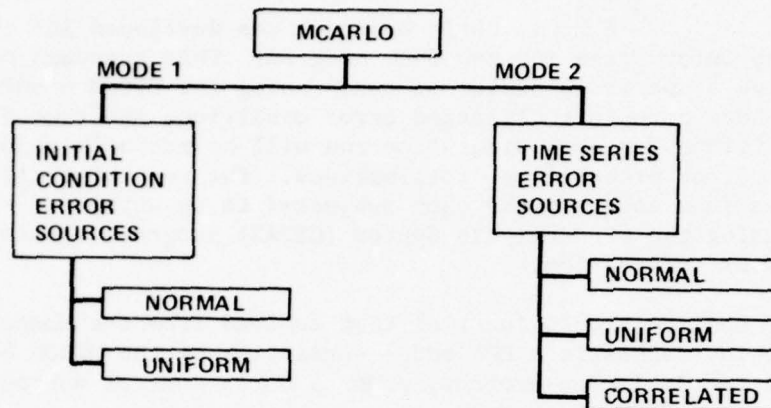


Figure 46. MCARLO structure.

3. MCARLO Operational Modes

Subroutine MCARLO has four modes of operation. The mode to exercise depends upon the location in the 6 DOF program from which MCARLO is called and the type of error source. The mode is identified by number in the argument list of the MCARLO call statement, i.e.,

MCARLO (RNSTRT, MODE, ITSNDX) .

- a. MODE = -1. Initial Condition Heading Print Mode

MCARLO is called from MAIN to write the following heading and column names at the start of each run initialization:

MONTE CARLO INITIAL CONDITIONS					
C-INDEX	MC-VALUE	MEAN	DISTRIBUTION	LOWER BOUND	UPPER BOUND

- b. MODE = 1. Initial Condition Error Source Mode

MCARLO is called from an initialization module under this mode. This mode flags MCARLO to randomize an initial condition error source from a user specified probability distribution. Mode 1 also provides for the storage of user input error source mean values on the first run of a run set. This allows the mean of the error source to remain fixed for all subsequent runs. Thus, all Monte Carlo values for a given error source will be about the original mean values for all runs of the run set.

c. MODE = 2. Time Series Mode

MCARLO is called from the flight simulation modules under this mode. Mode 2 flags MCARLO to generate random numbers for a time series error source based on user specified sample intervals* and probability distributions. The sample intervals can range from a lower bound of the integration stepsize to an upper bound of the flight time itself. The sampling can be pure periodic or random normally distributed with user control over both the periodic mean and standard deviation. (Protective logic is included to ensure that the period always advances but never advances beyond twice the mean of the period.) When MCARLO is called by mode 2, it first checks the flight time against the next time series sample time. If the sample time has been reached, it sets up the next sample time (either periodic or random, as determined by input option), and generates a new random value for the error source, then returns control to the calling routine. This procedure is repeated for each time series error source at each integration step.

d. Mode = 4. Time Series Initialization Mode

MCARLO is called from the initialization modules under a mode 4 to initialize the following pertinent time series error source parameters in MCARLO:

- 1) Reset the time series sampling time (TNXST) to zero at the start of each new run.
- 2) Save the time series error source means for normally and uniformly distributed error sources.
- 3) Initialize the time series error source variables associated with correlated normal output.

4. MCARLO Error Probability Distribution

Subroutine MCARLO has three error source probability distributions. The distribution to use depends upon user specified input data. Each distribution is identified by number in the following manner:

- 0 - Normal distribution
- 1 - Uniform distribution
- 2 }
3 } Correlated normal distribution*.
4 }

*Each of the three different numbers in the correlated normal distribution category identifies a specific parameter in the 6 DOF program that is a correlated random variable. More information on this in the input section.

a. Normal Distribution

Normally distributed error source values are picked from the system library random number generator based on user specified normal distribution parameter values indicated in Figure 47.

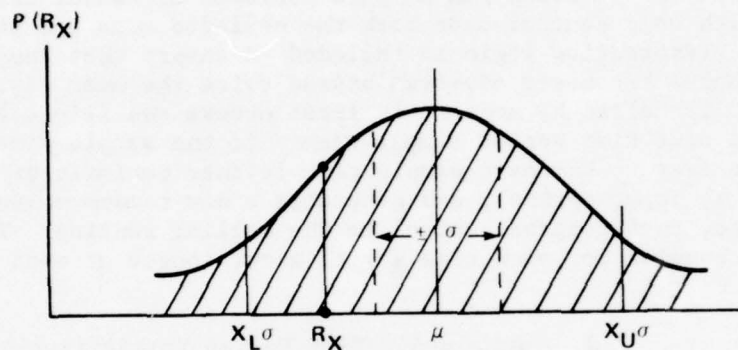


Figure 47. Normally distributed error source.

The distribution parameters, mean (μ), standard deviation (σ), and cutoff values (σX_L and σX_U) are specified on input data cards. The limits (X_L and X_U) are multiples of the standard deviation (σ). For instance, assume a standard deviation of 2 ft, a mean of 0, and limits of ± 6 ft; the input values of X_L and X_U would be

$$X_L = -3$$

and

$$X_U = 3$$

b. Uniform Distribution

Uniform distributed error source values are picked from the system library random number generator based upon user specified uniform distribution parameter values indicated in Figure 48. The input format for a uniformly distributed error source is identical to that for a normally distributed error source so that the standard deviation for a uniformly distributed error source would be utilized in a manner analogous to its interpretation for a normally distributed error source.

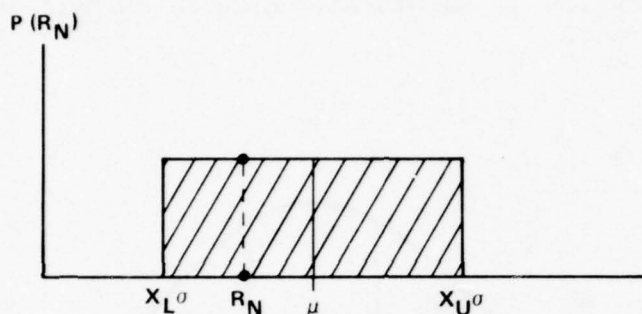


Figure 48. Uniformly distributed error source.

The random number, R_N , returned by MCARLO is computed from the following equation where R_X is the random number generated by the system library random number generator from the distribution shown in Figure 49.

$$R_N = \mu + (R_X(X_U - X_L) + X_L)\sigma$$

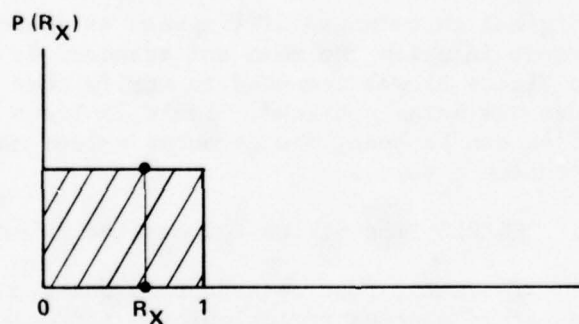


Figure 49. System library random number distribution.

c. Correlated Normal Distribution

The correlated normal distribution involves the generation of digital white noise to be used as the forcing function in an n th order filter to produce a random but correlated output. An example of n th order filters used in the Monte Carlo program is given in Section III. B. 13. The digital white noise is produced by calling the system library normally distributed random number generator.

The distribution parameter values shown in Figure 47 used to produce the white noise is given in Figure 50. The output from the digital white noise generator is sampled and held with the hold period (NAT) specified by input.

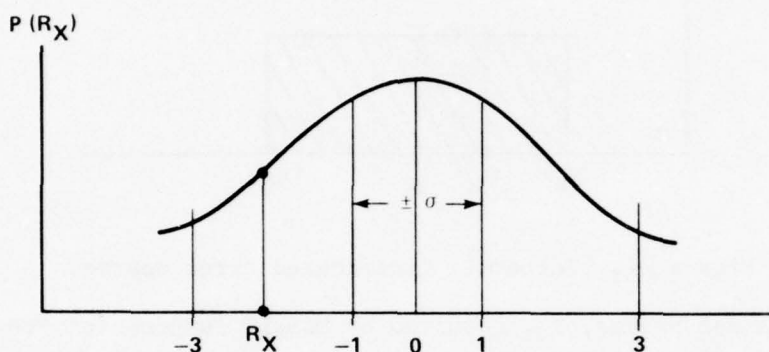


Figure 50. Expected digital white noise distribution.

The random number generator is called only at the beginning of an integration step; therefore, the calling frequency must be input as multiples of the 6 DOF program integration stepsize. No random numbers are generated during the intermediate Runge-Kutta passes.

The output digital white noise will appear as shown in Figure 51. Sample runs were made in which the mean and standard deviation of an output similar to Figure 51 was computed to verify that something near the expected values was being obtained. Table 55 lists the results of this sample run. As can be seen, the computed values match very closely with the expected values.

5. MCARLO Time Series Output Statistical Information

The mean, root mean square, and standard deviation of all time series error sources are calculated for each run of a run set and printed out at the end of each run. A sample of this printed output is given in the following listing:

<u>C-Index</u>	<u>Mean</u>	<u>Variance</u>	<u>Standard Deviation</u>	<u>RMS</u>
1688	0.311	0.415	0.644	0.715
1681	0.219	0.217	0.465	0.514
70	20.814	18.960	4.354	21.265

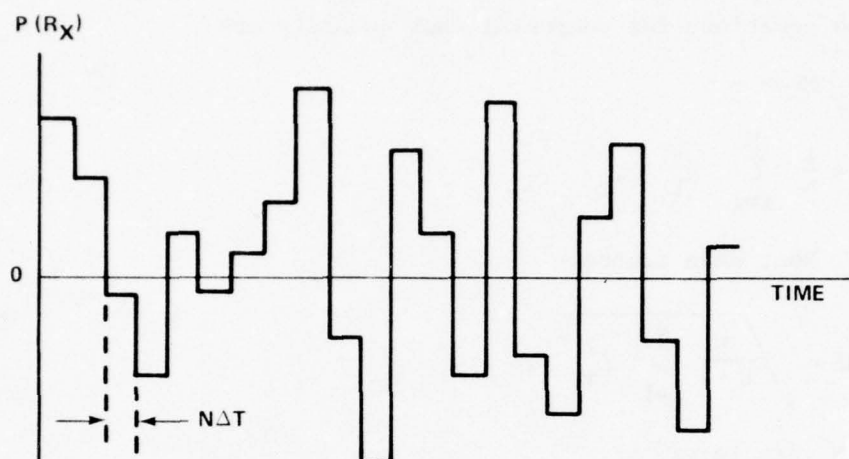


Figure 51. Digital white noise.

TABLE 55. WHITE NOISE MEAN AND STANDARD DEVIATION

NBR Points	Mean	Standard Deviation
4	0.33906	1.05079
8	0.12430	0.94270
12	0.32426	0.97609
16	0.18078	0.92107
20	0.06838	1.07162
24	0.03911	1.01745
28	0.11203	1.02958
32	0.12258	0.99166
36	0.18264	0.97269
40	0.13704	0.96311
44	0.01243	1.02618
48	0.06378	1.04694
52	0.00576	1.06904
56	0.02060	1.03755
60	0.04752	1.01945
64	0.07061	1.07774
68	0.03115	1.08620
72	0.05118	1.07271
76	0.07003	1.05797
80	0.08658	1.08227
84	0.07411	1.05841
88	0.08188	1.04525

The equations for computing each quantity are

a) Mean -

$$\mu = \frac{1}{N} \sum_{i=1}^N X_i .$$

b) Root mean square -

$$RMS = \sqrt{\frac{1}{N-1} \sum_{i=1}^N X_i^2} .$$

or for N very large,

$$RMS = \sqrt{\frac{1}{N} \sum_{i=1}^N X_i^2} .$$

c) Standard Deviation

$$\sigma = \sqrt{RMS^2 - \mu^2} .$$

6. Addition of New Error Source Models

The addition of new error source models to the 6 DOF program is described in the following paragraphs. The procedure required depends upon whether the error is an initial condition error source or a time series error source. In addition, the complexity of time series error source addition depends upon whether the probability distribution of the time series error source is normal, uniform, or correlated normal. The correlated normal time series error source is the more complex model because it involves filtered white noise.

a. Initial Condition Error Sources

Initial condition error modeling will always appear in one of the initialization modules. The module in which the source is modeled depends upon the point of application of the error source in the missile system. For example, an error source associated with the seeker will logically be modeled in the seeker initialization module, SLI. When the Monte Carlo variables have been identified, the following DO LOOP is established with the C-index of the Monte Carlo variable used to flag MCARLO:

```
C MONTE CARLO STEADY STATE WIND COMPONENT
DO 500 I = 1, 13512
  IDO = 1
  IF (ISNOX(I),EQ.51) CALL MCARLO (OUM, 1, IDO)
  IF (ISNOX(I),EQ.52) CALL MCARLO (OUM, 1, IDO)
500 CONTINUE
```

The DO LOOP variables are ~~defined~~ as:

13512 - total number of initial condition error source type 8 cards that are read in OINPT1.

ISNDX(I) - The Monte Carlo variable C-index that appears in the Ith type 8 card.

This DO LOOP checks all the initial condition error sources type 8 cards to determine if any of the type 8 cards contained the C-index number in the IF statement. If an 8-card does contain a C-index (ISNDX) equal to the number, then MCARLO is called to randomly select a value for the variable that has that C-index. The argument list of MCARLO contains a dummy variable DUM, the type of MODE (1 for initial conditions), and the type 8 card number (IDO) that contains the statistical information for the error source.

b. Time Series Error Sources

Time series error modeling will appear in both an initialization module and in a flight simulation module. The initialization module performs all initialization required for that model (MCARLO MODE = 4) and the flight simulation module calls MCARLO to generate the time series random number sequence for the model (MCARLO MODE = 2).

The DO LOOP example that follows was developed for the wind gust model. Initialization is performed in module G2I, while the time series random number generation is performed in the wind module G2.

1) Time series initialization - G2I -

```
C MONTE CARLO INITIAL VALUE OF TIME SERIES WIND GUSTS
DO 501 I = 1,ITCI
  IDO = I
  IF(IISNDX(I).NE.70) GO TO 501
  CALL MCARLO ( DUM,4,IDO)
  WNDWC = 1.
  IF(VWTE.EQ.0.) GO TO 505
  SIGU = VWTE/2.9
  GO TO 506
505 CONTINUE
  VWTE = 2.9 * SIGU
506 CONTINUE
  SSIGU = SIGU*SQRT(1.69/D(2664))
  BLU = -12.1*SIGU + 475.
  IF(VWTEH/VWTE.GT..1) WNDWC = VWTE/VWTEH
  IPL(N) = 59
  N = N + 1
501 CONTINUE
```


2) Time series random number generation - G2 -

```

      ICK = 0
      DO 500 IOL = 1, ITCT
      ITSNDX = IOL
C
C  MONTE CARLO WIND GUSTS TIME SERIES
      IF (ITNDX(IOL).NE.70) GO TO 502
      UBAR = 0.
      IF (VWTE.NE.0.) UBAR = ABS((VXE*VHXE + VYE*VHYE + VZE*VHZE)/VWTE)
      CALL MCARLO(DUM, 2, ITSNDX)
      WNDWC2 = UBAR/BLU + WND4J
      GLW = CSIGU*SQRT(WNDWC2)
      SLWD = RLW - WNDWC2*SLW
      GVWTE = VWTE + GLW*SLW
      ICK = 1
502 CONTINUE
500 CONTINUE

```

The DO LOOP variables are defined as:

ITCT - total number of time series error source type 8 cards read in OINPT1.

ITNDX(I) - the Monte Carlo variable C-index that appears on the Ith type 8 card.

These two DO LOOPS check all the time series error source type 8 cards to determine if any of the type 8 cards contained the C-index number in the IF statement. If an 8-card does contain a C-index (INTDX) equal to the number, then all the calculations and MCARLO calls relating to that model are performed. The argument list of MCARLO in the initialization modules contains a dummy variable DUM, the type of MODE (4 for initialization), and the type 8 card number (IDO) that identifies the Monte Carlo time series variable. The argument list of MCARLO in the flight simulation module contains a dummy variable, DUM, the type of MODE (2), and the type 8 card number (ITSNDX) that identifies the Monte Carlo time series variable.

Other information and calculations are also contained within the DO LOOPS. The specific information and calculations that appear depends upon the model. The time series model given here is a correlated normally distributed model that involves filtered white noise. This involves setting up several auxiliary calculations for the integration of the differential equation inside the MCARLO MODE 2 DO LOOP.

c. Input/Output Variables and Cross Reference of C-Array

Tables 56, 57, and 58 present the input/output variables and cross reference of C-array for MCARLO.

TABLE 56. INPUT FROM DATA CARD - MCARLO

Fortran Symbol	Symbol Used in Text	C Index	Definition
RNSTRT	R_N	3511	Random number generator starting value (seed) - must be an odd octal whole number
IDIST		3674	Type of distribution of initial condition error source
SIGMA	σ	3514	Initial condition error source standard deviation
SIGLB	σ_{X_L}	3554	Initial condition error source lower bound
SGGUB	σ_{X_U}	3594	Initial condition error source upper bound
ITDIST		3763	Type of distribution of time series error source
TSPER		3773	Time series sample period of periodic sample rate or mean of sample period if random sample rate
TSGMA	σ	3723	Time series error source standard deviation
TLB	σ_{X_L}	3733	Time series error source lower bound
TUB	σ_{X_U}	3743	Time series error source upper bound

NOTE: All of these inputs, with the exception of RNSTRT, are read in on 8-cards. Each variable has a unique field assigned to on the 8-card. See Section IV. A. 8 for definition of these fields. RNSTRT is read in on a 3-card.

TABLE 57. INPUT FROM OTHER SUBROUTINES - MCARLO

Fortran Symbol	Symbol Used in Text	C Index	Definition
ISNDX	ISNDX	3634	Array of Monte Carlo. Variable C-indices appearing on 8-cards (initial condition error sources)
ISGCT	13512	3512	Total number of initial condition error sources for this run
ITNDX	ITNDX	3753	Array of time series Monte Carlo error sources C-indices appearing on 8-cards
ITCT	ITCT	3721	Total number of time series error sources for this run
TYPPEP		3783	Flag for time series values, = 0 stochastic = 1 deterministic
TPSIG	σ	3793	Array of time series error source standard deviation
TNXST	TNSST	3803	Time series sampling time; reset each run
ITNDX2		3813	C-indices of time series error sources

TABLE 58. OUTPUT - MCARLO

Fortran Symbol	Symbol Used in Text	C Index	Definition
TMU	u	2805	Calculated mean value of the time series output
TVM		2815	Variance of the time series output
TSIG	σ	2825	Standard deviation of the time series output
TRMS	RMS	2795	RMS of the time series output
YMC		1564	Current Y mean value
YMC2		1565	Current Y mean squared
ZMC		1574	Current Z mean value
ZMC2		1575	Current Z mean squared

D. CIRCULAR ERROR PROBABILITY ANALYSIS SYSTEM

1. Functional Description

CEPAS consists of a distinct set of subroutines that interfaces the 6 DOF program through a control subroutine named CEPAS. Subroutine CEPAS accepts miss distance coordinates from the 6 DOF program after the completion of a run set and automatically generates CEP related information. Through the use of a control parameter input card, user control can be exercised over both the assumptions of the analysis and the output information. This control parameter card is read in by the 6 DOF input subroutine OINPT1 following all 6 DOD/Monte Carlo input data. Detailed input information concerning this control parameter card is given in the input description section of this report, Section III. D. 8.

2. Related Subroutines

The set of subroutines in the stochastic 6 DOF simulation program that are unique to CEP calculations are:

- a) CEPAS - CEP analysis system control subroutine.
- b) CEPP - CEP calculation subroutine.
- c) KSTEST - Kolmogorov-Smirnov (K-S) test subroutine.
- d) ZTABLE - Table of areas of the normal probability curve.
- e) PPLOT - Printer plot subroutine.
- f) XLOC - Auxiliary routine for locating X coordinate for use in PPLOT.
- g) NORM - Calculates normalized random value.
- h) RANNUM - Uniformly distributed random number generator.
- i) NORMAL - Normal (Gaussian) distributed random number.

A list of the variables appearing as arguments to these subroutines is contained in Section III.

3. Assumptions

The CEP calculations made by CEPAS are obtained by either parametric statistical methods, assuming an elliptical bivariate normal distribution, or by nonparametric methods, where no specific distribution is assumed. Because more information can generally be obtained (e.g., confidence circles) from a given size sample when the distribution is known, it is advantageous to use the parametric methods when they apply. For this reason, CEPAS automatically subjects the input miss distance data to a normality test (a K-S test is used [6,7]) to determine whether to use the parametric or nonparametric methods. If the hypothesis of normally distributed data is not rejected by the K-S

test, the parametric method is used; otherwise, the nonparametric method is used. A user option is available which causes the parametric calculations to be used regardless of the outcome of the K-S test. If this option is utilized, however, and the actual underlying population of miss distance coordinates is significantly non-normal, the resulting CEP information will be unreliable.

The a priori selection of an elliptical bivariate normal distribution is justified in part by the fact that the assumption has yielded satisfactory results for a large number of past systems [4]. If subsequent data obtained from Monte Carlo simulation runs shows that the assumption of a bivariate normal distribution is not justified, the use of other distributions can be considered.

Given that the missile impact points are elliptical bivariate normally distributed, the miss distance statistics could meaningfully be summarized using at least two obvious approaches. One approach would be to calculate an estimate of the parameters of an ellipse containing a given fractional part of the population of impact points. The fractional part would then be interpreted as the probability of a future shot having an impact point within the ellipse. Since the ellipse parameters would be estimates of the true population parameters, based upon the sample points, a confidence ellipse with a specified probability of containing the population ellipse could be defined. An alternative approach would be to convert the elliptical parameters to equivalent CEP parameters. The latter approach was actually taken in CEPAS for two primary reasons: (a) ellipses generated with different system components (e.g., seekers, autopilots, etc.) are difficult to compare when attempting to determine the component exhibiting the most satisfactory performance, and (b) CEP has traditionally been used for representing planar miss distance statistics, with the consequence that the results are more readily recognized by missile system engineers. The conversion from elliptical parameters to equivalent CEP parameters is accomplished utilizing a transformation developed by Stanford Research Institute [8]. It should be noted that even when the underlying population of miss distance coordinates is actually distributed as assumed, at least two factors will prevent any given CEP circle from containing 50% of the sample impact point. The first factor is that even if the CEP of the missile system was known exactly, data sampling fluctuations would generally prevent precisely 50% of the impact points from being within the given CEP circle. The second factor is that the population parameters are, in fact, not known, but must be estimated based upon the sample data itself.

Regardless of whether the CEP calculations are parametrically or nonparametrically based, the CEP circle center is taken to be the centroid of the sample miss distance coordinates.

The calculation of the CEP and confidence circle radii, for the parametric case, is discussed in Section III. D. 7. No confidence circle is calculated in the nonparametric case. The CEP radius in the nonparametric case is assumed to be such that as many points lie inside the circle as outside. The only occasions where this cannot be done are the very infrequently occurring ones where more than one impact point lies exactly on the CEP circle circumference, and the number of remaining points is odd. In this case, the number of points inside and outside the circle will differ by one.

4. 6 DOF Simulation System Compensation

When CEP calculations are parametrically based, additional CEP information can be optionally obtained from CEPAS, using the supposition that the 6 DOF program does not precisely represent the actual missile system. The deviation of the 6 DOF program from the actual system performance in terms of miss distance coordinates would only be approached by comparing results of a large number of test firings with simulations of such test firings. Since such an approach is economically impractical, the simplifying assumption has been made that the 6 DOF simulator represents an impact point measuring system having a CEP equal to $\lambda(\lambda \geq 0)$ times the CEP of the missile system, where λ is an input parameter. This assumption appears justified in part by the fact that if a firing was made, and an analogous (same conditions simulated 6 DOF) simulation run made, then the actual and the simulated impact points could be expected to differ by some amount. Further, if a large number of such comparisons were made, some distribution of the differences would be expected (ignoring bias errors). In this sense, the 6 DOF simulator can be considered a measuring system of the actual missile system impact points. The mathematical formulas utilized in CEPAS were derived under the assumption that a measuring system utilized to record the position of actual impact points would yield different position data each time the same impact point is measured. (This fact is due to the inherent imprecisions in the measuring system.) While it is recognized that this is not strictly the sense upon which the formulas are being utilized in CEPAS (with $\lambda > 0$), it is felt that a close analogy exists between the 6 DOF simulation program and a measuring system.

In normal operation, CEPAS defaults to $\lambda = 0$, and the resulting CEP information can be interpreted as a prediction of the missile system CEP, based on the assumption that the impact points predicted by the 6 DOF program exhibit no dispersion about actual impact points.

When λ is input greater than zero, two sets of CEP information are calculated by CEPAS. The $\lambda = 0$ case is calculated for reference, and a second set of CEP information is calculated under the assumption that the 6 DOF program exhibits a CEP about a single actual impact point of λ times the CEP of the missile system. The equations used in the CEP calculations for $\lambda > 0$ are discussed in Section III. D. 7.

5. Confidence Circles

The CEP parameters (centroid and radius) of the miss distance population are estimated in CEPAS using sample data, and are consequently subject to the usual estimation errors. In order to bound these errors with a specified probability, a user option permits inputting any combination of five confidence levels (99%, 95%, 90%, 80%, and 70%). The selection of a given confidence level will result in CEPAS computing a circle of radius R within which the actual missile system CEP is assumed to be located. The validity of this calculation depends upon the fidelity of the 6 DOF simulation program and the data points being bivariate normally distributed. For each confidence level selected, CEPAS will calculate and display the confidence circle. Confidence circles are not calculated if the CEP is calculated nonparametrically (Section III. D. 3.), i.e., if the data are not bivariate normally distributed.

6. Printer Plots

Printer plots of the CEP circle, the confidence circle (if generated), and the input miss distance points can be generated as a user option. If the user has input a value of λ greater than zero (Section III. D. 4.), then two plots will be generated for each confidence level entered by the user; one plot will display the CEP and confidence circles for $\lambda = 0$, and the other will display the same information for the input values of λ .

Samples of the printer plots are included in Section IV. B. 3.

7. Equations

The equations used for calculating CEP and confidence circles are included below.

The Chi-square, normal, and critical K-S tables required for computations are loaded in various programs arrays.

a. Sample Estimate of Standard Deviations in Y and Z.

$$\text{Azimuth: } S_Y^2 = \frac{1}{N-1} \left[\sum_{i=1}^N Y_i^2 - \frac{1}{N} \left(\sum_{i=1}^N Y_i \right)^2 \right]$$

$$\text{Deviation: } S_Z^2 = \frac{1}{N-1} \left[\sum_{i=1}^N Z_i^2 - \frac{1}{N} \left(\sum_{i=1}^N Z_i \right)^2 \right]$$

where (Y_i, Z_i) denotes ith set of input miss distance coordinates and N denotes number input coordinate pairs.

b. CEP and Confidence Circle Centroid

Sample estimate of CEP and confidence circle centroid is (\bar{Y}, \bar{Z}) , where

$$\bar{Y} = \frac{1}{N} \sum_{i=1}^N Y_i$$

$$\bar{Z} = \frac{1}{N} \sum_{i=1}^N Z_i .$$

c. Determination of CEP and Confidence Circle for $\lambda = 0$

The calculation of the missile system CEP and confidence circle radii for $\lambda = 0$ (i.e., assuming no measuring system CEP) is performed as follows:

$$\text{Let } S_{\text{MIN}}^2 = \text{Minimum } [S_Y^2, S_Z^2]$$

$$S_{\text{MAX}}^2 = \text{Maximum } [S_Y^2, S_Z^2] ,$$

then for

$$\frac{S_{\text{MIN}}}{S_{\text{MAX}}} \geq 0.3, \text{ CEP}_J = 0.615 S_{\text{MIN}} + 0.562 S_{\text{MAX}}$$

and

$$\begin{aligned} \frac{S_{\text{MIN}}}{S_{\text{MAX}}} < 0.3, \text{ CEP}_J = 0.9988 \left(\frac{S_{\text{MIN}}^2}{S_{\text{MAX}}^2} \right) - (0.0496) S_{\text{MIN}} , \\ + (0.675) S_{\text{MAX}} \end{aligned}$$

where CEP_J represents the CEP radius calculated on the assumption that $\lambda = 0$, (6 DOF program impact points exhibits no dispersion about actual impact points). The confidence circle radius, R_J , is calculated from

$$R_J = \sqrt{\frac{2(N-1)}{X_{0,P}^2}} \text{ CEP}_J ,$$

where N is the number of data points, ν is the degrees of freedom ($\nu = 2(N-1)$ in this case), and P is one of the confidence levels requested by the user. Chi-square (χ^2) values are tabulated by degrees of freedom and confidence level.

d. Determination of CEP and Confidence Circle for $\lambda > 0$

If $\lambda > 0$ then the following formulas are utilized by CEPAS:

$$CEP_S = \frac{CEP_J}{\sqrt{1 + \lambda^2}}$$

$$R_S = \frac{R_J}{\sqrt{1 + \lambda^2 - \frac{\lambda^2 \chi^2_{\nu, P}}{2(N-1)}}}$$

where CEP_S and R_S are the CEP and confidence circle radii with the effect due to the assumed dispersion of the measuring system removed.

8. Input Description and Variables

The input format for CEPAS control parameter data card is given in Section IV. A. 9.

(Note): The CEP calculations made by CEPAS are obtained by either parametric statistical methods, assuming an elliptical bivariate normal distribution, or by nonparametric methods, where no specific distribution is assumed. Because more information congenially be obtained (e.g., confidence circles) from a given size sample when the distribution is known, it is advantageous to use the parametric methods when they apply. For this reason, CEPAS automatically subjects the input miss distance data to a normality test (a K-S test is used) to determine whether to use the parametric or nonparametric methods. If the hypothesis of normally distributed data is not rejected by the K-S test, the parametric method is used; otherwise, the nonparametric method is used. A user option is available which causes the parametric calculations to be used regardless of the outcome of the K-S test. If this option is utilized, however, and the actual underlying population of miss distance coordinates is significantly non-normal, the resulting CEP information will be unreliable.)

Table 59 contains a list of variables as they appear in the argument lists of the various CEPAS subroutines.

E. Executive Subroutines

1. Module Initialization Executive Subroutine (AUXI)

The module initialization subroutines are called by subroutine AUXI according to the input module data control cards (type 2 input data cards - see Section IV for input card formats).^{*} AUXI is called by the MAIN program after the input subroutine, OINPT1, is called, and prior to entering the integration loop. AUXI contains calls to a number of initialization subroutines which exist only as nonfunctional entry points in the subroutine DUMMY. Thus, for example, AUXI calls A2I, which by the naming convention would correspond to the initialization subroutine for the forces and moments module, A2. However, no subroutine A2I exists, which results in the compiler accessing the entry point A2I in DUMMY, which simply returns control back to AUXI.

Table 60 shows the functional module initialization subroutines, along with the module number which initiates the subroutine call in AUXI.

2. Module Executive Subroutine (AUXSUB)

Subroutine AUXSUB is an executive routine which calls the modules input on type 2 data cards in the order of input (see Section IV for input data card format). AUXSUB is called by the MAIN program. It is in the integration loop, and consequently, is called by MAIN at every integration step. AUXSUB contains calls to modules that exist only as nonfunctional entry points in subroutine DUMMY.

Table 61 lists the existing modules and their associated module numbers which, when input on type 2 data cards, cause AUXSUB to call the modules in input order.

3. SUBL1 - Executive Subroutines

This executive subroutine is functionally inactive. It is called by MAIN, and in turn calls INPT1, OUP11, STGE1, CNTR1, RNDM1, AUXAL, AUXB1, and AUXCL, depending upon the subroutine numbers stored in the array, SUBNO (I). However, all of the subroutine names called (INPT1, OUP11, etc.) exist only as entry points in subroutine DUMMY.

^{*}AUXI will automatically call an initialization subroutine for each module specified on a type 2 input card; i.e., no input cards are required for initialization subroutines.

TABLE 59. CEPAS SUBROUTINE ARGUMENT VARIABLES

Fortran Symbol	Symbol Used in Text	C Index	Definition
NP		CEPAS, CEPP KSTEST, PLOT	Number of points
IBVNSW		CEPAS, CEPP	<p>= 1, if desire to use bivariate normal assumption regardless of outcome of K-S test</p> <p>≠ 1, if to use bivariate normal only if K-S test does not reject assumption of normality</p> <p>If #1 and data fails K-S test for normality, CEP will be calculated as the radius, R, of a circle containing 1/2 of the sample points</p>
IPLOT		CEPAS CEPP	= 1, for plots of CEP(s) and points, otherwise, ≠ 1.
XLAMBD		CEPAS CEPP PLOT	(Program CEP)/(Missile CEP), = 0, if no estimate of program CEP is made
KSSIG		CEPAS CEPP KSTEST	Significance level for K-S test desired, negative if not K-S test desired
CEPSIG		CEPAS CEPP	Confidence level (CEPSIG(1) = 90, CEPSIG(2) = 99, CEPSIG(3) = 70, etc.)
PSIZE		CEPAS CEPP PLOT	Plot size of Y-axis (for scaling), if = 0, PLOT scales itself
X		CEPP PLOT	Array of X-component of miss distances
Y		CEPP PLOT	Array of Y-component of miss distances
RX		NORM	Monte Carlo value of normally distributed error source

TABLE 59. (Continued)

Fortran Symbol	Symbol Used in Text	C Index	Definition
XL		NORM	Lower bound of time series, error source
XU		NORM	Upper bound of time series, error source
XMU		NORM	Mean of time series error source
SGMA		NORM	Standard deviation of time series error source
RNSTRT		NORM	Random number generator starting value
XBAR		KSTEST	Not used in KSTEST
		PLOT	X-coordinate of CEP centroid
SXHAT		KSTEST	Not used
NI		KSTEST	K-S test failure flag, = 1 fails.
Z		ZTABLE	Standardized random variable
FREQ		ZTABLE	Accumulative probability
NZT		ZTABLE	Not used
CEP		PLOT	CEP
ICHI		PLOT	Input confidence level
RCONF		PLOT	Radius of the ICHI referenced confidence circle
TITLE		PLOT	Alphanumeric titles for output purposes
YBAR		PLOT	Y-coordinate of CEP centroid
XVAL		XLOC	Input value of X-coordinate
HSPRD		XLOC	X-axis scale factor
IWD } INDX }		XLOC	Indexes used in determining X-coordinate location

4. SUBL2 - Executive Subroutine

a. Functional Description

Executive subroutine, SUBL2, is called by MAIN immediately after the module initialization subroutine, AUX1, is called. SUBL2, in turn, calls INPT2, OUP2, STGE2, CNTR2, RNDM2, AUX2, AUXB2, and AUXC2, depending upon the subroutine numbers stored in the array, SUBNO(I)*. The array, SUBNO(I), is initialized in OINPT1, by the subroutine numbers entered on type 1 input data cards, with the current

configuration of the simulation program, two type 1 cards are input to enter subroutine numbers 3 and 4 into the SUBNO(I) array. This will cause subroutines OUP2 and STGE3 (described in Sections III. G. 2 and 3. F. 11 *, respectively) to be called by SUBL2.

Table 60. Module Initialization Subroutine Numbers

Name	Function	Subroutine Number
ALI*	AERO coefficient module initialization	2
A3I	Engine module initialization	4
SPOTI	Spot jitter module initialization	38
C1I	Autopilot module initialization	7
C4I	Actuator initialization	10
D1I	Translational dynamics module initialization	17
D2I	Rotational dynamics module initialization	18
S1I	Seeker module initialization	28

*ALI is an entry point in C4I.

TABLE 61. MODULES AND ASSOCIATED MODULE NUMBERS

Module Name	Function	Module Number
A1	AERO coefficient table look-up	2
A2	Forces and moments module	3
A3	Engine module	4
C1	Autopilot module	7
C4	Actuator module	10
D1	Translational dynamics module	17
D2	Rotational dynamics module	18
G2	Winds module	23
G3	Air data module	24
SPOT	Spot jitter module	38
G5	Coordinate transformation module	26
S1	Seeker module	28

5. SUBL3 - Executive Subroutine

Executive subroutine, SUBL3, is called by MAIN at every integration step. SUBL3, in turn, calls INPT3, OUP3, STGE3, CNTR3, RNDM3, AUXA3, AUXB3, and AUXC3 depending upon the subroutine numbers stored in the array, SUBNO(I).^{*} The array, SUBNO(I), is initialized in OINPT1 by the subroutine numbers entered on type 1 input data cards. With the current configuration of the simulation program, two type 1 cards are input to enter subroutine numbers 3 and 4 into the SUBNO(I) array. This will cause SUBL3 to call subroutines OUP3 and STGE3 (described in Sections III. G. 2 and III. F. 12).^{*} Table 62 presents the SUBL3 input/output variables.

TABLE 62. SUBL3 INPUT/OUTPUT VARIABLES

Fortran Symbol	C Index	Definition
NOSUB	2461	Number of subroutines specified on type 1 input data cards
SUBNO(I)	2462	Subroutine numbers entered on type 1 input data cards

6. Table Look-Up Subroutines: TABLE, TABL2, and TABL3

These three subroutines are used for the express purpose of passing tabular aerodynamic data to the special function subroutines FINTP1, FINTP2, and FINTP3. These special function subroutines performs linear interpolation between two points in three types of tabular data tables. These data tables are:

- a) TABLE FINTP1 - one dependent, one independent variable.
- b) TABL2 FINTP2 - one dependent, two independent variables.
- c) TABL3 FINTP3 - one dependent, three independent variables.

The independent variable tables must be monotonically increasing data arrays. The argument list variables of the three subroutines are:

- a) TABLE (X, XI, YI, NX, YK, XLABEL, Y) -
 - X - Instantaneous value of independent variable.
 - XI - Independent variable array (table).
 - YI - Dependent variable array (table).

^{*}All of the named subroutines except INPT3 and OUP3 exist only as entry points in the subroutine DUMMY.

NX - Number of points in each table.

XK - Flag used in FINTP1.

XLABEL - reserved for hololith character name of data table.

Y - linear interpolated value of the dependent variable.

b) TABLE (X, Y, XYI, ZI, NXY, XINTER, XLABEL, Z) -

X - Instantaneous value of the first independent variable XI.

Y - Instantaneous value of the second independent variable YI.

XYI - This single array contains both the first (XI) and second (YI) independent variable tabular values. The first independent variable (XI) values occupies the leading element locations and the second independent variable (YI) values occupies the remaining element locations.

ZI - Dependent variable array. This array contains all dependent variable tabular values. The dependent variable values as a function of the first independent variable XI are subgroups of data in the array. The subgroups are then a function of the second independent variable YI. (The subgroups must be ordered such that they are a function of YI with YI monotonically increasing.)

NXY(I) - Number of points in the data tables:

I = 1, number of first independent variable (XI) data points

I = 2, number of second independent variable (YI) data points.

XINTER - Flag used in FINTP2.

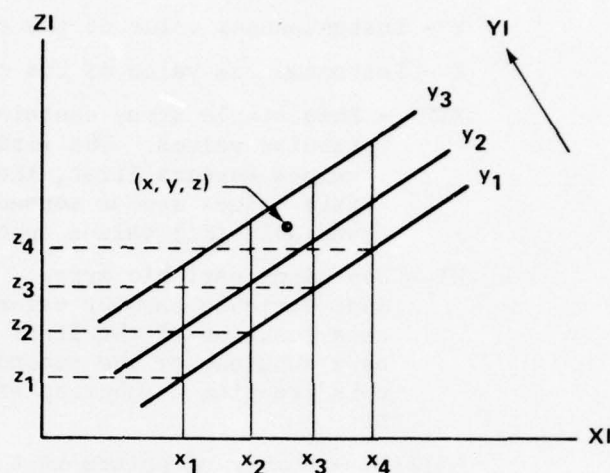
XLABEL - Reserved for hololith character name of data table.

Z - linear interpolated value of the dependent variable.

The following is an example of TABL2 use.

Assume the following set of data:

ZI	XI	YI
z ₁	x ₁	y ₁
z ₂	x ₂	
z ₃	x ₃	
z ₄	x ₄	
z ₅	x ₁	y ₂
z ₆	x ₂	
z ₇	x ₃	
z ₈	x ₄	
z ₉	x ₁	y ₃
z ₁₀	x ₂	
z ₁₁	x ₃	
z ₁₂	x ₄	



These tabular values would be assigned to the argument list arrays as follows:

$$XYI = x_1, x_2, x_3, x_4, y_1, y_2, y_3$$

$$Z_I = \left[\overbrace{z_1, z_2, z_3, z_4}^{y_1} \middle| \overbrace{z_5, z_6, z_7, z_8}^{y_2} \middle| \overbrace{z_9, z_{10}, z_{11}, z_{12}}^{y_3} \right] .$$

The number-of-points variables would be set as:

$$\begin{aligned} NXY(1) &= 4 \\ NXY(2) &= 3 \end{aligned} .$$

The discrete point (x, y) would be passed into the subroutine, a linear interpolation would be performed between the data points that bracketed (x, y) and a singular value of z would be returned. Thus,

$$\left. \begin{aligned} X &= x \\ Y &= y \end{aligned} \right\} \text{input}$$

Z = z - returned value.

c) TABL3 (X, Y, Z, XYZI, WI, NXYZ, XINTER, XLABEL, W) -

X - Instantaneous value of the first independent variable XI.

Y - Instantaneous value of the second independent variable YI.

Z - Instantaneous value of the third independent variable ZI.

XYZI - This single array contains all three independent variable tabular values. The first independent variable (XI) values appears first, the second independent variable (YI) values appear second, and the third independent variable (ZI) values appear last.

WI - Dependent variable array. This array contains all dependent variable tabular values. The dependent variable values as a function of the first independent variable (XK) appears as a subgroup of the second independent variable YI with this grouping a subgroup of the third independent variable ZI.

NXYZ(I) - Number of points in the data tables:

I = 1, number of first independent variable (XI) data points

I = 2, number of second independent variable (YI) data points

I = 3, number of third independent variable (ZI) data points.

XINTER - Flag used in FINTP2.

XLABEL - Reserved for hololith character name of data table.

W - Linear interpolated value of the dependent variable.

F. Auxiliary and Function Subroutines

1. Aerodynamic Coefficient Table Error Indication
Subroutines: AERROR and TERROR

Subroutine AERROR is used to indicate that the numerical range of an aerodynamic coefficient data table has been exceeded by the trajectory being flown. The message "OUT OF AERO TABLE ARGUMENT ARRAY" and the table name is printed out, along with a dump of the C-array element string that contains all the aerodynamic table values. The integration termination switch, LCONV, is then set to 2 to flag subroutine STGE3 that the run is to be terminated.

Subroutine TERROR is used to indicate that an entire aerodynamic coefficient table is missing. The message "NO AERO POINTS SPECIFIED FOR ARG" and the missing table name is written out. The run is then terminated by a CALL EXIT statement.

NOTE: These two subroutines are not being utilized by the program. No provision has been made to detect these errors in the aero tables not to call these subroutines.)

2. AMRK - Numerical Integration Routine

a. Functional Description

Numerical integration of the state vector derivatives is accomplished using the standard four pass fixed step Runge-Kutta technique. This routine numerically solves a simultaneous system of N first order differential equations.

AMRK calls AUXSUB, which in turn calls each functional module to evaluate state vector derivatives, update the state vectors, and calculate scalar quantities needed for evaluation of the derivatives.

b. Equations

The following equations show the calculations performed by AMRK. All state vector derivatives are evaluated on each pass of the four passes. Specifically, if the state vector derivative, \dot{Y}_i , is a function of time, n state vectors, and m scalar quantities,

$$\dot{Y}_i = f(t, Y_{j=1,n}, X_{k=1,m})$$

Then Y_i at $(t_0 + t)$ is evaluated by

$$\bar{Y}_i = \bar{Y}_{i0} + 1/6(K_{1i} + 2K_{2i} + 2K_{3i} + K_{4i}),$$

where

$$K_{1i} = f(t_0, \bar{Y}_{j=1,n}, X_{k=1,m})\Delta t$$

$$K_{2i} = f\left[\left(t_0 + \frac{t}{2}\right), \left(\bar{Y}_{j0} + \frac{K_{1j}}{2}\right)_{j=1,n}, (X_k)_{k=1,m}\right]\Delta t$$

$$K_{3i} = f\left[\left(t_0 + \frac{t}{2}\right), \left(Y_{j0} + \frac{K_{2j}}{2}\right)_{j=1,n}, (X_k)_{k=1,m}\right]\Delta t$$

$$K_{4i} = f\left[(t_0 + t), (Y_{j0} + K_{3j})_{j=1,n}, (X_k)_{k=1,m}\right]\Delta t,$$

and

t_0 = Time at start of integration step

\bar{Y}_{i0} = Value of i th state vector being evaluated at start of integration step

\bar{Y}_{j0} = Value of all n state vectors at start of integration step

t = Integration step size.

Sometimes it is necessary to avoid calculation of source scalar quantities on all but the first pass of the four passes. Therefore, a flag, XNDRK, is set to specify the first pass. Accordingly,

First pass - XNDRK = + 1.

All other passes - XNDRK = - 1.

c. Initialization

AMRK integration variables (state vector derivatives) are assigned in the initialization routine of each functional module. All state vector derivatives and integrated values are stored in the C-array. The IPL-array stores the pointers that point to the C-location or index of the derivative. The integrated value is automatically moved to .3 C-locations above the index of the derivative. For instance, if a second order derivative, \ddot{Y} , is to be assigned to C-location 300, then \ddot{Y} will be located in 303. Then the appropriate initialization routine

IPL (N) = 300
N = N + 1.

This will result in

$C(300) = \ddot{Y}$
 $C(303) = \ddot{Y}$.

N is the counter specifying the number of differential equations to be evaluated. N must be increased by the number of differential equations added to the IPL-array in each initialization routine.

If it is desired to continue the integration of this variable, \ddot{Y} , to bet \bar{Y} , then

IPL (N) = 300
IPL (N + 1) = 303
N = N + 2.

This will result in

$$\begin{aligned}C(300) &= \ddot{Y} \\C(303) &= \dot{Y} \\C(306) &= \bar{Y} \quad .\end{aligned}$$

d. Assumptions and Limitations

There are two important restrictions placed on the integration scheme.

(1) Rail Launched Missiles. If the missile is rail launched, then the integration stepsize is fixed in the program at 0.002 sec (in seeker initialization routine). This was done so that all runs with the same initial conditions would have the same rail drop-off time, regardless of the input value of integration stepsize. This was deemed necessary because rail drop off is checked only at the end of an integration pass. Thus, if integration stepsize is varied effectively, rail length and rail drop off time would vary, resulting in slightly direct flight paths for identical initial conditions.

Following rail dropoff, the integration stepsize is switched from 0.002 sec to the input value. Switching is normally accomplished in the seeker module, since integration must be synced with the seeker sample period (see following).

(2) Integration Synchronization with Sample Period. Numerical integration must be synchronized with sample period [2] in order to insure accurate integration. Logic is built into the seeker subroutines to insure that integration and sample period are synchronized. This is accomplished by:

$$\Delta t = \tau / [\text{AINT}(\tau / \Delta t_{\text{INPUT}})] \quad ,$$

where

τ = Sample period (sec)

Δt_{INPUT} = Input integration stepsize (sec)

$\text{AINT}(X)$ = Computer function that integerizes the argument (X)

Δt = Computer integration stepsize that the program will use.

The above function will always compute an integration stepsize that is equal to or greater than the input stepsize. Since there is an upper bound on the stepsize that can be used to integrate the differential equations in this simulation program, there is the possibility that a stepsize larger than the upper bound will be computed. (Upper bound is approximately 12.5 msec, with the exception of the OCS seeker model)

S2 which has an upper bound of approximately 0.5 msec). Therefore, one should insure that a reasonable stepsize is input and verify that a reasonable stepsize is computed. For example, if the sample period is 16.7 msec, then a stepsize of 8.35 msec or less must be input to insure that the computed stepsize is 12.5 msec or less.

e. Input/Output and Cross Reference of C-Array

Tables 63, 64, and 65 present the input/output and cross reference of C-array for AMRK.

TABLE 63. INPUT FROM DATA CARDS - AMRK

Fortran Symbol	Symbol Used in Text	C Index	Definition
DELT	Δt	2664	Integration stepsize (sec)

TABLE 64. INPUT FROM OTHER MODULES - AMRK

Fortran Symbol	Symbol Used in Text	C Index	Definition
T	t	2000	Flight time (sec)
N	NJ	2661	Number of differential equations
IPL	IPL	2562	Integration pointer array
C(J)	Y_j	IPL	State vector derivatives
C(J + 3)	Y_j	IPL + 3	Integrated value of state vector

TABLE 65. OUTPUTS - AMRK

Fortran Symbol	Symbol Used in Text	C Index	Definition
C(J + 3)	Y_j	IPL + 3	Integrated value of state vector
XNDRK	XNDRK	1976	Runge - Kutta pass flag +1. first pass -1. second, third, and fourth pass

3. Trig Special Function Routines: COSD, SIND, and ATAND

The special function trig routines COSD, SIND, and ATAND allow the user to work in units of degrees when dealing with angles. Use of the Fortran supplied functions COS, SIN, and ATAN2 is made through these intermediate special function routines. The input to the special functions COSD and SIND is Z, an angle expressed in degree, while the outputs are returned in X and Y, respectively.

```
Y = COSD(Z)
Y = SIND(Z) .
```

Output of the special function ATAND is

```
Z = ATAND(Y,X) ,
```

where Z is an angle in degrees with assignment to the proper quadrant and a range of ± 180 degrees.

4. DUMMY - Auxiliary Subroutine

Subroutine DUMMY contains, as ENTRY points, all of the subroutine names called in the simulation program. This feature allows the program to be modularly altered (e.g., removing a module or subroutine or substituting a module or subroutine) without the necessity of locating and removing all calls to nonexistent subroutines. A disadvantage to this approach is that the inadvertent omission of a needed subroutine will be detectable only by erroneous output results, because the subroutine will exist as an entry point in DUMMY, and a call to the subroutine will not cause a premature program termination.

5. DUMPO - Auxiliary Subroutine

Subroutine DUMPO prints the entire C-array when called. With the current program configuration, DUMPO can be called a maximum of seven times; six times by the input variable DOC and one time by the input variable OPTN10.

DOC allows C-array dumping for six integration intervals, starting with $t = 0$, and continuing for the next five integration steps. The input variable, DOC, is set to the number of C-array dumps fewer than six desired. Thus, if the six dumps are desired, DOC would be set to zero on input. If no dumps were desired, DOC would be set to six, etc. DUMPO is called by subroutine OUP2 to provide a C-array dump at $t = 0$ if DOC is input less than six. Subsequent calls (if any) of DUMPO are made from subroutine OUP3, within the integration loop.

If the input variable, OPTN10, is set greater than zero, the MAIN program will call DUMPO at the end of a case and dump the C-array.

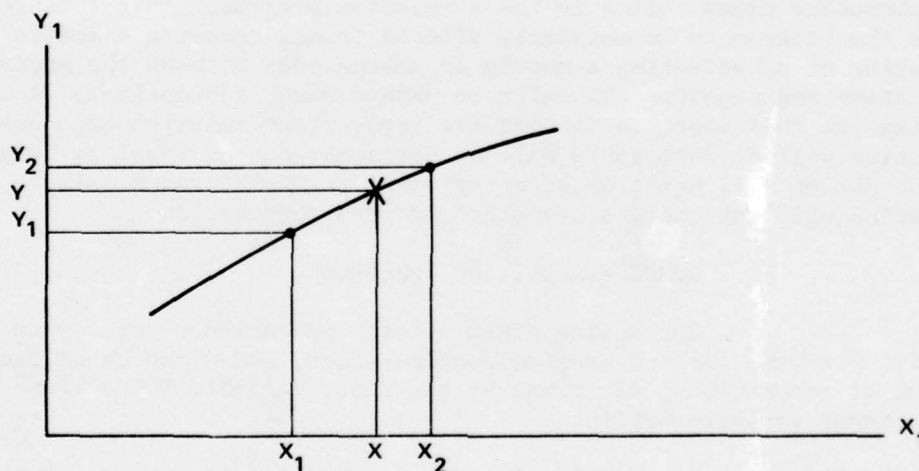
6. FINTP1 - Aero Table Linear Interpolation of a Function with one Dependent and One Independent Variable

Function FINTP1 utilizes the following equation to linearly interpolate between the two points for the value of the dependent variable when the dependent variable is a function of only one independent variable.

$$Y = P_{CT} (Y_2 - Y_1) + Y_1 ,$$

where

$$P_{CT} = \frac{X - X_1}{X_2 - X_1} .$$



The argument list variables, which are internal inputs to the subroutine, are defined as:

- X - Instantaneous value of the independent variable XI.
- XI - Independent variable array.
- YI - Dependent variable array.
- N - Number of points in the arrays.
- F - Flag that allows bypassing the computation of PCT.
- XL - (Not used).

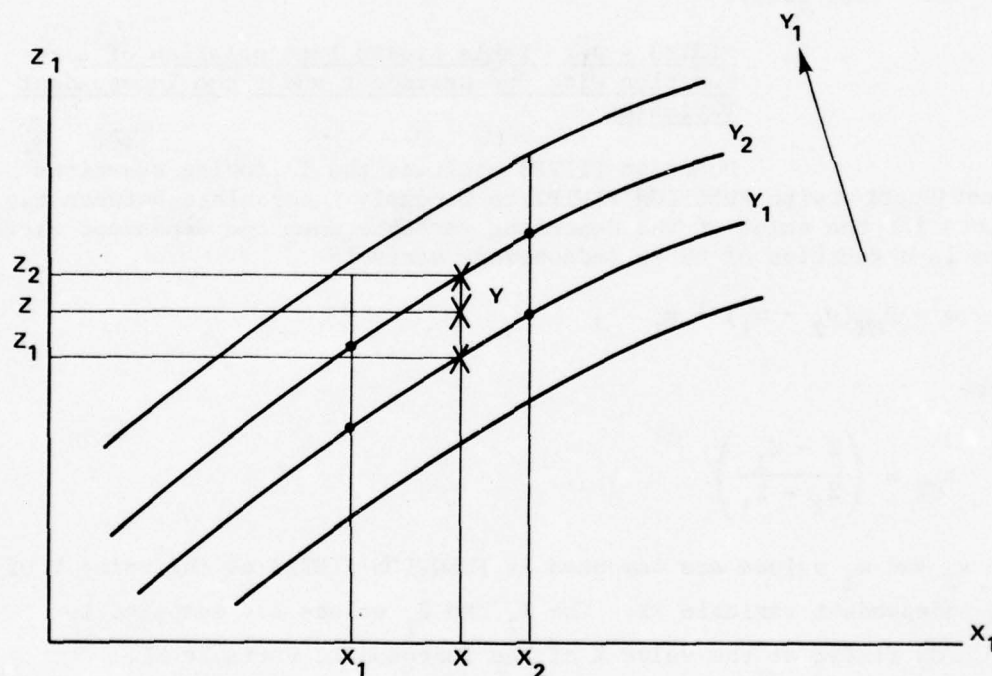
7. FINTP2 - Aero Table Linear Interpolation of a Function With One Dependent and Two Independent Variables

Function FINTP2 utilizes the following equations in conjunction with FUNCTION FINTP1 to linearly interpolate between two points for the value of the dependent variable when the dependent variable is a function of two independent variables:

$$Z = P_{CT} (Z_2 - Z_1) + Z_1 \quad ,$$

where

$$P_{CT} = \frac{Y - Y_1}{Y_2 - Y_1} \quad .$$



The Z_1 and Z_2 values are computed in FUNCTION FINTP1 at the value X of the independent variable XI .

The argument list variables, which are internal inputs to the sub-routine, are defined as:

X - Instantaneous value of the first independent variable XI.
 Y - Instantaneous value of the second independent variable YI.
 XI - First independent variable array.
 YI - Second independent variable array.
 ZI - Dependent variable array.
 NXO - Number of points in the first independent variable array.
 NY - Number of points in the second independent variable array.
 NX - Number of points in the first independent array.
 F - Flag that allows bypassing the computation of PCT.
 XL - (Not Used).

8. FINTP3 - Aero Table Linear Interpolation of a Function with One Dependent and Three Independent Variables

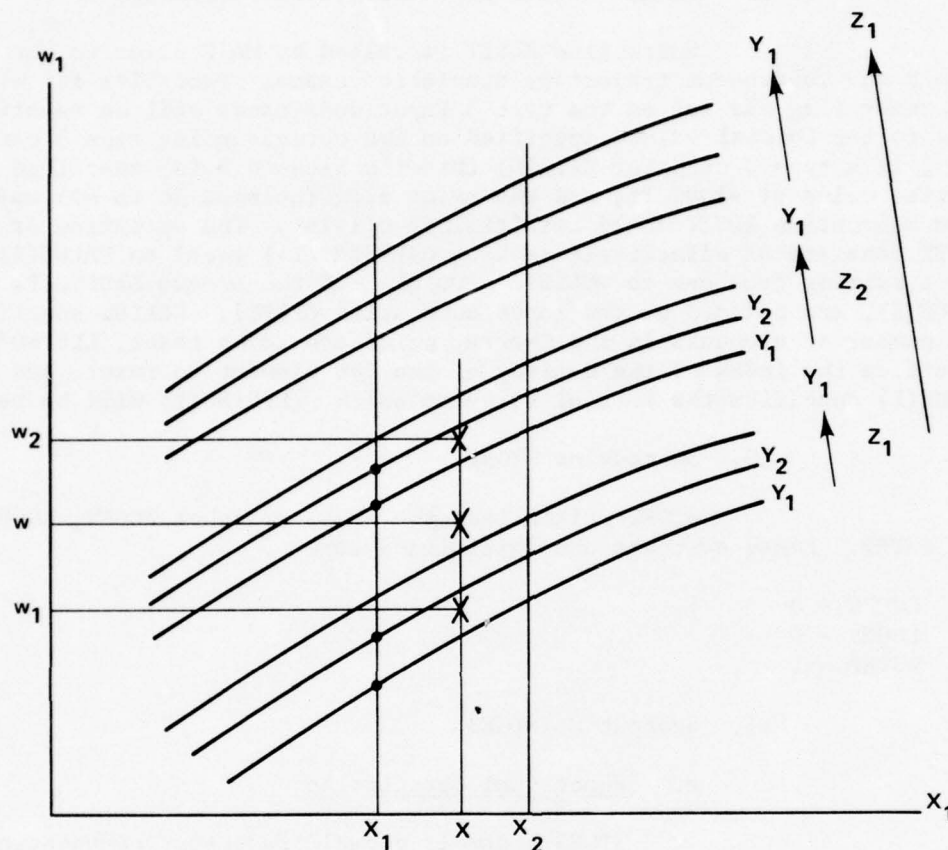
Function FINTP3 utilizes the following equations in conjunction with FUNCTION FINTP2 to linearly interpolate between two points for the value of the dependent variable when the dependent variable is a function of three independent variables:

$$w = P_{CT}(w_2 - w_1) + w_1 ,$$

where

$$P_{CT} = \left(\frac{Z - Z_1}{Z_2 - Z_1} \right) .$$

The w_2 and w_1 values are computed in FUNCTION FINTP2 at the value Y of the independent variable YI. The Z_2 and Z_1 values are computed in FUNCTION FINTP1 at the value X of the independent variable XI.



The argument list variables, which are internal inputs to the subroutine, are defined as:

- X - Instantaneous value of the first independent variable XI.
- Y - Instantaneous value of the second independent variable YI.
- XI - First independent variable array.
- ZI - Third independent variable array.
- WI - Dependent variable array.
- NZ - Number of points in the ZI array.
- NY - Number of points in the XI array.
- F - Flag to bypass computation of PCT in FUNCTION FINTP2.
- XL - (Not used).

9. RESET - Multicase Variable Reinitialization

Subroutine RESET is called by MAIN prior to the second and subsequent trajectory simulation cases. Variables for which the reset flag was set on the type 3 input data cards will be reinitialized to the initial values specified on the corresponding type 3 cards. Thus, if a type 3 card for C(1615) (missile X-coordinate) specified an initial value of -1000 ft, and the reset flag (columns 46 to 60) was 1., then subroutine RESET would reinitialize C(1615). The operation of RESET consists of effectively setting C(LISTNO(I)) equal to VALUE(I), for I ranging from one to NOLIST. NOLIST, and the arrays LISTNO(I) and VALUE(I), are defined by the input subroutine OINPT1. NOLIST specifies the number of elements in the C-array which are to be reset, LISTNO(I) specifies the index of the C-array of the Ith element to reset, and VALUE(I) specifies the initial value to which C(LISTNO(I)) will be reset.

10. Subroutine STGE2

STGE2 initializes the STGE3 switches KCONV, LCONV, and KSTEP. These switches are initialized as:

```
KCONV = 0
LCONV = 0
KSTEP = 1 .
```

11. Subroutine STGE3

a. Functional Description

STGE3 controls normal trajectory computation termination and calls OUP3 for output following trajectory termination. There are three modes of normal trajectory computation termination handled by STGE3. The events defining these three modes are:

- 1) Flight time (T) reaches the input maximum flight time boundary (TF).
- 2) Missile reaches the point of closest approach to the target trajectory intersects the target plane) (flagged in G4).
- 3) Missile flies into the ground (flagged in G4).

Trajectory computation will be terminated by the event that occurs first. When termination is to occur as a result of one of the previously mentioned events, STGE3 sets the switch KSTEP equal to 2 to flag MAIN that the case is to be terminated.

Mode 1 is handled directly by STGE3. The actual flight time T is compared to the input maximum flight time boundary TF. If T is within 0.01 sec of TF, STGE3 sets the switch KSTEP for case termination. However, if T exceeds TF, STGE3 initiates an integration step size halving

scheme to iterate for a final integration step size to force T to fall within the 0.01-sec tolerance of FT. If, however, T does not fall within this tolerance of TF after ten interval halving passes, the case will be automatically terminated.

Modes 2 and 3 are handled indirectly by STGE3. These events are determined in other modules with the module making the determination setting the switch LCONV equal to 2 to flag STGE3 that an event has occurred and that trajectory computation is to terminate. STGE3 monitors LCONV, and when a value of 2 appears, STGE3 sets the switch KSTEP equal to 2 to flag MAIN that the case is to be terminated.

The definition of variables used in STGE3 is given in Table 66.

b. Initialization Subroutine

Subroutine STGE2 initially sets the flags LCONV = 0 and KSTEP = 1. STGE2 is called by subroutine SUBL2 at the start of trajectory initialization.

12. ZERO - Auxiliary Subroutine

Subroutine ZERO zeros certain elements of the C-array. The variable names and the corresponding C-array indices are:

<u>Variable</u>	<u>C-array</u>
<u>Name</u>	<u>Index</u>
NPLOT	1984
OPOINT	2023
NOMOD	2361
NOSUB	2461
NOLIST	3066
NOOUT	3167

G. Input/Output Subroutines

1. OINPT1 - Input Subroutine

Subroutine OINPT1 reads the input data cards. The input information is stored in arrays determined by the data card type number (see Section IV for input data card formats). Table 67 lists the input data card types and Table 68 lists the array in which input information is stored. Other than the type 6 card, which must come at the end of a data set, the cards can be input in any order. The module and staging subroutine control cards; however, the order must correspond to the desired execution order of the subroutines and modules.

TABLE 66. DEFINITION OF VARIABLES USED IN STGE3

Fortran Symbol	C Index	Source Module(s) or Input Data	Definition
T	2000	AMRK	Number of seconds into flight simulation (flight time)
TF	2001	INPUT	Upper bound to simulation flight time (flight time cutoff) (sec)
PCNT	2003	OUP2 OUP3 STGE3	Time boundary in seconds below which no output/plotting from OUP3 is performed
STEP	2010	INPUT	Switch that specifies the nature of the next case that follows termination of this case. (STEP=11 indicates that no additional case follows)
KSTEP	2011	STGE2 STGE3	Switch used to flag MAIN that run termination has occurred. (Set to 1 in STGE2; set to 2 in STGE3) 1 - continue integration 2 - stop integration
LCONV	2020	STGE2 G4 S2 S3	Switch used to flag STGE2 that run termination is to occur. 0 - continue integration 1 - ? 2 - terminate computation
DER(1)	2664	INPUT	Integration step size (sec)
KCONV	2021	STGE2 OUP2 STGE3	Pass counter for step size halving in the iteration loop to force T within the hard wired tolerance of 0.01 sec of TF. (Set to zero in STGE2 and OUP2)
N	2561		Counter for loading IPL
NPT	1975	Program	array integration mode control
NJ	1974	Variables	switch number of derivations

TABLE 67. INPUT DATA CARD INFORMATION

Data Field											
Card Type	1	2	3	4	5	6	7	8	9	10	11
1	Card Type	Identification	Subroutine No.								
2	Card Type	Identification	Module No.								
3	Card Type	Identification	C-array Index				Index variable value	Reset flag			
4	Card Type	Identification	C-array Index								
6	Card Type	Identification									
7	Card Type	Identification	C-array index	Not used	Scale option	Not used	Fixed scale upper limit	Fixed scale lower limit			
8	Card Type	Identification	C-array index	Type distribution of error source	Type of period for time series sampling	Standard development of sample period of time series parameter see Section IV. A. 6	Error source standard development if normal distribution; an interval multiple if uniform distribution	Error source upper bound	Error source lower bound	C-index of location to store random error value, if blank error stored in field 3	Time series sampling period, if periodic error value, sample rate; or mean of sample period if random sample rate
9	Card Type	A 9-card requires the reading of another data card whose parameters are described in Section IV. A. 7.									
10	Card Type	Identification of variables for which mean variable and standard development is computed	C-array index								

TABLE 68. FORTRAN ARRAY NAMES

Data Card Type	Stored in Array										
	1	2	3	4	5	6	7	8	9	10	11
1			SUBNO								
2			MODNO								
3			L				C (L)	LISTNO			
4		ONAME1 ONAME2	OUTNO								
6											
7		VLABEL	OUTPLT								
8	Initial Condition Time Series		I SNDX I SNDX ITNDX ITNDX2	IDIST			SIGMA	SIGLB	SIGUB		
				ITDIST		TPSIG	TSGMA	TLB	TUB	ITNDX2Q	TSPER
9											
10			IMVNDX								

The logic of OINPT1 reads variable values on type 3 cards directly into the specified position of the C-array in the order in which the cards are read. Hence, a previously defined element of the C-array will be overridden by the new value if the same C-index is specified on another 3-card encountered later in the data card set. Thus, an input variable can be changed in the data card set by simply adding the desired card behind the original one(s) in the set. This cannot be done, however, with the data cards other than type 3 cards. Adding an additional type 2 (module selection) card, for example, without removing the one to be replaced will cause both modules to be executed in the integration loop.

2. OUPT3 - Output Subroutines

a. Functional Description

OUPT3 controls printed output of desired data generated during integration of the missile trajectory. Specifically, OUPT3 performs the following:

1) Saves maximum and minimum values of the Y and Z components of laser designator spot jitter.

2) The C-array dump option (DOC) that allows output of the C-array at the first DOC-6 integration steps is exercised in this routine. OUPT3 checks the flag ITCNT (if $ITCNT \leq 6$, dump C-array) to determine if a C-array dump is desired. ITCNT is set initially to DOC + 1 in OUPT2 and bumped up by 1 each pass through OUPT3 until it exceeds 6. No C-array dump is made if ITCNT is greater than 6.

3) The trajectory time (T) and integration step size (DER(1)) is printed out by OUPT3, following a change in integration step size made in the integration subroutine, AMRK.

4) Output data specified on type 4 input data cards is output from OUPT3. The symbol names located in the second and third ALPHA fields of type 4 data cards are printed out five symbols per row with double spacing between each row. This symbol block is output before the first block of output data is printed and then every two pages of print thereafter. The value of the parameters specified by the C-index on type 4 cards is printed out at each time point interval specified by the input variable, CPP. These data blocks are output until two pages of print are filled. At this time, the symbol block is reprinted, followed by a resumption of the data block output print.

b. Initialization Subroutine

OUPT2 sets KCONV, the run termination switch to zero, initializes certain output and plot flags and calls DUMPO to execute the first C-array dump if $DOC < 6$.

3. PLOT4-PLOT Routine

a. Functional Description

The 6 DOF simulation program has a plotting capability. However, the array (GRAPH) and the file (TAPE1) for storing and disposing of plot requested data are not a permanent part of the simulation program. Instead, a plot-package UPDATE deck and a DISPOSE card must be used when making runs requiring plots.

This approach was taken because the addition of the storage part of the plot package increased the memory requirements significantly. Thus, to keep job turn-around time in the computer as low as possible for normal runs, the plot storage package was not included as a permanent part of the program.

Plotting is done with the Houston Instrument COMLOT Digital Incremental Plotter. This plotter is not available at the central computer site, but instead is tied to and driven on-line at various remote terminals. This means that the operation (loading paper, pens, turning on, etc.) of the plotter is left up the user.

Plot data are stored on a disc file named TAPE1. To plot, TAPE1 must be disposed of when the run is completed. This is done by placing a DISPOSE card in the job control language input stream. For example, to plot on the COMLOT at a remote terminal logged in as GT use the following dispose card:

```
DISPOSE(TAPE1, PR = IGT) .
```

Place the DISPOSE card after the LGO card. In addition, to avoid losing plot data if an abnormal termination occurs during execution, place a DISPOSE card after the EXIT card as well.

A summary of plot capability utilization follows:

1) Use the following UPDATE package:

```
*IDENT PLOT1
*DELETE MC7.3
  .,TAPE1) (start in card column 6)
*INSERT MC7.43
  DIMENSION GRAPH (300,15) (start in card column 7)
*INSERT IO.165
  DIMENSION GRAPH (300,15) (start in card column 7)
*INSERT IO.200
  DIMENSION GRAPH (300,15) (start in card column 7)
*DELETE PLOT.6
```

- 2) Place a DISPOSE card after the LGO card; example,

DISPOSE (TAPE1, PR = IGT)

- 3) Input 7-cards and 3-cards as required. A description of 7- and 3-cards required for plotting is given in Section IV. A. 7.

b. Input/Output

Up to 15 variables may be plotted for a given trajectory simulation. Plotting is controlled by use of 7-cards with plotting options falling in two categories. The first category involves the plotting of time histories and the second involves plotting of selected pairs of variables, one against the other.

(1) Time History Plots, Y versus T. For each 7-card input, one variable (specified by the C-index on the 7-card) will be plotted against time. The time array is saved automatically. Scaling of the ordinate axis may be automatic (based on range of data in plot array) or the ordinate scale limits may be specified. The 7-card contains the following input fields:

- a) 7 in card column 2.
- b) Ordinate label, card column 9 to 20.
- c) C-index of variable to be plotted against time, right adjusted in card columns 21 to 25.
- d) Scale option, card column 27 -
 - 0 - automatic scaling
 - 1 - fixed scale limits.
- e) Limits for fixed scale (Y-axis only) -
 - Upper limit, card columns 31 to 45
 - Lower Limit, card columns 46 to 60.

The time axis is automatically scaled based on the data range of the time array.

(2) Paired Plots, Y versus X. Any variable in the C-array may be plotted against any other variable in the C-array. This option requires a 3-card to specify the number of paired plots and 7-card for the abscissa and a 7-card for the ordinate. Thus, one paired plot requires two 7-cards. In addition, an order must be observed in reading these cards in. The order is as follows:

- a) All paired plot 7-cards must be in front of all nonpaired plot 7-cards.
- b) All paired plot variables must be on consecutive 7-cards.

- c) The abscissa 7-card (X) must be the first 7-card in a paired plot pair.
- d) The number of paired plots must be specified by 3-card input variable PLOTN2, whose C-index is 1983.

The paired plot 7-card contains the following input fields:

- a) 7 in card column 2.
- b) Axis label in card column 9 to 20.
- c) C-index of plot variable right adjusted in card columns 21 to 25.
- d) Scale option, card column 27
 - 0 - automatic scaling
 - 1 - fixed scale limits, ordinate only, abscissa automatically scaled
 - 2 - fixed scale limits, ordinate and abscissa.
- e) Limits for fixed scale -
 - Upper limit, card columns 31 to 45.
 - Lower limit, card columns 46 to 60.

Each variable on the paired plot 7-cards will be plotted versus time (under the first category) before the paired plots are made. These time history plots may be suppressed by setting PLONT4 = 1. This option will eliminate all time history plots. Therefore, if this option is selected and it is desired to have some time history plots, then the time history variable and the variable time (T) will have to be treated as paired plot variables.

c. Input/Output Variables and Cross Reference of C-Array

The input/output variables and cross reference of C-array are presented in Tables 69, 70, 71.

TABLE 69. INPUT FROM DATA CARDS (3-CARD) - PLOT4

Fortran Symbol	Symbol Used in Text	C Index	Definition
PLOTN2		1983	Number of paired plots
PLOTN4		1982	Time history suppression switch - 0 - plot all paired plot variables against time 1 - plot no automatic time histories
PPP		2005	Plot sample interval (sec)
PST		2002	Plot sample start time (sec)

TABLE 70. INPUT FROM OTHER MODULES AND SUBROUTINES - PLOT4

Fortran Symbol	Symbol Used in Text	C Index	Definition
GRAPH(I,J)		None	Storage array for the Ith time point of the Jth variable to be plotted. Defined in OUP3
TIME(I)		2025 to 2324	Storage array for the Ith time point of flight time. Defined in OUP3

TABLE 71. OUTPUT - PLOT4

Fortran Symbol	Symbol Used in Text	C Index	Definition
			A plot file, TAPE1, contains all plot data. To plot, TAPE1 must be disposed of when the run is completed. This is done by palcing a DISPOSE card after the LGO card. For example, to plot at remote terminal GT: DISPOST (TAPE1, PR = 1GT)

IV. INPUT/OUTPUT FORMAT

A. Input

1. Introduction

Program inputs fall into ten major categories. The category of each data card input is identified to the input section of the program by the card type punched in card column 1. The data categories and the corresponding card types are indicated in Table 72.

The program is designed in the deterministic mode to sequentially simulate multiple trajectory cases in a single run; or in the stochastic mode, a number of Monte Carlo runs are made (the number of runs determined by the number of 6-cards in the data deck) followed by statistical analysis performed on the data generated. An example data deck setup for a deterministic run is shown in Figure 53. A Monte Carlo deck setup is shown in Figure 54. The program input logic is structured to optionally allow the input data sets for successive cases to include only data which differs from or augments data in the immediately preceding case. Thus, for example, if case 2 differed from case 1 by only the value of the launch heading azimuth angle, then only the new value of launch heading azimuth angle would be required in data set 2.

TABLE 72. INPUT DATA CATEGORIES AND CORRESPONDING CARD TYPE

Card Type (Card COL 1)	Data Category
1	Output and staging subroutine selection
2	Module selection
3	Program parameter input values
4	Print variable selection
6	Data set termination indicator
7	Plot variable selection
8	Monte Carlo input parameter selection
9	CEPAS control information
10	Mean and standard deviation output variable selection

The program is designed in the deterministic mode to sequentially simulate multiple trajectory cases in a single run; or in the stochastic mode, a number of Monte Carlo runs are made (the number of runs determined by the number of 6-cards in the data deck) followed by statistical analysis performed on the data generated. An example data deck setup for a deterministic run is shown in Figure 52. A Monte Carlo deck setup is shown in Figure 53. The program input logic is structured to optionally allow the input data sets for successive cases to include only data which differs from or augments data in the immediately preceding case. Thus, for example, if case 2 differed from case 1 by only the value of the launch heading azimuth angle, then only the new value of launch heading azimuth angle would be required in data set 2.

Program variables which can be set by input are initialized to zero by the program prior to reading the input cards for the first case. Consequently, program constants (constant gains, deadband angles, etc.) which are to have values of zero do not require an input card. Program variables which are to be initialized to zero, but varies during simulation, however, will require an input card with the initial value reset flag set if multiple cases are being run, and the desired initial value of the variable is zero for each case.

The program input logic does not require that the cards be arranged according to card type sequence. Thus, type 1, type 2, etc., cards can appear anywhere in a data set; cards of a given type can even be separated by different card types. The order of appearance of the type 2 (module selection cards), however, dictates the execution order of the modules during a simulation. Because the module execution order is critical to a valid simulation, the order of appearance of the type 2 cards within a data set must be as specified in Section IV. A. 3.

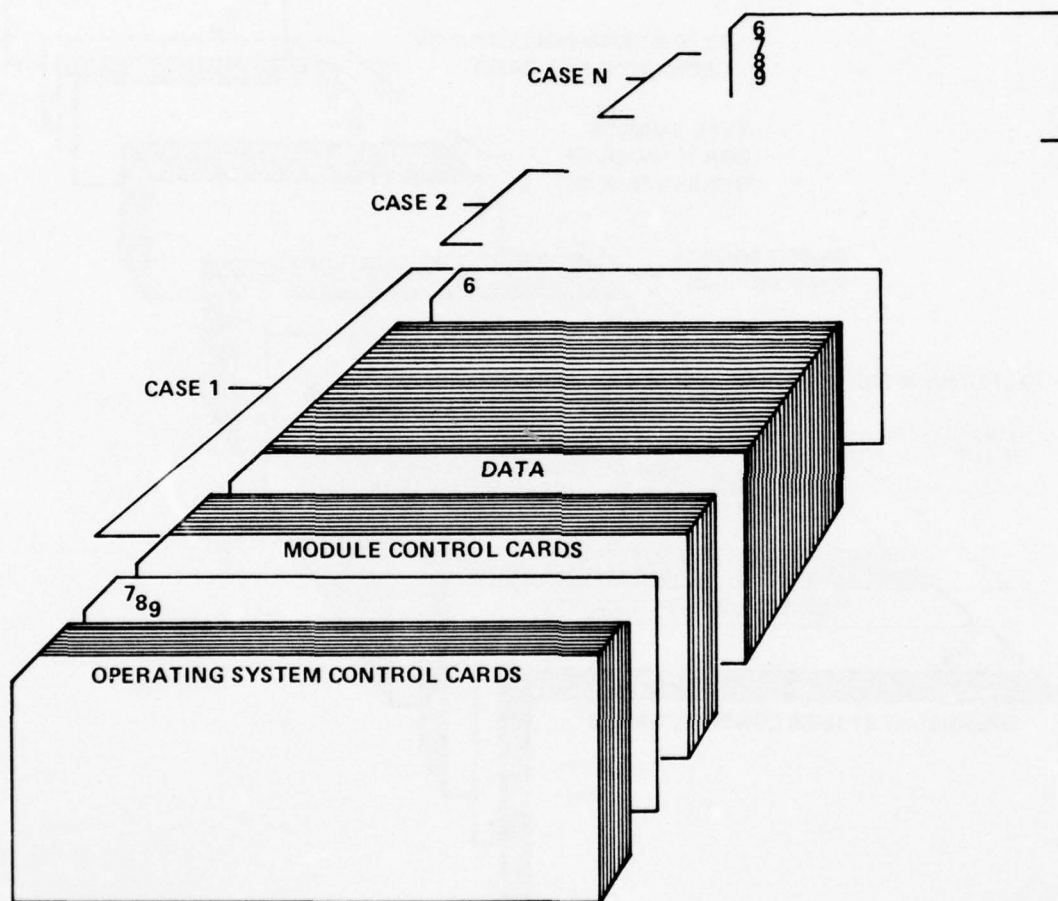


Figure 52. Deterministic deck setup.

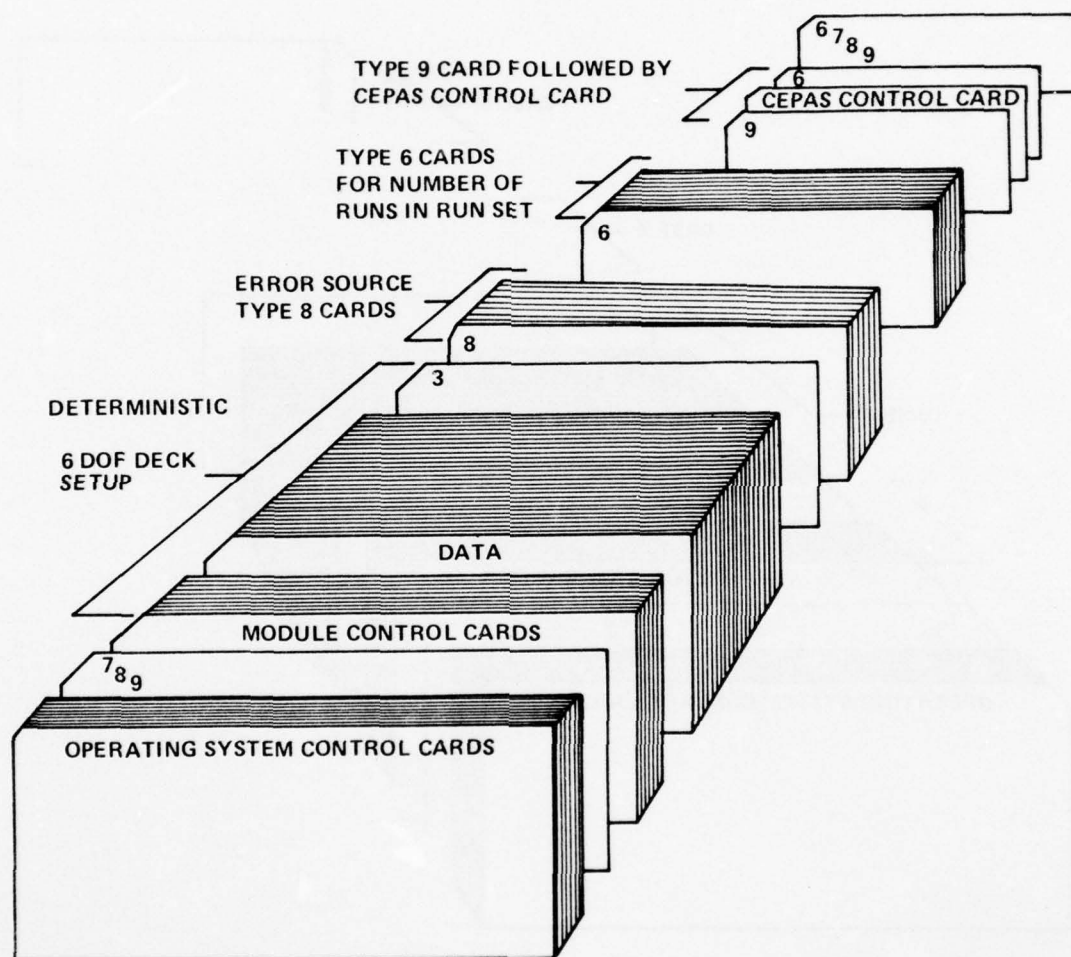


Figure 53. Monte Carlo deck setup.

As was previously mentioned, the number of runs in a Monte Carlo run set is controlled by the number of 6-cards in the data deck. CEP calculations are controlled by a 9-card (Figure 53). CEPAS information and type 9 cards are handled differently from all other card types. In this case, no other information other than card type number is punched on this card. The CEPAS control parameter card is placed immediately following the type 9 card. The type 9 card and CEPAS control parameter card are then placed in front of the last type 6 card.

2. Card Type 1 - Output and Staging Subroutine Selection

Data entered on type 1 cards controls, in principle, which output and staging subroutines are used during a simulation. With the current configuration of the program, however, only one option is available. Therefore, the type 1 cards must be input as shown in Figure 54 (the order of appearance in the deck is unimportant).

3. Card Type 2 - Module Section

Data entered on type 2 cards determines which modules will be executed during a simulation. Moreover, as previously mentioned, the order of appearance in the deck of the type 2 cards determines the order of module execution. Therefore, the cards must be input in the order as illustrated in Figure 55. The winds module (G2) cards can be omitted if a run is to be made with no winds.

The module name field is used for data identification only. Any name, comment, etc., can be entered in this field. The module number must be the number (shown) recognized by the program.

4. Card Type 3 - Program Parameter Input Values

The type 3 cards specify initial parameter variable values. If the reset flag is set to 1, the program will reset the variable to the input value at the end of the case corresponding to the data set. Any subsequent cases, therefore, will use the same initial variable value, until a data set is encountered which changes the initial value. If multiple cases are being run, each variable that changes its value during the simulation should either have the reset flag set or have an initial value defined for each case; otherwise, cases after the first will be initiated with the variable equal to its terminal value in the preceding case.

Initial values from type 3 cards are read directly into a single array using the number entered in column 21 through 25 as the array subscript. Therefore, the index value must be right justified and represent the correct array index. Table 73 shows the array index for each input variable. The name field is for print identification only. Because the initial value data on type 3 cards is read directly into the location in the variable array specified on the card, two or more type 3 cards with the same index entry will result in all but the last input value being obliterated. The last encountered value will be the one used for the parameter initial value.

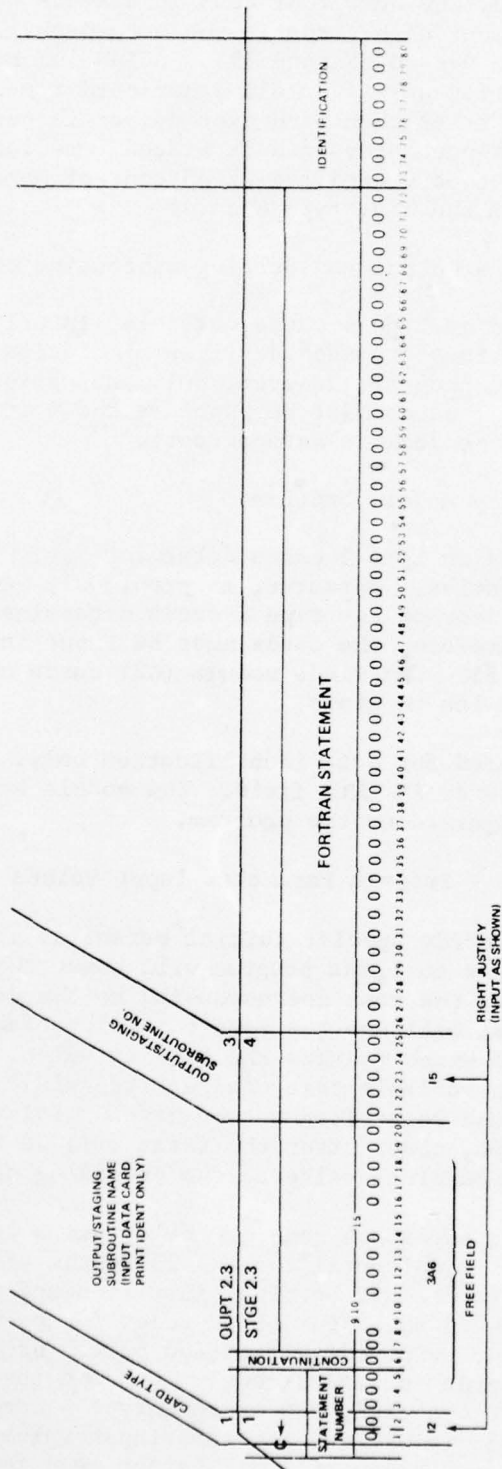


Figure 54. Type 1 card format.

CARD TYPE	MODULE NAME (INPUT DATA CARD PRINT IDENT ONLY)	MODULE NUMBER
2	G2	23
2	G3	24
2	SPOT	38
2	G5	26
2	A1	2
2	A3	4
2	A2	3
2	D1	17
2	D2	18
2	S1	28
2	C1	7
2	C4	10

GENERAL PURPOSE FIELD									
0	0	0	0	0	0	0	0	0	0
1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9
ONE	TWO	THREE	FOUR	FIVE	SIX	SEVEN	EIGHT		
0	0	0	0	0	0	0	0	0	0
1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9

12 3A6 15 RIGHT JUSTIFY

Figure 55. Type 2 card format.

TABLE 73. INPUT DATA

Fortran Symbol	C Index	Definition
		<u>Input to Executive Routines</u>
		<u>Plot Control</u> (see Section III. E. 3)
PLOTN2	1983	Number of paired plots
PLOTN4	1982	Time history plot suppression switch: 0 - plot all paired plot variables against time 1 - plot no automatic time histories
PPP	2005	Plot sample interval (sec)
PST	2002	Plot sample start time (sec) Use UPDATE package listed below. *IDENT PLOT1 *DELETE MC7.3 ., TAPE1) (Start in card column 6) *INSERT MC7.43 DIMENSION GRAPH(300,15) (Start in card column 7) *INSERT IO.165 DIMENSION GRAPH(300,15) (Start in card column 7) *INSERT IO.200 DIMENSION GRAPH(300,15) (Start in card column 7) *DELETE PLOT.6 Place a DISPOSE card after the LGO card; example DISPOSE(TAPE1, PR = IGT)
		<u>Print Control</u>
CPP	2015	Printing interval (sec)
DOC	2013	Allows dumping of C-array for the first (6 DOC) integration intervals (normally input 6.)
OPTN10	2022	C-array dump option end of run: 0 - no C-array dump 1 - dump C-array at end of run
		<u>Integration Parameters</u>
T	2000	Initial value of flight time (sec)
TF	2001	Maximum allowable flight time (sec)

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JUL 76 C L LEWIS, W R HOOKER, A W LEE

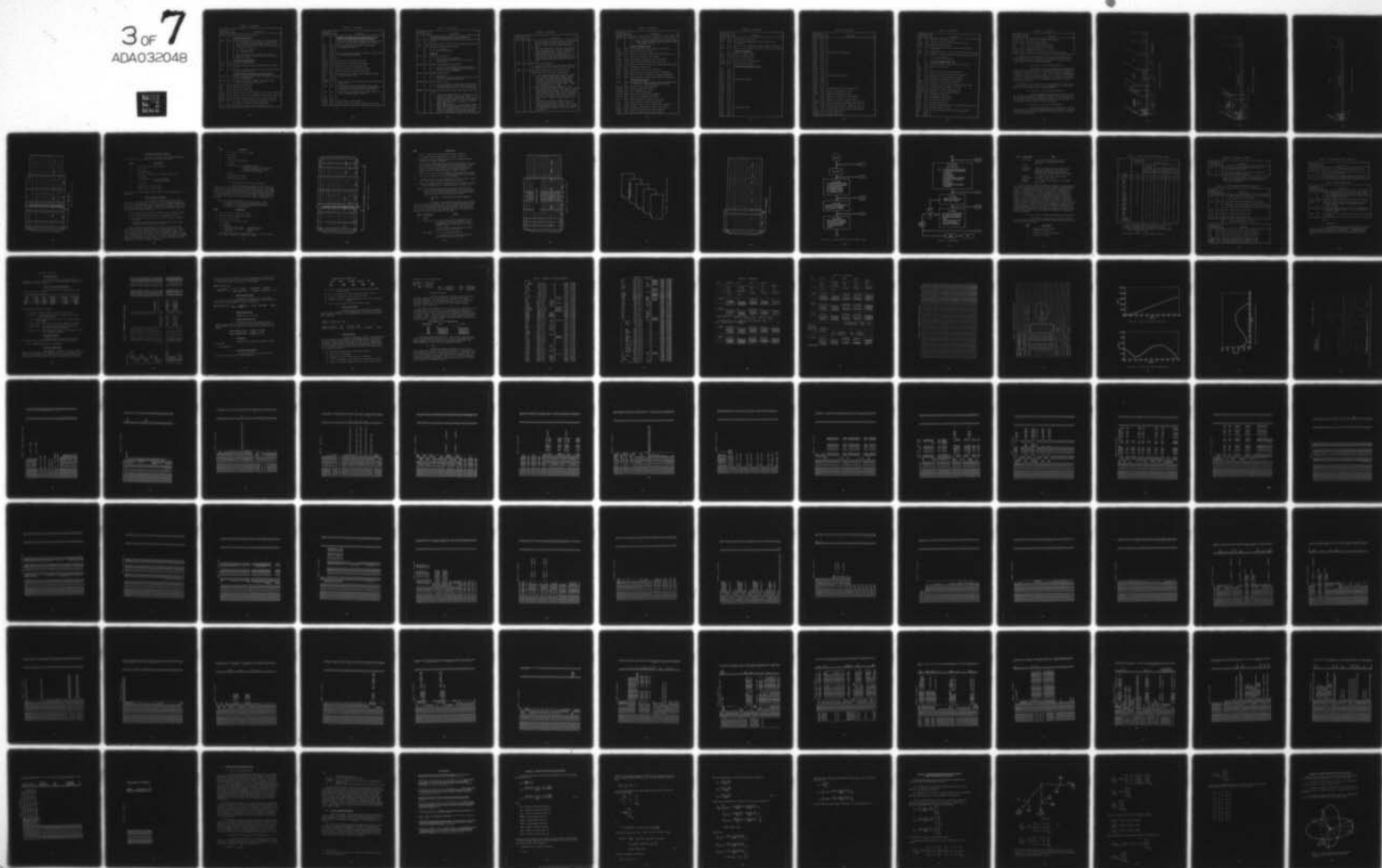
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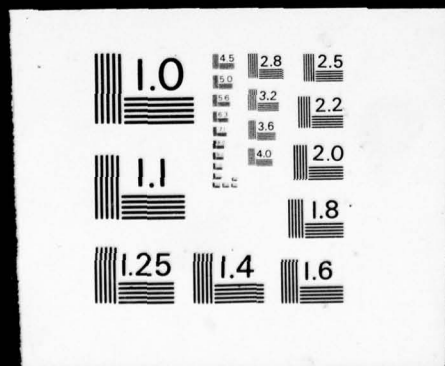


TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
DER(1)	2664	Integration step size (sec)
		<u>Multiple Run Control</u>
STEP	2010	Flag that indicates the nature of the next case to be run. STEP may take on any one of eleven values. The input value of STEP determines the point in MAIN at which the next case will be start execution. Normal input values are: 2 - normal run follows 11 - terminate case (The entry point in MAIN based on the value of STEP is indicated in Figure 64 for all values of STEP from 1 to 11)
		<u>Constants for Simulation</u>
AGRAV	1627	Gravity constant (ft/sec)
RHZRO	1665	Distance of earth fixed coordinate above sea level (ft)
CRAD	1751	Radians to degrees conversion factor (57.295778 hard-wired in module DII)
		<u>Missile Weight, Engine, and Airframe Parameters</u>
QNALGN	1403	Engine misalignment option switch (QNALGN > 0) selects engine misalignment)
QBURN	1405	Engine burnout switch (QBURN > 0) signals engine burnout at simulation initiation)
CISP	1414	Specific impulse (sec)
DWT	1415	Missile weight (lb)
DWP	1416	Propellant weight (lb)
RDCGO	1417	Launch value of CG displacement along X-body axis (ft)
RDCGF	1418	Burnout value of CG displacement along X-body axis (ft)
FMI XO	1419	Initial moments of inertia about X and Y body axes
FMI YO	1420	(Due to assumed missile axis symmetry, FMIZF is taken to be equal to FMIYF) (slug-ft ²)
RLCGO	1431	Distance between launch CG and REAR lug (ft)

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
		<u>Missile and Target Initial Position and Velocity Values and Missile Initial Attitude Setting</u>
		(Input of the following parameters is governed by the two input options, OPTN2 and OPTN4; see Table 74 .
RXE	1515	Initial components of missile in earth fixed coordinate system (ft)
RYE	1619	
RZE	1623	
VXE	1603	
VYE	1607	Initial velocity components of missile in earth fixed coordinate system (ft/sec)
VZE	1611	
BPSIO	1754	
BTHTO	1753	
BPHIO	1752	Initial body roll Euler angle (deg)
BTHTG	427	Initial seeker pitch gimbal angle (deg)
BPSIG	431	Initial seeker yaw gimbal angle (deg)
RTXE	1651	Target position in earth fixed coordinate system (normally zero) (ft)
RTYE	1655	
RTZE	1659	
RSLANT	1667	Initial magnitude of the line-of-sight vector (slant range) (ft)
BSLOV	1666	Initial value of the line-of-sight vector angle (measured in a vertical plane from missile local horizontal to the line-of-sight vector (deg).
VWXE	100	Initial velocity components of a steady wind in the earth coordinate system (ft/sec)
VWYE	101	
VWZE	102	
VMACH	204	Initial value of Mach number
VMWTE	1674	Initial velocity of missile relative to the wind

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
		<u>Launcher Parameters (Input Only if OPTN4 > 0)</u>
RAIL	1317	Rail length (between rear of front lug and end of rail) (ft)
RLUG	1316	Spacing between front and rear missile launch lugs (ft)
VIB	626	Launch transient vibration flag: 0 - no vibration 1 - run with vibration
		<u>Options</u>
OPNW	50	Wind option selector: 0 - no winds (no input required) 1 - steady winds (see Table 75) for input data requirements
QNALGN	1403	Thrust misalignment option selector: 0 - no thrust misalignment (no inputs required) 1 - compute thrust misalignment forces (see Table 75 for input data requirements)
QBURN	1405	Engine burnout switch: 0 - engine burn 1 - initialize trajectory after engine burnout (see Table 77 for additional inputs)
OPTARG	1639	Target motion option: 0 - no target motion (no additional input required) 1 - integrate target motion to update target position (see Table 70 for input data requirements)
OPTN2	3502	Initial position and velocity input option (see Table 74) 0 - input position and velocity of missile and input position of target. Input Euler angles of missile and seeker gimbal angles. Input missile initial velocity relative to the wind (VMWTE or VMACH) and wind velocity components (if wind option OPTNW = 1) 1 - input RSLANT and BLSOV. Initial position components (RXE, RZE) are computed from RSLANT and BSLOV. RYE automatically set to zero. Initial velocity components (VXE, VYE, VZE) computed from the wind velocity (VWXE, VWYE, VWZE which

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
		<p>must be input) and missile velocity relative to the wind (VMACH or VMWTE, which also must be input). Target position automatically set to zero</p> <p>2 - input initial position components RXE and RZE (RYE automatically set to zero). RSLANT computed from RXE and RZE. Initial velocity components (VXE, VYE, VZE) computed from wind velocity and missile velocity relative to the wind (VMACH or VMWTE, which also must be input.) Initial target position automatically set to zero</p>
OPTN3	3503	<p>Roll rate option selector:</p> <p>0 - compute roll rate from moments about roll axis</p> <p>1 - maintain roll rate at zero or input constant</p>
OPTN4	3504	<p>Rail launch dynamics and fire selector option:</p> <p>(see Table 74 for input data requirements)</p> <p>0 - no rail dynamics compute; direct fire. Input initial seeker gimbal angles (BHTG, BPSIG). The initial body Euler angles (BPSIO, BHTO) are computed from the seeker gimbal angles under the constraint that the X-gimbal axis points along the line-of-sight vector. (BPHIO is automatically set to zero)</p> <p>1 - rail dynamics computed; direct fire. Input initial body Euler angles (BPSIO, BHTO). (BPHIO automatically set to zero). The initial seeker gimbal angles (BHTG, BPSIG) are computed from the initial body Euler angles under constraint that the X-gimbal axis points along the line-of-sight vector. (BPHIO is automatically set to zero)</p> <p>2 - rail dynamics computed; indirect fire. Input initial body Euler angles (BPSIO, BHTO). (BPHIO automatically set to zero). The seeker is automatically caged at the input initial gimbal angle values. (BPSIG, BHTG) until target acquisition</p>

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
OPTN6	3506	Missile initial velocity (relative to wind) option: 0 - input missile initialmach number (VMACH, C(204)) 1 - input missile initial velocity relative to the wind (VMWTE, C(1674)) <u>Seeker Parameters - S1</u>
DT	446	Laser designator pulse repetition time (sec)
SWP	452	Autoerection drift factor
RLOCK	445	Maximum quadrant tracker acquisition range (ft)
BDB	447	Tracker deadband at 10 km (deg)
CFOVZ	448	Total seeker field-of-view in pitch (deg)
CFOVY	449	Total seeker field-of-view in yaw (deg)
GSX	450	Seeker quadrant tracker error signal acquisition gain
SEPS	451	Integrator drift rate
GS	456	Quadrant tracker error signal gain
WSL	457	Zero location of integrator lead compensation
WSN	458	Pole location of additional lead-lag compensation
WL2	459	Zero location of additional lead-lag compensation <u>Autopilot Parameters</u>
TDY	866	Minimum time before trajectory pitch program will be switched to terminal homing guidance (sec)
GBIAS	854	Gravity bias program (deg/sec)
HLIMO	850	Pitch command limit (deg)
HLIME	851	Yaw command limit (deg)
QBIAS	852	Pitch rate command bias (deg/sec)
RBIAS	853	Yaw rate command bias (deg/sec)
GZ	867	Pitch navigation guidance filter gain
GY	855	Yaw navigation guidance filter gain
WP1	861	Complex pole of roll control filter (rad/sec)
DP1	862	Damping coefficient of roll control filter
TAUZ	863	Pitch navigation filter pole (rad/sec)
TAUY	864	Yaw navigation filter, pole (rad/sec)

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
HLIMP	865	Roll command limit (deg)
WQ1	871	Pitch and yaw compensation filter complex pole (rad/sec)
DQ1	872	Pitch and yaw compensation filter damping coefficient
TAUL	877	Pitch and yaw navigation guidance filter zero (rad/sec)
		<u>Acuator Parameters</u>
BDP	1231	Roll fin setting (deg)
BDQ	1232	Pitch fin setting (deg)
BDR	1233	Yaw fin setting (deg)
WDELT	1143	Actuator rate limit (deg/sec)
GDELT	1144	Actuator pole (rad/sec)
		<u>Optional Seeker Models - S2, S3</u>
KQ1	545	Pitch channel gains
KQ2	547	
KQ3	549	
KQ5	551	
KQ6	553	
KQ7	555	
KQ8	557	
KQ10	559	
KQ11	561	
KQ12	563	
KR1	546	
KR2	548	
KR3	550	Yaw channel gains
KR5	552	
KR6	554	
KR7	556	
KR8	558	
KR10	560	
KR11	562	

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
DR12	564	
WTQ1	573	
WTQ2	575	
WGQ1	577	
WGQ3	581	
WGQ4	583	Pitch channel frequencies
WGQ5	585	
WGQ6	587	
WRQ2	591	
WRQ4	595	
WTR1	574	
WTR2	576	
WGR1	578	
WGR3	582	
WGR4	584	Yaw channel frequencies
WGR5	586	
WGR6	588	
WRR2	592	
WRR4	596	
RCL	597	Rate command limit in pitch and yaw
TCLQ	598	Torque command limit in pitch
TCLR	599	Torque command limit in yaw
JI	565	Moment of inertial of inner gimbal
JO	566	Moment of inertia of outer gimbal
GEOCS	497	Rate gyro gain to autopilot, pitch and yaw
FRI	567	Inner gimbal friction coefficient (in.-oz)
FRO	568	Outer gimbal friction coefficient (in.-oz)
FFOV	604	Blind range decimal percent field-of-view
TARHT	601	Target height (ft)
TARWD	602	Target width (ft)

TABLE 73. (Continued)

Fortran Symbol	C Index	Definition
TAU	600	Seeker sample period (sec)
TLAG	606	Optical contrast seeker transport lag (sec)
WPTO	1738	Tipoff rate (deg/sec)
AMP2	1742	Peak amplitude of pitch moment forcing function (ft/lb)
AMP1	1746	Peak amplitude of yaw moment forcing function (ft/lb)
VIB	626	Launch transient vibration flag (pitch and yaw only): 0 - no vibration 1 - run with vibration
<u>Optional Seeker Model - S4</u>		
DT	446	Laser designator pulse repetition rate (sec)
GS	456	Detector output gain
SEPS	451	
SWP	452	Sprint restraining torque constant
WSL	457	Lead integral compensation zero (rad/sec)
WSN	458	Platform compensation role (rad/sec)
WL2	459	Platform compensation zero (rad/sec)
CROSS	506	Gimbal cross-coupling coefficient
BLUR	519	Diameter of laser spot on seeker detector (deg)
CKNULL	523	Proportionality constant to 0 null
STOTSW	524	Digital to linear switching point
STOTMX	525	Detector output limiter (deg/sec)
RDES	526	Designator range (ft)
HEES	527	Designator altitude (ft)
RVIS	529	Visibility (statue mi)
CPT	530	Target reflectivity
ETHR	531	Threshold energy density at seeker operative (J/km^2)
EDES	532	Laser designator energy
WCZ	500	Guidance filter natural frequency (rad/sec)
WF	502	
BF	505	

TABLE 73. (Concluded)

Fortran Symbol	C Index	Definition
CZETA	507	Guidance filter damping coefficient
SGBIAS	509	Seeker g-bias (deg/sec)
WCN	518	Guidance filter pole (rad/sec)
WCL	510	Guidance filter zero (rad/sec)
SGSTOT	511	Standard deviation of S/T ratio
GSLIM	539	Seeker output rate limits for linear operation

A sample type 3 card placing an initial value of zero into the program variable array at location 367 is shown in Figure 56. The 1 in the reset flag field will cause the variable to be restored to an initial value of zero for subsequent cases.

5. Card Type 4 - Print Variable Selection

The values of up to 50 variables can be reprinted at user specified simulation flight time intervals (CPP is the input print interval variable; see Table 73). The array index of each variable to be printed is entered on a type 4 card. In this case, the variable name is placed in columns 9 through 20 (rather than 3 through 20 as in types 1, 2, and 3 cards), and this name appears in the printout to identify the variable. The print order will correspond to the order of the type 4 cards in the data set.

An example of a type 4 card is shown in Figure 57, indicating that the value in the 352nd location of the variable array is to be printed and is to be identified by the name "PHI MISSILE."

6. Card Type 6 - Data Termination Indicator

This card signals the program that the end of a data set has been encountered. Include one at the end of each data set or one for each Monte Carlo run desired. (Example: for 25 run Monte Carlo set, 25 type 6 cards would be included at the end of the data set.) An example of a type 6 card is shown in Figure 58.

7. Card Type 7 - Print Variable Selection

Plotting options fall into two categories: (a) time history plots and (b) plots of selected pairs of variables. The format is shown in Figure 59 and a description of each data field for the two types of 7-cards follows:

a. Time History Plots, Y versus T

For each 7-card input, one variable (specified by the C-index on the 7-card) will be plotted versus time.

<u>Field</u>	<u>Description</u>
1	Card type (7 for plot variable)
2	Not used
3	Ordinate label
4	C index of variable to be plotted against time
5	Not used.
6	Scale option: 0 - automatic scaling 1 - fixed scale limits
7	Not used
8	Upper limit for fixed scale
9	Lower limit for fixed scale

The time axis is automatically scaled based on the data range of the time array.

b. Paired Plots, Y versus X

Any variable in the C-array may be plotted against any other variable in the C-array. This option requires input of a 3-card (see Section IV. A. 4) to specify the number of paired plots and a 7-card for the abscissa and a 7-card for the ordinate. Thus, one paired plot requires two 7-cards. In addition, the following order must be observed when reading these cards:

- 1) All paired plot 7-cards must precede all time history 7-cards.
- 2) All paired plot variables must be on consecutive 7-cards.
- 3) The abscissa 7-card, X, must be the first 7-card in a paired plot pair.
- 4) The number of paired plots must be specified by 3-card input variable PLOTN2, whose C-index is 1983.

Each variable on the paired plot 7-cards will be plotted versus time (under the first option) before the paired plots are made. These time history plots may be suppressed by inputting PLOTN4 = 1. This option eliminates all time history plots. Therefore, if PLOTN4 = 1 and it is desired to have time history plots, then the time history variable and the variable time (T) will have to be treated as paired plot variables. Additional variables that must be input by 3-card when using the plot capability are listed in Tables 73 through 79.

<u>Field</u>	<u>Description</u>
1	Card type (7 for plot variable)
2	Not used
3	Axis label
4	C-index of plot variable
5	Not used
6	Scale option: 0 - automatic scaling 1 - fixed scale limits, ordinate only, abscissa automatically scaled 2 - fixed scale, both axes
7	Not used
8	Fixed scale upper limit.
9	Fixed scale lower limit

8. Card Type 8-Monte Carlo Input Variables

Card type 8 is used to select an error source for randomization (Figure 60). The error source identified by the 8-card must be one of the variables listed in the Monte Carlo input data tables given at the end of each module section. If the variable is not given in any of the tables, then it may be incorporated into the program by the instructions given in Section III. C. 6. Error sources called out on 8-cards that are not in the program will simply be ignored by the program.

NOTE: One 8-card corresponds to one error source. Thus, an 8-card must be input for each error source to be randomized. If no 8-cards are input, then the run is assumed to be deterministic.

<u>Field</u>	<u>Description</u>
1	Card type (08) for Monte Carlo input)
2	Error source name (information only).
3	C-index of error source
4	Type distribution of error source: 0 - normal 1 - uniform 2 - Y-component spot jitter Correlated normal 3 - Z-component spot jitter (filtered white 4 - wind gusts noise)
5	Type period for time series sampling if input is for time series error source (ignored if field 11 is blank)

<u>Field</u>	<u>Description</u>
	Blank - regular period sampling with period = field 11
	R - sampling period random normal with mean = field 11
6	Standard deviation of sampling period if time series parameter (field 11 not blank) and field 5 = 4
7	Error source standard deviation if normal distribution; an interval multiplier if uniform distribution (if distribution is uniform, the lower error bound will be less than the mean by the product of field 7 and field 8, and the upper bound will be greater than the mean by the product of field 7 and 9)
8	Error source lower bound
9	Error source upper bound
	} In standard deviations from the mean if normal distribution, or as defined by 7, if uniform
10	C-index of location to store random error value (if blank, random error value store in location specified by field 3)
11	Time series sample period if periodic sample rate (field 5 blank), or mean of sample period if random sample rate (field 5 = R)

NOTE: The distinction between an initial error source 8-card and a time series error source 8-card is made by the input in field 11. If field 11 is left blank, the program interprets the 8-card as a time series error source.

9. Card Type 9 - CEPAS Flag and Control Parameter Card

The input card format for the CEPAS control parameter card is shown in Figure 61. The control parameter card must follow a type 9 card as shown in Figure 62. Both of these cards (the type 9 card and control parameter card) must be placed in front of the last type 6 card in the data deck as shown in Figure 63. The multiple case entry point in MAIN step is drawn in Figure 64.

<u>Field</u>	<u>Description</u>	<u>Value</u>
1	Unused	
2	Normal switch	0 - use bivariate normal assumption only if data passes K-S test for normality - use/nonparametric CEP calculation if data fails normality test 1 - use bivariate normal assumption regardless of outcome of K-S test
3	Plot switch	0 - if no printer plots desired 1 - if printer plots of CEP and confidence circles and impact points desired

1	2	3	4	5	6	7
0000	0000	0000	0000	0000	0000	0000
1111	1111	1111	1111	1111	1111	1111
2222	2222	2222	2222	2222	2222	2222
3333	3333	3333	3333	3333	3333	3333
4444	4444	4444	4444	4444	4444	4444
5555	5555	5555	5555	5555	5555	5555
6666	6666	6666	6666	6666	6666	6666
7777	7777	7777	7777	7777	7777	7777
8888	8888	8888	8888	8888	8888	8888
9999	9999	9999	9999	9999	9999	9999

CEPAS CONTROL CARD

ONE	TWO	THREE	FOUR	FIVE	SIX	SEVEN	EIGHT
0000	0000	0000	0000	0000	0000	0000	0000
1111	1111	1111	1111	1111	1111	1111	1111
2222	2222	2222	2222	2222	2222	2222	2222
3333	3333	3333	3333	3333	3333	3333	3333
4444	4444	4444	4444	4444	4444	4444	4444
5555	5555	5555	5555	5555	5555	5555	5555
6666	6666	6666	6666	6666	6666	6666	6666
7777	7777	7777	7777	7777	7777	7777	7777
8888	8888	8888	8888	8888	8888	8888	8888
9999	9999	9999	9999	9999	9999	9999	9999

GENERAL PURPOSE B FIELD

Figure 61. CEPAS control card format.

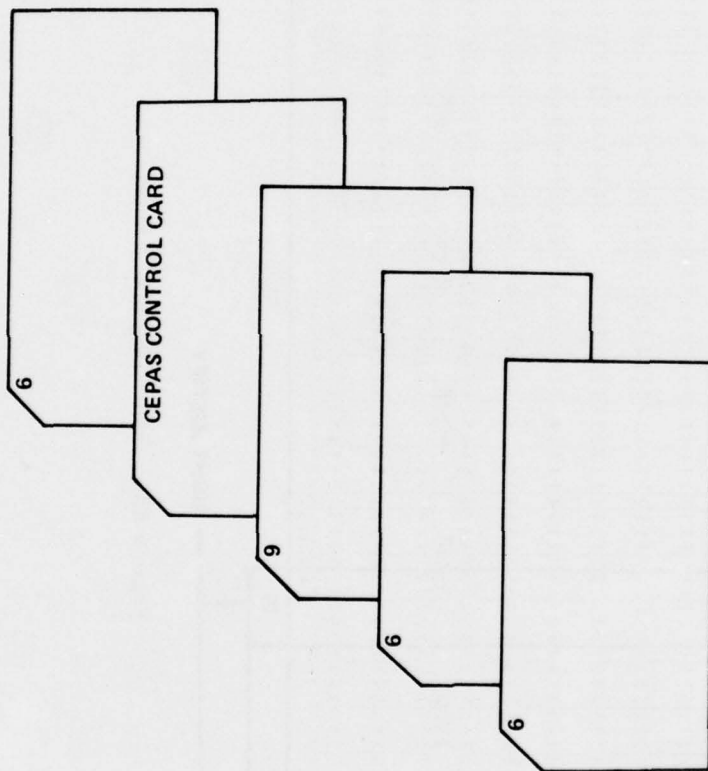


Figure 62. Control parameter card setup.

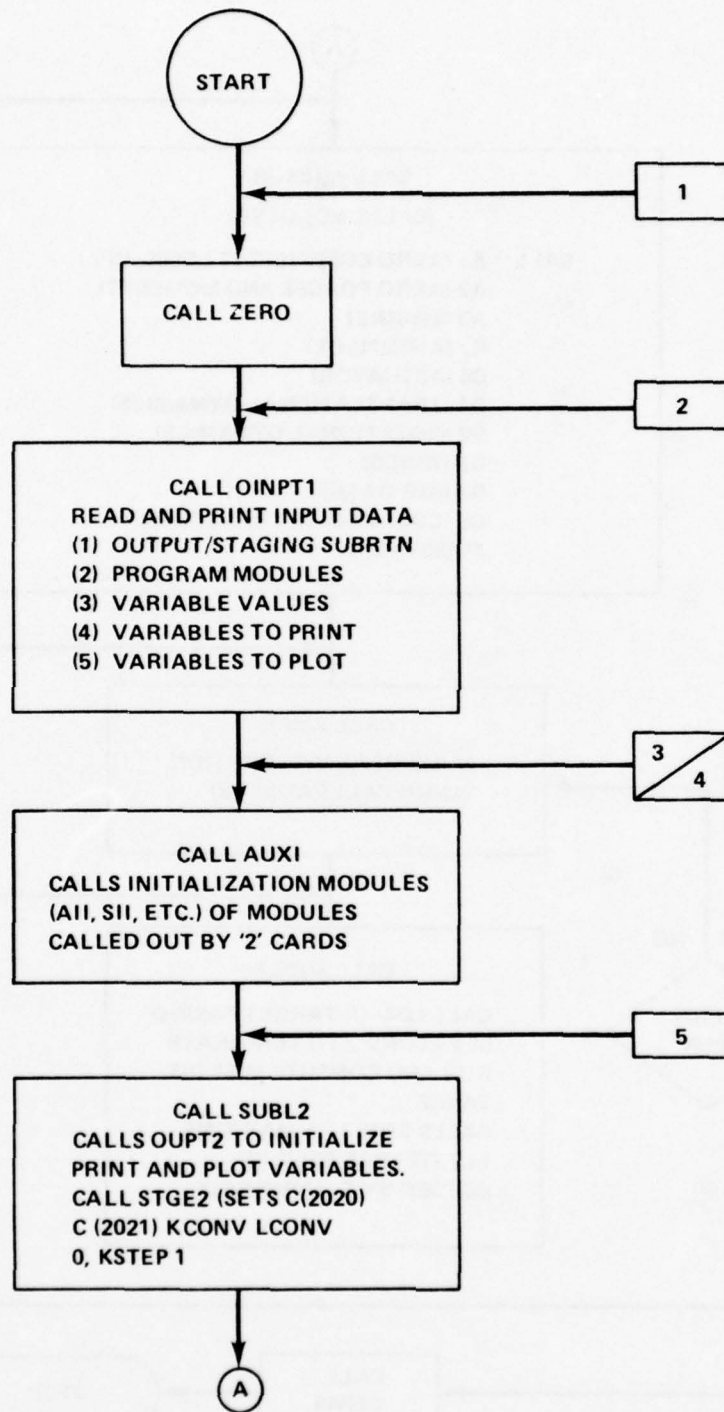


Figure 64. Multiple case entry point in MAIN - step.

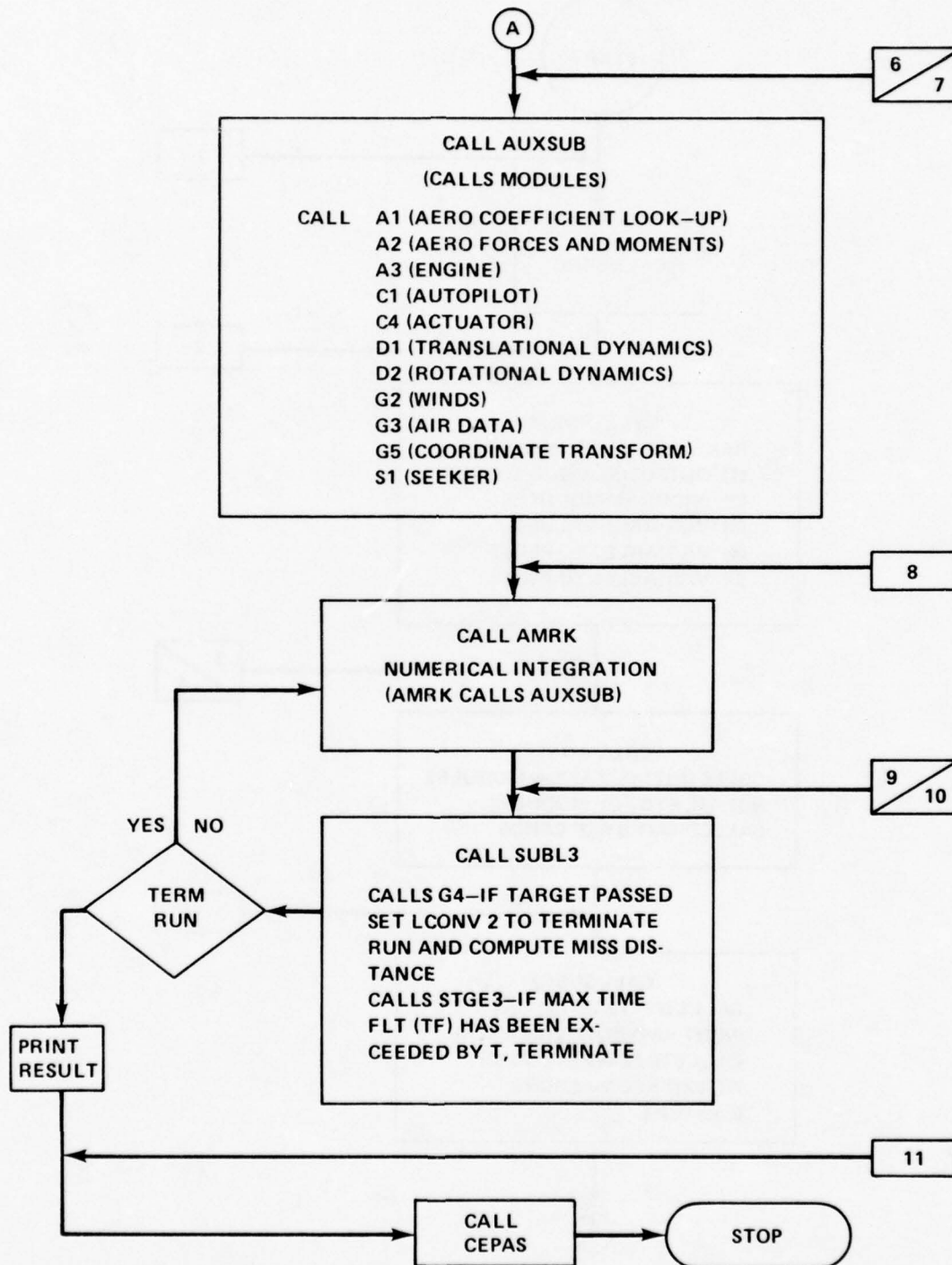


Figure 64. (Continued).

<u>Field</u>	<u>Description</u>	<u>Value</u>
4	Lambda (λ)	Set equal to assumed ratio of 6 DOF program CEP to missile system CEP ($\lambda \geq 0$)
5	Unused	
6	Confidence levels	Enter any combination of available confi- dence levels (99%, 95%, 90%, 80%, 70%) for which a confidence circle radius is desired (left justify; enter in any order)
7	Printer plot scale factor (PSIZE)	0 - Scale printer plots automatically according to data range > 0 - Scale plots according to the number input here

The CEP calculations made by CEPAS are obtained by either parametric statistical methods, assuming an elliptical bivariate normal distribution, or by nonparametric methods, where no specific distribution is assumed. Because more information can generally be obtained (e.g., confidence circles) from a given size sample when the distribution is known, it is advantageous to use the parametric methods when they apply. For this reason, CEPAS automatically subjects the input miss distance data to a normality test [(K-S) test is used] to determine whether to use the parametric or nonparametric methods. If the hypothesis of normally distributed data is not rejected by the K-S test, the parametric method is used; otherwise, the nonparametric method is used. A user option is available which causes the parametric calculations to be used regardless of the outcome of the K-S test. If this option is utilized, however, and the actual underlying population of miss distance coordinates is significantly non-normal, the resulting CEP information will be unreliable.

10. Card Type 10 - Mean and Standard Deviation Selection

The format and a description of each data field for the type 10-cards follows. The 10-cards may appear anywhere in the data deck and may be in any order.

<u>Field</u>	<u>Description</u>
1	Card type (10 for mean and standard deviation)
2	Variable name (information only)
3	C-index of variable

TABLE 74. INPUT DATA OPTIONS FOR INITIAL VALUES

	Unrestricted Inputs	Restricted Inputs					
		No Rail Dynamics		Rail Dynamics Included			
				Direct Fire		Indirect Fire	
		0	0	1	1	2	2
OPTN4	0	0	0	1	1	2	2
OPTN2	0	1	2	1	2	1	2
RXE	X	I	X	I	X	I	X
RYE	X	O	O	O	O	O	O
RZE	X	I	X	I	X	I	X
VXE	X	I	I	I	I	I	I
VYE	X	I	I	I	I	I	I
VZE	X	I	I	I	I	I	I
RTXE	X	O	O	O	O	O	O
RTYE	X	O	O	O	O	O	O
RTZE	X	O	O	O	O	O	O
BPSIO	X	I	I	X	X	X	X
BTHTO	X	I	I	X	X	X	X
BPHIO	X	O	O	O	O	O	O
BTHTG	X	X	X	I	I	X	X
BPSIG	X	X	X	I	I	X	X
RSLANT		X	I	X	I	X	I
BSLOV		X		X		X	
VWXE		X	X	X	X	X	X
VWYE	X	X	X	X	X	X	X
VWZE		X	X	X	X	X	X
(VMAHC)* (VMWTE)		X	X	X	X	X	X

X - denotes variables that must be specified by input data.

I - denotes variables that are computed internally.

O - denotes variables that are either set to zero initially or will be computed as zero.

*Input VMACH if OPTN6 = 0; input VMWTE if OPTN6 = 1.

TABLE 75. WIND OPTION - OPTNW = 1

Fortran Symbol	C Index	Definition
BPSIW	51	Wind direction angle between wind velocity vector and negative X_E -axis (deg)
WTE	52	Wind speed with respect to the earth (steady horizontal winds only) (ft/sec)

NOTE: If wind option OPTNW = 1 is input, the initial value of the components of the wind (VWXE, VWYE, VWZE) must be input also.

TABLE 76. THRUST MISALIGNMENT OPTION - QNALGN = 1

Fortran Symbol	C Index	Definition
BALPHT	1401	Thrust offset angle (α_T) measured from a line parallel to the X_B -axis and the thrust (deg)
BPHIT	1402	Thrust offset angle (ϕ_T) measured from the plane parallel to the X_B - Z_B plane to the plane containing the thrust and the line parallel to the X_B -axis (deg)
RFXCG	1313	Thrust offset along X_B -axis (ft)
RFYCG	1314	Thrust offset along Y_B -axis (ft)
RFZCG	1315	Thrust offset along Z_B -axis (ft)

TABLE 77. ENGINE BURNOUT SWITCH - QBURN - 1

Fortran Symbol	C Index	Definition
WP	1739	Initial roll rate about X_B -axis (deg/sec)
WQ	1743	Initial pitch rate about Y_B -axis (deg/sec)
WR	1747	Initial yaw rate about Z_B -axis (deg/sec)
BALPHA	367	Initial vertical angle of attack (α , deg)
BALPHY	368	Initial sideslip angle of attack (β , deg)
BPHIP	370	Initial aerodynamic roll angle (ϕ' , deg)

TABLE 78. TARGET MOTION OTTION - OPTARG = 1

Fortran Symbol	C Index	Definition
ATHRST	1629	Magnitude of the target acceleration vector (g)
ATURNT	1630	Scaling factor for the angular rotation rate of the target radius vector (g)
BGAMT	1631	Elevation angle of target, measured from the horizontal plane to the target position vector (deg)

TABLE 79. MONTE CARLO INPUTS

Fortran Symbol	C Index	Definition
RNSTRT	3511	Random number generator starting value. The nearest odd integer greater than or equal to RSSTRT will be used. (Changing RNSTRT will cause a different random number sequence to be used)
SIGSPOT	1581	Expected standard deviation of spot jitter output (ft)
SIGU	54	Expected standard deviation of the wind gust output (based on wind direction and missile direction being colinear)
QNALGN	1403	Engine misalignment switch. Set to 1 to compute misalignment component value if a thrust misalignment 8 card is input
VWTE	52	(See Table 2.8 for VWTE input when a wind gusts 8 card is input)

B. Output

1. Introduction

The program provides several print and plot outputs. Some of the print outputs occur automatically. The remaining print outputs and the plot outputs are user options. A brief discussion and an example of each output is included in the paragraphs which follow.

2. Automatic Printouts

a. Input Conditions

The input data cards for each data set are printed out in card format at the end of the input phase for each case. An example is shown in Table 80.

b. Monte Carlo Initial Conditions

The Monte Carlo initial conditions are given in the listing which follows.

MONTE-CARLO INITIAL CONDITIONS					
C-INDEX	MC-VALUE	MEAN	DISTRIBUTION	LOWER BOUND	UPPER BOUND
52	-4.861	0.000	NORMAL	-3.000	3.000
51	54.903	0.000	UNIFORM	0.000	360.000
1247	.339	0.000	UNIFORM	-1.000	1.000
1248	-4.34	0.000	UNIFORM	-1.000	1.000
1249	-.091	0.000	UNIFORM	-1.000	1.000
1253	-.254	0.000	UNIFORM	-1.000	1.000

The headings are defined as follows:

- 1) C Index - Subscript number locating the Monte Carlo.
- 2) MC Value - Random number returned by MCARLO based on user input distribution.
- 3) Mean - User specified mean value about which MAARLO returns the MC-VALUE.
- 4) Distribution - User input distribution (NORMAL or UNIFORM).
- 5) Lower Bound - User input lower bound of the distribution from which MC-VALUE is selected.
- 6) Upper Bound - User input upper bound of the distribution from which MC-VALUE is selected.

c. Time and Step Size

Simulation time and integration step size are printed before and after the missile exits the launcher rail.

TIME = 0.0020000 STEP SIZE = 2.0000000E-03

d. Front Lug Clears Rail

When the front lug clears the rail, a pitch down moment is present on the missile. Because of the potential significance of this transient, a printout occurs at this point, giving the time that the front lug clears the rail, the velocity of the missile

TABLE 80. PRINTOUT OF INPUT DATA EXAMPLE

INPUT DATA									
1	QU T 2,3	3-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
1	STGL 2,3	4-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	G2-T	23-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	G3-H	24-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	SPUT	36-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	G5-H	26-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	A1-T	2-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	A3-T	4-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	A2-H	3-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	J1-H	17-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	J2-H	18-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	S4	31-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	C1-T	7-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
2	C4-T	10-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	T	2.000000E+01	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	OPTNW	50-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	VWTF	52-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	TF	2.000000E+02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	OPP	2.000000E+00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
8	SPOT JITTER - Z	1581 3	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
8	SPOT JITTER - Y	1580 2	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	AKOAR	837-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	AKOAR	838-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
8	AKOAR	837-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
8	AKOAR	838-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	XE	1515-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
1	APP. ANGLE	571-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
1	BALPHA	357-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
1	BALPHY	358-0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0

relative to the wind (airspeed), the pitch moment, and the magnitude of the separation distance from the rear of the launcher rail to the back of the rear lug. Also printed are the tipoff rates.

FRONT LUG CLEARS RAIL

T = 1.12E-01 REL VEL = 6.57E+01 PITCH MOMENT = -1.20E+02
 RANGO = 3.5352 TIPOFF RATES--ROLL = 0.0 PITCH = -15.5 YAW = -5

e. Rear Lug Clears Rail

A printout, occurring at the time the rear lug clears the rail contains the time, the velocity of the missile relative to the wind (airspeed), and the rail lug force.

REAR LUG CLEARS RAIL T = .1460 REL VEL = 85.656 RAIL FORCE = -55.20
 RANGO = 6.1082

f. Engine Burnout Time

BURNOUT TIME = 3.7532 SEC

g. Maximum Breaklock Value

When using the optional optical contrast seeker, maximum values for breaklock (loss of target image) pitch and yaw are printed. If this seeker is not used, zero is printed for both values.

+++MAX BREAKLOCK VALUE = 0.00000 IN PITCH
 +++MAX BREAKLOCK VALUE = 0.00000 IN YAW

h. Run Number

A count of the current total number of Monte Carlo runs.

RUN NUMBER = 26

i. Monte Carlo Time Series

A list of Monte Carlo time series variables and their values follows each Monte Carlo run.

MONTE CARLO TIME SERIES VALUES

C-INDEX	MEAN	VARIANCE	STD DEV	RMS
1681	-.069	.581	.752	.765
1680	.096	.637	.798	.804

- 1) C Index - Subscript number locating the Monte Carlo variable in the C-array.
- 2) Mean - Calculated mean value of the time series output.
- 3) Variance - Variance of the time series output.
- 4) Standard Deviation - Standard deviation (σ) of the time series output.
- 5) RMS - Root mean square of the time series output.

j. Spot Jitter Values

Values for the maximum and minimum deviations for the Y and Z components of laser designator spot motion are listed. Also, sample spot jitter Y and Z component mean, mean square, and radial RMS are printed.

MAX SPOT Y = 1.52 MIN SPOT Y = -1.03
MAX SPOT Z = 1.19 MIN SPOT Z = -1.35

SAMPLE SPOT JITTER Y-MEAN= .09585 MEAN SQUARE= .80369
SAMPLE SPOT JITTER Z-MEAN= -.06893 MEAN SQUARE= .76510 SPOT RADIAL RMS = 1.18964

k. End Conditions

The three programmed simulation terminations are:
(1) ground impacted with missile to target range greater than 500 ft;
(2) input value of maximum flight time exceeded; and (3) target plane intercepted. When simulation termination occurs due to conditions (1) and (2), no special end condition printouts are generated. When simulation termination is due to target plane intercept, the program prints the following information:

- 1) Miss distance (measured in the intercept plane).
- 2) Flight time at intercept.
- 3) Components of line-of-sight vector at intercept.
- 4) Y and Z components of miss distance (in the intercept plane).
- 5) Values of variables requested on print control type 4 cards.

A sample printout is shown below:

```
MISS DISTANCE = 1.6810804E+00 .
FLIGHT TIME = 3.2203602E+00
RDELX = -8.5689802E-02    RDELX = -6.2013629E-01    RDELZ = 1.5602482E+00
RYFP = -6.2182298E-01    RZFP = 1.5624933E+00
```

3. Optional Printouts

Periodic printouts of variables requested by input (on type 4 cards) occur every CPP seconds, where CPP is an input parameter (Table 80). The variable names input on type 4 cards appear only once, followed by the instantaneous values of the variables. Subsequent interval printouts include only the variable values. A sample is shown in Table 81.

The values of every location in the C-array will be printed for every integration step, for a maximum of (6 DOC) integration steps, where DOC is an input variable. The printouts are unlabeled, containing only the C-array values. Because the printout includes only numerical values, no sample is shown. Mean and standard deviation of selected variables (selected by input on type 10 cards) are printed following terminal conditions printout. A sample follows:

MEAN VARIANCE AND STANDARD DEVIATION		
C-LOCATION	MEAN	STD DEV
571	0.	0.
367	.49103190E+01	.34452543E+01
368	-.18781514E+00	.47258503E+01
357	.12699471E+00	.99612294E+00
358	-.31098493E+01	.62224015E+00
369	.71072849E+01	.26119775E+01

If CEP calculations are requested by input (type 9 card), several groups of optional printout will occur. A table of miss distances and Y and Z components of miss distance is printed first (Table 82). The CEPAS parameter control input data is listed in Table 83.

4. Plots

Example plot outputs resulting from the 7-cards shown in Table 81 are shown in Figures 65 through 67. Figures 65 and 66 are automatic time history plots, while Figure 67 is a paired plot for the two time history plots. If CEP information is computed, then plots of the CEP circle, the confidence circle, and the input miss distance points are generated (Figure 68). These plots are done on the computer printer and not on peripheral plotter.

TABLE 81. EXAMPLE TIME HISTORY PRINTOUT

INPUT DATA

1	GUPT 2.3	3-0	-0.0	-0.	-J.	-0.0000	-0-0.0000
1	STGE 2.3	4-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	G2-T	23-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	33-H	24-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	3PT	38-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	33-H	26-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	A1-T	2-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	A3-T	4-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	12-H	3-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	11-H	17-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	12-H	18-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	11	28-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	11-T	7-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
2	C4-T	21-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	T	2-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	OPTNM	50-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	MTF	52-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	IF	201-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	PP	2015-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JUG	2013-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	DER(1)	2004-0	-0.0	-0.	10E+02 1000000E+01	-0.0000	-0-0.0000
3	JPTN2	3012-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JPTN4	3014-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JPTN6	3016-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	VMACH	214-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	IMETA LOS=M	303-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	PSI LOS-V	304-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JALPHA	302-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JALPHY	308-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JT	440-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JFQVZ	440-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	JFQVY	440-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	ILIMO	801-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	ILIME	801-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	ILIMP	805-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	ILIAS	802-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	ILIAS	803-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	ILIAS	804-0	-0.0	-0.	10E+01 1000000E+01	-0.0000	-0-0.0000
3	AP1	801-0	-0.0	-0.	10E+03 -0.	-0.0000	-0-0.0000
3	JP1	802-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	FOY2	806-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	A11	871-0	-0.0	-0.	10E+03 -0.	-0.0000	-0-0.0000
3	J41	872-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	IAUL	877-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	IAUZ	803-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	IAUY	804-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	J2	807-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JY	805-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JELTPB	1141-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JELTQB	1142-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JELTRB	1142-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	AUETL	1143-0	-0.0	-0.	10E+03 -0.	-0.0000	-0-0.0000
3	UETL	1144-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	JDP	1231-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JUQ	1232-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JUR	1233-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JXERR	1201-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JZERR	1201-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JYERR	1202-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JZERR	1203-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JMERR	1204-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JNERR	1205-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JFARA	1306-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JFLGTH	1307-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JFYCG	1313-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JFYCG	1314-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JFYCG	1315-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JLUG	1316-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JAL	1317-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JVALGN	1403-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JPTH	1404-0	-0.0	-0.	-0.	-0.0000	-0-0.0000
3	JBURN	1405-0	-0.0	-0.	1000000E+01	-0.0000	-0-0.0000
3	JISP	1414-0	-0.0	-0.	10E+03 -0.	-0.0000	-0-0.0000
3	JAT	1415-0	-0.0	-0.	10E+03 -0.	-0.0000	-0-0.0000
3	JWP	1416-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000
3	JDCGF	1418-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JDCGO	1417-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JMIYO	1419-0	-0.0	-0.	10E+01 -0.	-0.0000	-0-0.0000
3	JMIYO	1420-0	-0.0	-0.	10E+02 -0.	-0.0000	-0-0.0000

TABLE 81. (Continued)

3	ALCOG	1-21-0	-0.00	0.	12E+01	-0.	-0.0000	-0-0.0000
3	VXE	1003-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	VYE	1007-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	VZE	1011-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	KE	1015-0	-0.00	0.	12E+01	.1000000E+01	-0.0000	-0-0.0000
3	YE	1019-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	ZE	1023-0	-0.00	0.	12E+02	.1000000E+01	-0.0000	-0-0.0000
3	GRAV	1027-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	JPTARG	1039-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	JOIVE	1006-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	2	1739-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	1	1743-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	4	1747-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	CRAD	1751-0	-0.00	0.	78E+02	-0.	-0.0000	-0-0.0000
3	PHIG	1752-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	THIO	1753-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	PSIO	1754-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	PSIO	1754-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	STEP	2-10-0	-0.00	0.	12E+01	-0.	-0.0000	-0-0.0000
3	PPP	2-15-0	-0.00	0.	12E+01	.1000000E+01	-0.0000	-0-0.0000
3	DER1	2664-0	-0.00	0.	10E+01	.1000000E+01	-0.0000	-0-0.0000
3	KE	1015-0	-0.00	0.	12E+01	.1000000E+01	-0.0000	-0-0.0000
3	CLUCK	445-0	-0.00	0.	12E+01	-0.	-0.0000	-0-0.0000
3	JT	446-0	-0.00	0.	10E+01	-0.	-0.0000	-0-0.0000
3	JOB	447-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	FOVZ	448-0	-0.00	0.	12E+02	-0.	-0.0000	-0-0.0000
3	FOVY	449-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	JOA	450-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	SEPS	451-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	JAP	452-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	CBK	453-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	JO	454-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	JPTNSK	455-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	JS	456-0	-0.00	0.	10E+01	-0.	-0.0000	-0-0.0000
3	ASL	457-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	ASH	458-0	-0.00	0.	10E+02	-0.	-0.0000	-0-0.0000
3	AL2	459-0	-0.00	0.	12E+02	-0.	-0.0000	-0-0.0000
3	ASL	457-0	-0.00	0.	10E+01	-0.	-0.0000	-0-0.0000
3	ASL	457-0	-0.00	0.	00E+02	-0.	-0.0000	-0-0.0000
3	ST	460-0	-0.00	0.		.1000000E+01	-0.0000	-0-0.0000
3	DER1	2664-0	-0.00	0.	10E+01	.1000000E+01	-0.0000	-0-0.0000
3	KE	1015-0	-0.00	0.	10E+01	.1000000E+01	-0.0000	-0-0.0000
3	BETA DEG	308-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	BPS	359-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	POYMC	203-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	ALPHA DEG	367-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3		1-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3		1-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3		1-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3		1-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	BTH	354-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	GAMMA	357-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	RANGE	371-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PHI MISSLE	352-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	R COM	623-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	BZ	12-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	EPS Y	436-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	HLA1R	407-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PSI GIMBAL	431-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	FTHRST	1411-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	FTHRST	1411-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	EPS Z	435-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	HLA2Q	403-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	THETA GIMBAL	427-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	BT	11-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	Q COM	811-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	SPOT JITY	1083-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	RJELY	1036-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	EXX	800-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	AIR SPEED	207-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	YAW FLAP	1233-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PITCH FLAP	1232-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	ROLL FLAP	1231-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	ALTITUDE	209-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	KE	1015-0	-0.00	0.	10E+01	.1000000E+01	-0.0000	-0-0.0000
3	ZE	1023-0	-0.00	0.	10E+03	.1000000E+01	-0.0000	-0-0.0000
3	RANGE	371-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	ALTITUDE	209-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PPP	2005-0	-0.00	0.	10E+01	-0.	-0.0000	-0-0.0000
3	PST	2002-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PLOTIN	1902-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
3	PLOTIN2	1903-0	-0.00	0.	10E+01	-0.	-0.0000	-0-0.0000
3		-0-0	-0.00	0.	-0.	-0.0000	-0-0.0000	-0-0.0000
TIME	.0020100 STEP SIZE				100E-03			

TABLE 81. (Continued)

TIME	BETA DEG	BPS	POYNMC	ALPHA DEG	
				BTH	GAMMAH
	RANGE	PHI MISSLE	R COM	BZ	EPS Y
	WLANR	PSI GIMBAL	FTHRST	FTHRST	EPS Z
	WLANQ	THETA GIMBAL	PV	Q COM	SPOT JITY
	RDELY	RXX	AIR SPEED	YAW FLAP	PITCH FLAP
	ROLL FLAP	ALTITUDE			
.0020000	0.	0.	6.9089499E-06	0.	0.
	0.	0.	0.	0.	0.
	6.5600933E+03	0.	-1.1217513E-01	1.0000000E+03	-3.2529870E-03
	5.1000000E-01	3.2530333E-03	2.8590000E+02	2.8590000E+02	-3.2530362E-03
	5.1000000E-01	-3.0243801E-01	1.0000000E+00	-2.3928811E-02	0.
	0.	6.5309435E+00	7.6297409E-02	-2.0029375E-06	-1.7220392E-03
	-3.4644674E-18	3.5000000E+01			
.1000000	0.	0.	4.0666650E+00	0.	0.
	0.	0.	0.	0.	0.
	6.5573983E+03	0.	-5.0578945E-01	1.0000000E+00	3.2278827E-03
	5.0000000E-01	-3.2278217E-03	2.2000000E+03	2.2000000E+03	-3.0980929E-03
	5.0000000E-01	-3.0891898E-01	1.0000000E+00	-1.0000000E+00	0.
	0.	-8.1253618E+01	5.8528318E+01	-5.7490656E-01	-8.9373930E-01
	-1.7763568E-15	3.5000000E+01			
FRONT LUG CLEARS RAIL T = 1.12E-01 REL VEL = 6.56E+01 PITCH MCMNT = -1.20E+02					
RANGE = 3.5299 TIPOFF RATES--ROLL = 0.0 PITCH = -15.6 YAW = .0					
REAR LUG CLEARS RAIL T = .1460 REL VEL = 85.531 RAIL FORCE = -55.30					
RANGE = 6.0991					
TIME= .1500000 STEP SIZE=	1.2500000E-02				
.2000000	-9.6200540E-03	0.	1.6309476E+01	2.6472564E-01	0.
	0.	0.	0.	0.	-2.5135145E-03
	6.5485209E+03	-1.4701422E-04	-7.1059677E+00	-1.0000000E+00	-9.1811891E-03
	-5.0000000E-01	2.0767625E-03	2.1659259E+03	2.1659259E+03	-8.8509778E-03
	-5.0000000E-01	7.8733268E-01	-1.0000000E+00	-1.5987612E-01	1.9498511E-04
	1.9498511E-04	-7.6682525E+01	1.1721640E+02	-8.6156668E-01	-5.1074979E+00
	6.655588E-06	3.4901545E+01			
.3000000	-4.483619E-02	0.	3.6752247E+01	2.9804319E-01	0.
	0.	0.	0.	0.	5.4924442E-03
	6.5338706E+03	-4.1014492E-03	-9.3714262E+00	-1.0000000E+00	-2.8085353E-02
	-5.0000000E-01	-2.2135342E-02	2.1483333E+03	2.1483333E+03	-2.3883665E-02
	-5.0000000E-01	2.0021364E+00	-1.0000000E+00	-1.0769658E-01	2.6432921E-04
	2.6432921E-04	8.9851397E+01	1.7594799E+02	2.4821423E-01	-7.5536664E+00
	9.5753521E-04	3.4378739E+01			

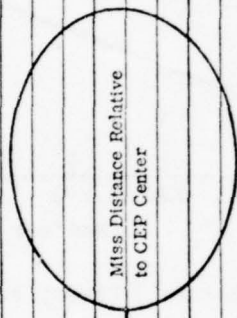
TABLE 81. (Concluded)

TIME	BETA DEG	BPS	PDVNMG	ALPHA DEG	
				STH	GAMMAH
	RANGE	PPI MISSILE	R COM	BZ	EPS Y
	WLAMR	PSI GIMBAL	FTHRST	FTHRST	EPS Z
	WLAMD	THETA GIMBAL	RY	Q COM	SPOT JITY
	POELY	BXX	AIR SPEED	YAW FLAP	PITCH FLAP
	ROLL FLAP	ALTITUDE			
7.700000	1.111311E-01	0.	8.0793640E+02	1.2434822E+00	0.
	0.	0.	0.	0.	6.2890294E-02
	1.9468856E+02	4.0889947E-02	2.9745381E-01	1.0000000E+00	-5.7751414E-02
	-5.0033003E-01	7.6513364E-02	0.	0.	2.4876831E-02
	-1.7763568E-14	-1.3597456E+00	-1.0000000E+00	-8.9618514E-01	-1.0040791E-01
	-1.0043791E-01	-7.1191124E-01	8.2459320E+02	3.1898294E-01	8.3695563E-01
	-2.5071586E-03	7.8785544E+00			
7.800000	2.0411641E-01	0.	8.0295983E+02	1.2601078E+00	0.
	0.	0.	0.	0.	3.9798802E-02
	1.1233916E+02	1.3058831E-01	-1.2245936E+00	1.0000000E+00	1.6929502E-02
	-1.7763568E-14	5.9966074E-02	0.	0.	2.0876783E-02
	-1.7763568E-14	-1.3413099E+00	1.0000000E+00	-3.4541795E+00	-1.7165891E-01
	-1.7165891E-01	-7.1301750E+01	8.2200120E+02	5.6424813E-01	-8.5213405E-01
	-4.2034587E-02	4.6276931E+00			
7.900000	6.1354528E-01	0.	7.9833680E+02	1.2752660E+00	0.
	0.	0.	0.	0.	-2.3718599E-02
	3.0267782E+01	2.9324974E-01	-1.7174043E+00	-1.0000000E+00	-2.3932388E-01
	-1.5530000E+00	4.9777946E-01	0.	0.	1.4769288E-02
	-1.0000000E+00	-1.3229151E+00	-1.0000000E+00	-1.5623704E+00	-2.0024444E-01
	-2.0024444E-01	-7.1306211E+01	8.1943596E+02	2.1137649E-01	-8.6457804E-01
	-1.0639904E-01	1.2846528E+00			
***MAX BREAKLOCK VALUE = 0.0000 IN PITCH					
***MAX BREAKLOCK VALUE = 0.0000 IN YAW					
RUN NUMBER = 1					
MISS DISTANCE = 1.8205676E-01					
FLIGHT TIME = 7.9369581E+00					
ROELX = -1.2198553E-03		ROELY = -1.8020441E-01		ROELZ = 2.5511378E-02	
		RYFP = -1.8025988E-01		RZFP = 2.5578962E-02	
7.937500	5.8775581E-01	0.	7.9620489E+02	1.3024813E+00	0.
	0.	0.	0.	0.	-4.8954043E-02
	4.7949219E-01	2.6198915E-01	-1.4921610E+00	-1.0000000E+00	-1.5775664E+02
	-1.1875000E+00	4.4490916E-01	0.	0.	-1.7652239E+02
	-1.1875000E+00	-1.3793143E+00	-1.0000000E+00	-1.9659238E+00	-1.7984852E-01
	-1.7984852E-01	-8.6424176E+01	8.1847750E+02	8.8791453E-01	-4.4461476E-01
	-8.6424176E-02	7.0070194E-03			
START PLOTTING AT 7.000000					
PLOTTING ENDED AT					

[illegible]

TABLE 83. EXAMPLE CEPAS STATISTICAL OUTPUT

CASE NO. 1	
MEAN=	.535450 DEV= 1.5547
STEPS=	5 YMIN=3.644 YMAX= 3.025
DATA=	.711000 CRITICAL VAL= .270000
CASE NO. 2	
MEAN=	.535450 DEV= 1.5547
STEPS=	5 YMIN=3.644 YMAX= 3.025
DATA=	.711000 CRITICAL VAL= .270000
X-COMPONENT OF MISS-DISTANCE FAIL K-S TEST FOR NORMALITY AT .05000 SIGNIFICANCE LEVEL	
Y-COMPONENT OF MISS-DISTANCE FAIL K-S TEST FOR NORMALITY AT .05000 SIGNIFICANCE LEVEL	
JOINT CEP= 2.087 FOR THE FOLLOWING 25 POINTS	
(-17.0, -2.59)	MISS DIST= 3.15
(-1.18, -2.35)	MISS DIST= 1.83
(-1.77, -2.10)	MISS DIST= 2.85
(-3.02, -1.72)	MISS DIST= 4.25
(-1.03, -.75)	MISS DIST= .80
(-1.09, -.05)	MISS DIST= 2.50
(-1.04, 1.48)	MISS DIST= 1.75
(-1.40, 2.03)	MISS DIST= 1.79
(-1.50, 2.08)	MISS DIST= 2.08
(-3.03, 2.63)	MISS DIST= 3.69
(-1.81, 1.31)	MISS DIST= 1.49
(-2.61, -.03)	MISS DIST= 2.34
(-3.15, -1.17)	MISS DIST= 2.71
(-2.59, 2.26)	MISS DIST= 3.63
(-3.64, -.33)	MISS DIST= 3.12
(-12.4, .77)	MISS DIST= .81
(-.89, -.03)	MISS DIST= .67
(-2.38, -.49)	MISS DIST= 1.84
(-1.31, -.87)	MISS DIST= 1.60
(-2.05, 2.26)	MISS DIST= 3.11
(-2.14, -1.73)	MISS DIST= 2.78
(-.84, .25)	MISS DIST= .42
(-1.06, .52)	MISS DIST= 1.59
(-3.55, 2.26)	MISS DIST= 3.47
CONFIDENCE INTERVAL(S) FOR JOINT CEP	
CONFIDENCE LEVELS	99 (PER CENT)
	2.78 (FT)
MISSILE CEP= 1.461 ASSUMING SIMULATION CEP= 1.00 TIMES THE MISSILE CEP	
CONFIDENCE INTERVAL(S) FOR MISSILE CEP	
CONFIDENCE LEVELS	99 (PER CENT)



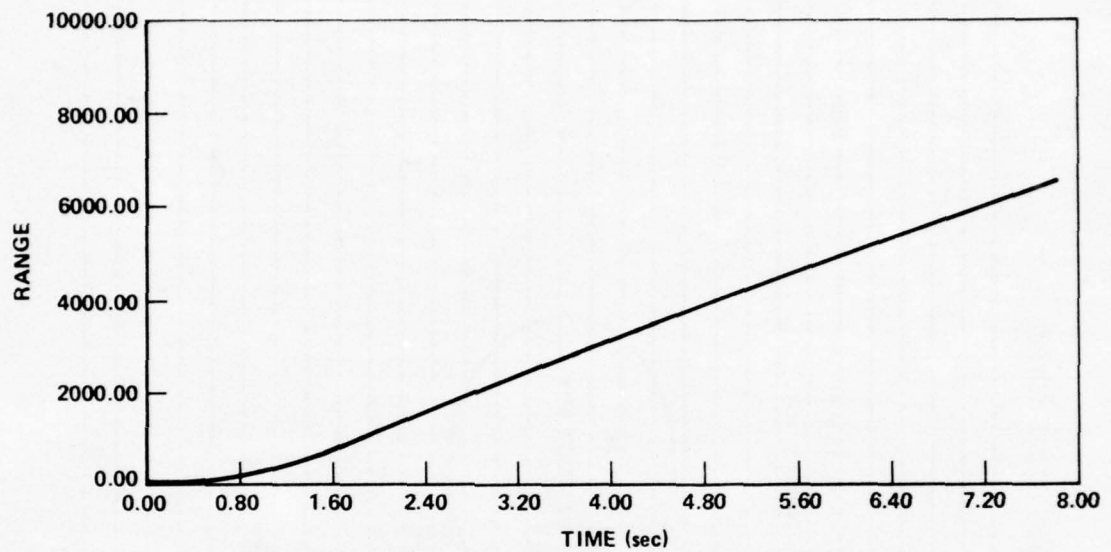


Figure 65. Range time history example plot.

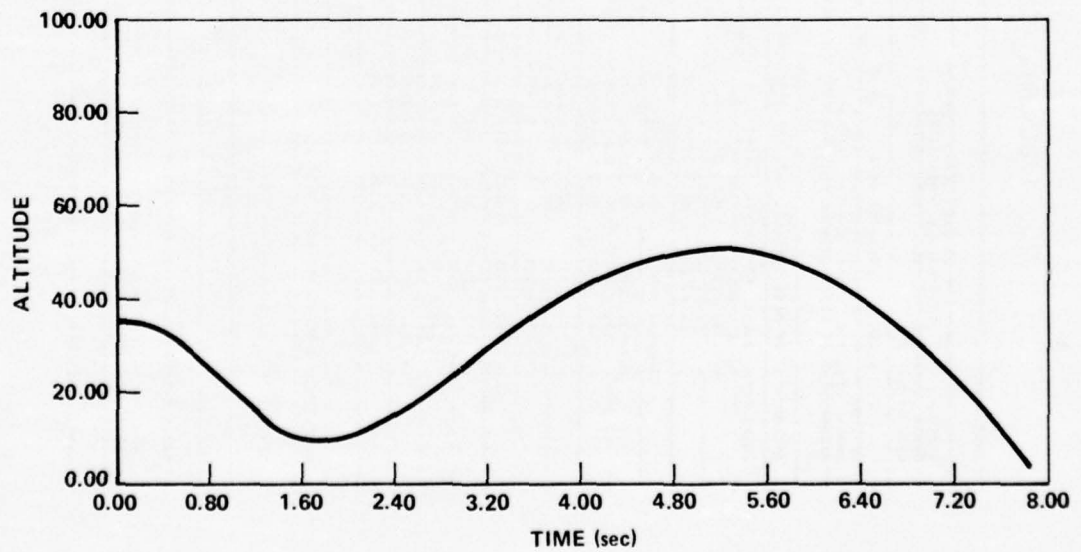


Figure 66. Altitude time history example plot.

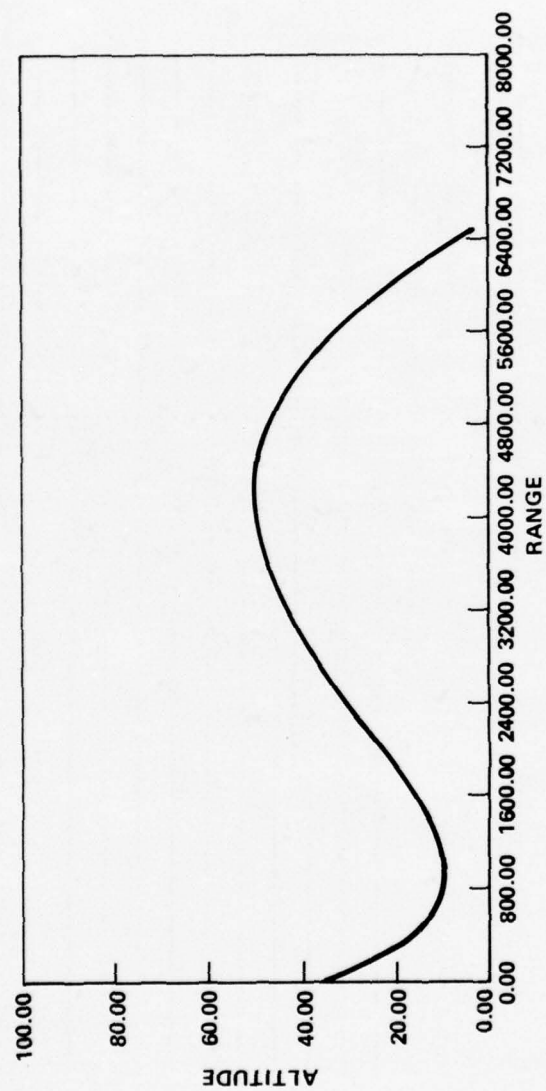
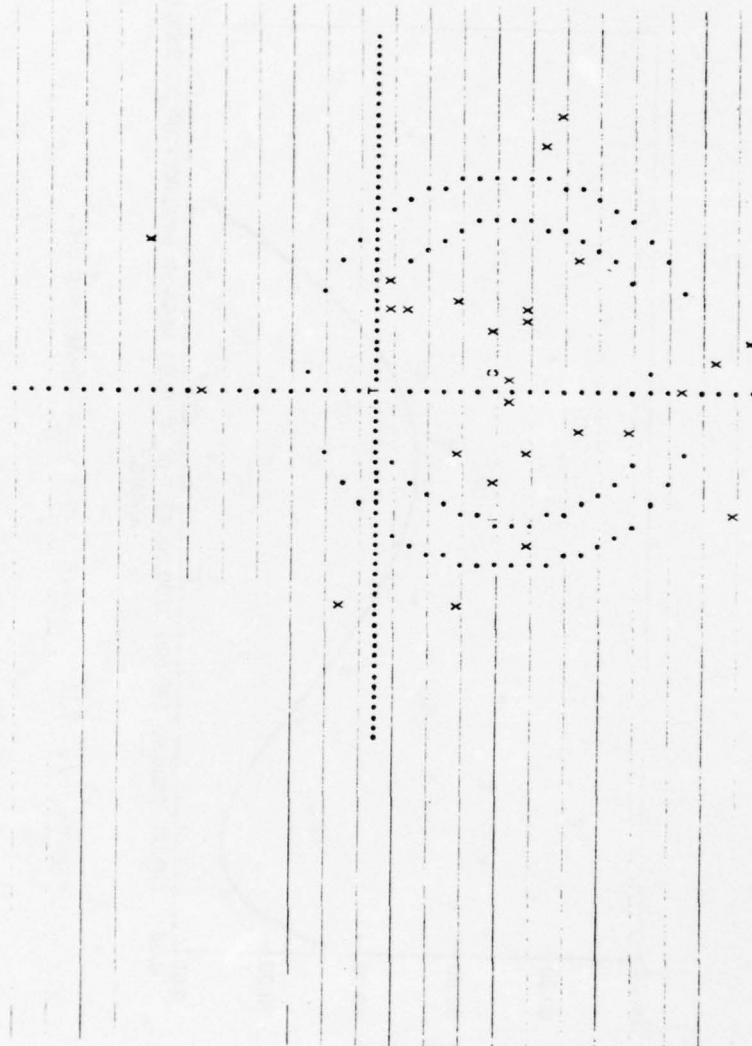


Figure 67. Altitude versus range example plot.

CEP CONFIDENCE CIRCLE FOR $\lambda_{MBDA} = 0.00$

POINTS X
 CEP CIRCLE
 CIRCLE CENTROID C
 TGT CENTER T
 99 PER CENT CONFIDENCE CIRCLE



CEP CENTROID = (.205, -1.174) DIST. FROM TGT CENTER = 1.192 CEP = 1.510
 THE 99 PER CENT CONFIDENCE CIRCLE RADIUS IS 1.949

Figure 68. Plots of the CEP circle, the confidence circle, and the input miss distance points.

TABLE 84. CROSS REFERENCE OF C ARRAY

EQUIVALENCE (C(11),BY)	S1	13
EQUIVALENCE (C(11),BY)	S1	165
EQUIVALENCE (C(11),BY)	S4	44
EQUIVALENCE (C(11),BY	S4	287
EQUIVALENCE (C(12),BZ)	S1	14
EQUIVALENCE (C(12),BZ)	S1	166
EQUIVALENCE (C(12),BZ)	S4	45
EQUIVALENCE (C(11),BY	S4	287
C(13) = 1.	A2	106
C(13) = -1.	S1	73
IF(C(13).LE.0.) GO TO 820	S1	212
C(13) = -1.	S1	213
C(13) = -1.	S4	167
IF(C(13).LE.0.) GO TO 820	S4	359
C(13) = -1.	S4	360
C(13) = -1.	S2	186
IF(C(13).LE.0.)GO TO 1	S2	386
C(13)=-1.	S2	387
IF(C(13).LE.0.)GO TO 1	S3	114
C(13)=-1.	S3	115
EQUIVALENCE (C(17), RDSTOT)	S4	46
C(17) = 0.	S4	99
EQUIVALENCE (C(17),RDSTOT)	S4	254
C(18) = 0.	S4	100
EQUIVALENCE(C(19),PSIZE)	MC7	30
EQUIVALENCE (C(19),PSIZE)	IO	21
EQUIVALENCE (C(21),IBVNSW)	MC7	20
EQUIVALENCE (C(21),IBVNSW)	IO	19
EQUIVALENCE (C(22), IPLOT)	MC7	21
EQUIVALENCE (C(22), IPLOT)	IO	20
EQUIVALENCE (C(23),XLAMB)	MC7	22
EQUIVALENCE (C(23),XLAMB)	IO	22
EQUIVALENCE (C(24), KSSIG)	MC7	23
EQUIVALENCE (C(24), KSSIG)	IO	23
EQUIVALENCE (C(25),CEPSIG)	MC7	24
EQUIVALENCE (C(25),CEPSIG)	IO	24

TABLE 84. (Continued)

EQUIVALENCE (C(31),LCEP)	MC7	32
EQUIVALENCE (C(31), LCEP)	G4	29
DIMENSION SVC(40),SVCT(40),IDISTT(7)	MCARLO	41
EQUIVALENCE (C(50),OPTNW)	G2	54
EQUIVALENCE (C(51),BPSIW)	G2	55
EQUIVALENCE (C(52), VWTE)	G2	7
EQUIVALENCE (C(52),VWTE)	G2	56
EQUIVALENCE (C(54), SIGU)	G2	8
EQUIVALENCE (C(54), SIGU)	G2	62
EQUIVALENCE (C(56), BLU)	G2	9
EQUIVALENCE (C(56), BLU)	G2	63
EQUIVALENCE (C(58), WNDW0)	G2	10
EQUIVALENCE (C(58), WNDW0)	G2	64
EQUIVALENCE (C(59), SLWD)	G2	11
EQUIVALENCE (C(59), SLWD)	G2	65
EQUIVALENCE (C(60), RLW)	MCARLO	4
EQUIVALENCE (C(60), RLW)	G2	12
EQUIVALENCE (C(60), RLW)	G2	66
EQUIVALENCE (C(62), SLW)	G2	13
EQUIVALENCE (C(62), SLW)	G2	67
EQUIVALENCE (C(65),CBPSIW)	G2	14
EQUIVALENCE (C(65),CBPSIW)	G2	68
EQUIVALENCE (C(66),SBPSIW)	G2	15
EQUIVALENCE (C(66),SBPSIW)	G2	69
EQUIVALENCE (C(68), VWTEM)	G2	70
EQUIVALENCE (C(69), GSIGU)	G2	16
EQUIVALENCE (C(69), GSIGU)	G2	71
EQUIVALENCE (C(70), GVMTE)	G2	17
EQUIVALENCE (C(100), VWXE)	G2	18
EQUIVALENCE (C(100),VWXE)	G2	58
EQUIVALENCE (C(0100),VWXE)	G3	8
EQUIVALENCE (C(100),VWXE)	D1	11
EQUIVALENCE (C(101), VWYE)	G2	19
EQUIVALENCE (C(101),VWYE)	G2	59

TABLE 84. (Continued)

EQUIVALENCE (C(0101),VMWE)	G3	9
EQUIVALENCE (C(101),VMWE)	D1	12
EQUIVALENCE (C(102),VMWE)	G2	20
EQUIVALENCE (C(102),VMWE)	G2	60
EQUIVALENCE (C(0102),VMWE)	G3	10
EQUIVALENCE (C(102),VMWE)	D1	13
EQUIVALENCE (C(0200),VMWE)	G3	19
EQUIVALENCE (C(0200),VMWE)	G5	7
EQUIVALENCE (C(0201),VMWE)	G3	20
EQUIVALENCE (C(0201),VMWE)	G5	8
EQUIVALENCE (C(0201),VMWE)	G3	21
EQUIVALENCE (C(0202),VMWE)	G5	9
EQUIVALENCE (C(0202),VMWE)	G3	22
EQUIVALENCE (C(0203),PDYNNC)	A2	21
EQUIVALENCE (C(0203),PDYNNC)	G3	23
EQUIVALENCE (C(0204),VMACH)	A1	12
EQUIVALENCE (C(0204),VMACH)	A2	22
EQUIVALENCE (C(204),VMACH)	D1	14
EQUIVALENCE (C(204),VMACH)	D1	14
EQUIVALENCE (C(204),VMACH)	C5	79
WRITE (6,30)	EXEC	282
EQUIVALENCE (C(367),C(368),C(204),C(369),C(370),C(1117),	G3	24
EQUIVALENCE (C(0205),DRHO)	G3	25
EQUIVALENCE (C(0206),VSOUND)	G3	26
EQUIVALENCE (C(0207),VAIRSP)	G5	10
EQUIVALENCE (C(0207),VAIRSP)	A2	23
EQUIVALENCE (C(0207),VAIRSP)	S4	52
EQUIVALENCE (C(207),VMWE)	G3	6
EQUIVALENCE (C(0208),RHZRO)	G3	27
EQUIVALENCE (C(0209),RH)	S4	118
C(209)=-RZE	S4	249
EQUIVALENCE (C(209),RH)	MC7	25
EQUIVALENCE (C(300),RMISS)	G4	25
EQUIVALENCE (C(300),RMISS)	MC7	28
EQUIVALENCE (C(301),L)	G4	26
EQUIVALENCE (C(301),L)	MC7	29
EQUIVALENCE (C(302),RYF)	G4	27
EQUIVALENCE (C(302),RYF)	MC7	31
EQUIVALENCE (C(303),RZF)	G4	28
EQUIVALENCE (C(303),RZF)	G5	43
EQUIVALENCE (C(0350),BTH)	A2	24
EQUIVALENCE (C(350),BTH)	G5	84
EQUIVALENCE (C(0351),BPSI)	G5	85
EQUIVALENCE (C(0352),BPHI)	G5	86
EQUIVALENCE (C(353),BPHI)	C1	94
EQUIVALENCE (C(353),BPHI)	C3	39
EQUIVALENCE (C(353),BPHI)	G5	87

TABLE 84. (Continued)

EQUIVALENCE (C(354),BTH2)	C3	40
EQUIVALENCE (C(355),BPS1)	G5	88
EQUIVALENCE (C(355),BPS1)	C3	41
EQUIVALENCE (C(0356),VTOTE)	G5	89
EQUIVALENCE (C(0357),BGAMH)	G5	90
EQUIVALENCE (C(357),BGAMH)	G4	13
EQUIVALENCE (C(0358),BGAMV)	G5	91
EQUIVALENCE (C(358),BGAMV)	G4	14
EQUIVALENCE (C(360),BPHIER)	D1	73
EQUIVALENCE (C(361),BTHZER)	D1	74
EQUIVALENCE (C(362),BPSIER)	D1	75
EQUIVALENCE (C(0363),BTHLV)	G5	92
C(363) = 0.	D1	126
EQUIVALENCE (C(0364),BPSLV)	G5	93
C(364) = 0.	D1	127
EQUIVALENCE (C(0365),BLAMV)	G5	94
EQUIVALENCE (C(0366),BLAMH)	G5	95
EQUIVALENCE (C(0367),BALPHA)	G5	96
EQUIVALENCE (C(0367),BALPHA)	A1	13
EQUIVALENCE (C(367),BALPHA)	A3	7
EQUIVALENCE (C(367),BALPHA)	D1	15
WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),	EXEC	282
EQUIVALENCE (C(0368),BALPHY)	G5	97
EQUIVALENCE (C(0368),BALPHY)	A1	14
EQUIVALENCE (C(368),BALPHY)	A3	8
EQUIVALENCE (C(368),BALPHY)	D1	16
WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),	EXEC	282
EQUIVALENCE (C(0369),BALPHP)	G5	98
EQUIVALENCE (C(369),BALPHP)	A1	15
WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),	EXEC	282
EQUIVALENCE (C(0370),BPHIP)	G5	99
EQUIVALENCE (C(0370),BPHIP)	A1	16
EQUIVALENCE (C(370),BPHIP)	A3	9
WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),	EXEC	282
EQUIVALENCE (C(0371),RANGE)	G5	100
EQUIVALENCE (C(371),RANGE)	D1	320
EQUIVALENCE (C(0371),RANGE)	S1	142
EQUIVALENCE (C(371),RANGE)	S4	76
EQUIVALENCE (C(371),RANGE),(C(1615),RXE),(C(1623),RZE)	S4	242
EQUIVALENCE (C(0371),RANGE)	G4	15
EQUIVALENCE (C(371),RANGE)	S2	57
EQUIVALENCE (C(371), RANGE)	S2	330
EQUIVALENCE (C(371), RANGE)	S3	64
EQUIVALENCE (C(0372),RXBA)	G5	101
EQUIVALENCE (C(0372),RXBA)	S1	143
EQUIVALENCE (C(0372),RXBA)	S4	243

TABLE 84. (Continued)

EQUIVALENCE (C(372), RXBA)	\$2
EQUIVALENCE (C(372), RXBA)	\$3
EQUIVALENCE (C(0373),RYBA)	G5
EQUIVALENCE (C(0373),RYBA)	S1
EQUIVALENCE (C(0373),RYBA)	S4
EQUIVALENCE (C(373), RYBA)	\$2
EQUIVALENCE (C(373), RYBA)	\$3
EQUIVALENCE (C(373), RYBA)	G5
EQUIVALENCE (C(0374),RZBA)	S1
EQUIVALENCE (C(0374),RZBA)	S4
EQUIVALENCE (C(0374),RZBA)	\$2
EQUIVALENCE (C(374), RZBA)	\$3
EQUIVALENCE (C(374), RZBA)	G5
EQUIVALENCE (C(380),RANGO)	A2
EQUIVALENCE (C(390),RXL)	G5
EQUIVALENCE (C(391),RYL)	G5
EQUIVALENCE (C(392),RZL)	G5
EQUIVALENCE (C(393),BPH2)	G5
EQUIVALENCE (C(0403),WLMQ)	S1
EQUIVALENCE (C(403),WLMZ)	S4
EQUIVALENCE (C(0403),EZ)	C1
EQUIVALENCE (C(403),WLMQ)	C3
C(403)=0.	\$ C(424)=0.
EQUIVALENCE (C(403), WLMQ)	\$ C(428)=0.
EQUIVALENCE (C(403), WLMQ)	\$2
EQUIVALENCE (C(403), WLMQ)	\$3
EQUIVALENCE (C(0407),WLMR)	S1
EQUIVALENCE (C(407),WLAMY)	S4
EQUIVALENCE (C(0407),EY)	C1
EQUIVALENCE (C(407),WLMR)	C3
C(403)=0.	\$ C(424)=0.
EQUIVALENCE (C(407), WLMR)	\$2
EQUIVALENCE (C(407), WLMR)	\$3
EQUIVALENCE (C(0408),WLQD)	S1
EQUIVALENCE (C(0408),WLQD)	S4
EQUIVALENCE (C(0411),WLQ)	S1
C(411)=0.	\$2
EQUIVALENCE (C(0411),WLQ)	\$3
EQUIVALENCE (C(0411),WLQ)	S4
C(411)=0.	\$2
EQUIVALENCE (C(0411),WLQ)	\$3
EQUIVALENCE (C(0411),WLQ)	S4
EQUIVALENCE (C(0412),WLRO)	S1
EQUIVALENCE (C(0412),WLRO)	S4
EQUIVALENCE (C(0415),WLR)	S1
C(415)=0.	\$2
EQUIVALENCE (C(0415),WLR)	\$3
EQUIVALENCE (C(0415),WLR)	S4

TABLE 84. (Continued)

C(415)=0.		S4	109
EQUIVALENCE (C(0415),WLR)		S4	260
EQUIVALENCE (C(0416),WLQSD)		S1	155
EQUIVALENCE (C(0416),WLQSD)		S4	261
EQUIVALENCE (C(0419),WLQS)		S1	22
C(419)=0.		S1	39
EQUIVALENCE (C(0419),WLQS)		S1	156
EQUIVALENCE (C(0419),WLQS)		S4	55
C(419)=0.		S4	110
EQUIVALENCE (C(0419),WLQS)		S4	262
EQUIVALENCE (C(0420),WLRSD)		S1	157
EQUIVALENCE (C(0420),WLRSD)		S4	263
EQUIVALENCE (C(0423),WLRSD)		S1	23
C(423)=0.		S1	40
EQUIVALENCE (C(0423),WLRSD)		S1	158
EQUIVALENCE (C(0423),WLRSD)		S4	56
C(423)=0.		S4	111
EQUIVALENCE (C(0423),WLRSD)		S4	264
EQUIVALENCE (C(0424),BHTGSD)		S1	159
EQUIVALENCE (C(424), BHTGSD) ,	(C(427), BHTG)	S4	265
\$ C(407)=0.	\$ C(424)=0.	S2	61
EQUIVALENCE (C(424), BHTGD) ,	\$ C(428)=0.	S2	198
EQUIVALENCE (C(424), BHTGD) ,	(C(427), BHTG)	S2	344
EQUIVALENCE (C(427),BHTG)	(C(427), BHTG)	S3	
EQUIVALENCE (C(0427),BHTG)		D1	17
EQUIVALENCE (C(0427),BHTG)		S1	24
EQUIVALENCE (C(0427),BHTG)		S1	160
EQUIVALENCE (C(0427),BHTG)		S4	57
EQUIVALENCE (C(0427),BHTG)		S4	266
EQUIVALENCE (C(424), BHTGD) ,	(C(427), BHTG)	S2	61
EQUIVALENCE (C(424), BHTGD) ,	(C(427), BHTG)	S2	344
EQUIVALENCE (C(424), BHTGD) ,	(C(427), BHTG)	S3	
EQUIVALENCE (C(0428),BPSIGD)		S1	161
EQUIVALENCE (C(0428),BPSIGD)		S4	267
EQUIVALENCE (C(428), BPSIGD) ,	(C(431), BPSIG)	S2	62
\$ C(407)=0.	\$ C(424)=0.	S2	198
EQUIVALENCE (C(428), BPSIGD) ,	(C(431), BPSIG)	S2	345
EQUIVALENCE (C(431),BPSIG)	(C(431), BPSIG)	S3	
EQUIVALENCE (C(0431),BPSIG)		D1	18
EQUIVALENCE (C(0431),BPSIG)		S1	25
EQUIVALENCE (C(0431),BPSIG)		S1	162
EQUIVALENCE (C(0431),BPSIG)		S4	58
EQUIVALENCE (C(0431),BPSIG)		S4	268
EQUIVALENCE (C(428), BPSIGD) ,	(C(431), BPSIG)	S2	62
EQUIVALENCE (C(428), BPSIGD) ,	(C(431), BPSIG)	S2	345
EQUIVALENCE (C(428), BPSIGD) ,	(C(431), BPSIG)	S3	

TABLE 84. (Continued)

10	EQUIVALENCE (C(433)*WLAMQ)	S4	281
10	EQUIVALENCE (C(434)*WLAMR)	S4	282
	EQUIVALENCE (C(0435)*BEP SZ)	S1	169
	EQUIVALENCE (C(435)* BEPSZ)	S4	50
	C(435)=0.	S4	119
	EQUIVALENCE (C(0435)*BEP SZ)	S4	283
	C(435)=0.	S4	199
	\$ C(436)=0.	S2	362
	EQUIVALENCE (C(435)* BEPSZ)	S3	90
	EQUIVALENCE (C(435)* BEPSZ)	S1	170
	EQUIVALENCE (C(0436)*BEP SZ)	S4	51
	EQUIVALENCE (C(436)* BEPSY)	S4	120
	C(436)=0.	S4	284
	EQUIVALENCE (C(0436)*BEP SZ)	S4	199
	C(436)=0.	S2	363
	\$ C(436)=0.	S2	91
	EQUIVALENCE (C(436)* BEPSY)	S3	171
	EQUIVALENCE (C(0437)*WZ)	S1	285
	EQUIVALENCE (C(0437)*WZ)	S4	172
	EQUIVALENCE (C(0438)*WY)	S1	286
	EQUIVALENCE (C(0438)*WY)	S4	173
	EQUIVALENCE (C(0439)*BGDEFI)	S1	122
	EQUIVALENCE (C(445)*RLOCK)	S1	123
	EQUIVALENCE (C(446)*DT)	S1	25
	EQUIVALENCE (C(446)*DT)	S4	39
	EQUIVALENCE (C(446)*DT)	S4	226
	EQUIVALENCE (C(446)*DT)	S4	9
	IF (ABS(C(446))-0.01*AIN T(C(446)/0.01+1.E-6)).LT.1.E-6) TO 30	C3	9
	IF (ABS(C(446))-0.01*AIN T(C(446)/0.01+1.E-6)).LT.1.E-6) TO 30	C3	124
	EQUIVALENCE (C(447)*RDB)	S1	125
	EQUIVALENCE (C(448)*CFOVZ)	S1	126
	EQUIVALENCE (C(449)*CFOVY)	S1	127
	EQUIVALENCE (C(450)*GSX)	S1	128
	EQUIVALENCE (C(451)*SEPS)	S1	26
	EQUIVALENCE (C(451)*SEPS)	S4	227
	EQUIVALENCE (C(451)*SEPS)	S4	19
	EQUIVALENCE (C(452)*SWP)	S1	129
	EQUIVALENCE (C(452)*SWP)	S1	27
	EQUIVALENCE (C(452)*SWP)	S4	59
	EQUIVALENCE (C(452)*SWP)	S4	228
	EQUIVALENCE (C(452)*SWP)	S4	130
	EQUIVALENCE (C(0456)*GS)	S1	28
	EQUIVALENCE (C(0456)*GS)	S4	229
	EQUIVALENCE (C(0456)*GS)	S4	131
	EQUIVALENCE (C(0457)*WSL)	S1	29
	EQUIVALENCE (C(0457)*WSL)	S4	230
	EQUIVALENCE (C(0457)*WSL)	S4	

TABLE 84. (Continued)

EQUIVALENCE (C(0458),WSN)	S1	132
EQUIVALENCE (C(0458),WSN)	S4	30
EQUIVALENCE (C(0458),WSN)	S4	231
EQUIVALENCE (C(0459),WL2)	S1	133
EQUIVALENCE (C(0459),WL2)	S4	31
EQUIVALENCE (C(0459),WL2)	S4	232
EQUIVALENCE (C(460),ST)	S1	135
C(460) = 0.	S4	112
IF (C(460).GT.0.)C(460)=-C(460)	S4	132
IF (C(460).GT.0.)C(460)=-C(460)	S4	132
IF (C(460).GT.0.)C(460)=-C(460)	S4	132
EQUIVALENCE (C(460),ST)	S4	239
C(461)=0.	S1	75
C(461)=1.	S1	80
EQUIVALENCE (C(461),CAGE)	S1	136
C(461) = 0.	S4	169
C(461) = 1.	S4	174
EQUIVALENCE (C(461),CAGE)	C3	42
C(461)=0.	S2	187
C(461)=1.	S2	192
C(462)=0.	S1	76
C(462)=1.	S1	81
EQUIVALENCE (C(462),TKRZ)	S1	137
C(462) = 0.	S4	170
C(462) = 1.	S4	175
EQUIVALENCE (C(462),TKRZ)	C3	43
C(462)=0.	S2	188
C(462)=1.	S2	193
C(463)=0.	S1	77
C(463)=1.	S1	82
EQUIVALENCE (C(463),TKRY)	S1	138
C(463) = 0.	S4	171
C(463) = 1.	S4	176
EQUIVALENCE (C(463),TKRY)	C3	44
C(463)=0.	S2	189
C(463)=1.	S2	194
C(464)=0.	S1	78
C(464)=1.	S1	83
EQUIVALENCE (C(464),TRKZY)	S1	139
C(464) = 0.	S4	172
C(464) = 1.	S4	177
EQUIVALENCE (C(0464),TRKZY)	C1	108
C(464)=0.	S2	190
C(464)=1.	S2	195
EQUIVALENCE (C(465), SDY)	S1	9
EQUIVALENCE (C(465), SDY)	S1	174

TABLE 84. (Continued)

TABLE 84. (Continued)

EQUIVALENCE	(C (490),	GR5),	(C (492),	GR6)	S3
C (491) = 0.					S4
EQUIVALENCE	(C (491),WLZSD)				S4
EQUIVALENCE	(C (489),	G05),	(C (491),	G06)	S2
EQUIVALENCE	(C (489),	G05),	(C (491),	G06)	S2
EQUIVALENCE	(C (489),	G05),	(C (491),	G06)	S3
EQUIVALENCE	(C (490),	GR5),	(C (492),	GR6)	S2
EQUIVALENCE	(C (490),	GR5),	(C (492),	GR6)	S2
EQUIVALENCE	(C (490),	GR5),	(C (492),	GR6)	S3
EQUIVALENCE	(C (493),	DTHCQ),	(C (494),	DTHCR)	S2
EQUIVALENCE	(C (493),	DTHCQ),	(C (494),	DTHCR)	S3
EQUIVALENCE	(C (494),WLZS)				S4
C (494) = 0.					S4
EQUIVALENCE	(C (494),WLZS)				S4
EQUIVALENCE	(C (493),	DTHCQ),	(C (494),	DTHCR)	S2
EQUIVALENCE	(C (493),	DTHCQ),	(C (494),	DTHCR)	S3
EQUIVALENCE	(C (495),WLZSD)				S4
EQUIVALENCE	(C (495),	DTHRGQ),	(C (496),	DTHRGR)	S2
EQUIVALENCE	(C (495),	DTHRGQ),	(C (496),	DTHRGR)	S3
EQUIVALENCE	(C (495),	DTHRGQ),	(C (496),	DTHRGR)	S2
EQUIVALENCE	(C (495),	DTHRGQ),	(C (496),	DTHRGR)	S3
EQUIVALENCE	(C (495),	DTHRGQ),	(C (496),	DTHRGR)	S2
EQUIVALENCE	(C (497),	GE0CS)			S2
EQUIVALENCE	(C (497),	GE0CS)			S2
EQUIVALENCE	(C (497),	GE0CS)			S3
EQUIVALENCE	(C (497),	GE0CS)			S4
C (498) = 0.					S4
EQUIVALENCE	(C (498),WLZSD)				S4
EQUIVALENCE	(C (500),WCZ)		(C (502),WF) , (C (505),BF	S4
EQUIVALENCE	(C (500),WCZ)		(C (502),WF) , (C (505),BF	S4
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S2
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S2
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S3
EQUIVALENCE	(C (501),WLZS)				S4
C (501) = 0.					S4
EQUIVALENCE	(C (501),WLZS)				S4
EQUIVALENCE	(C (501),	DR1),	(C (504),	R1)	S2
EQUIVALENCE	(C (501),	DR1),	(C (504),	R1)	S2
EQUIVALENCE	(C (501),	DR1),	(C (504),	R1)	S3
EQUIVALENCE	(C (500),WCZ)		(C (502),WF) , (C (505),BF	S4
EQUIVALENCE	(C (500),WCZ)		(C (502),WF) , (C (505),BF	S4
EQUIVALENCE	(C (503),WOP)				S4
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S2
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S2
EQUIVALENCE	(C (500),	D01),	(C (503),	Q1)	S3
EQUIVALENCE	(C (504),WRP)				S4
EQUIVALENCE	(C (501),	DR1),	(C (504),	R1)	S2
EQUIVALENCE	(C (501),	DR1),	(C (504),	R1)	S2

TABLE 84. (Continued)

EQUIVALENCE (C(501),	DR1),	(C(504),	R1)	S3	81
EQUIVALENCE (C(500),WCZ) ,	(C(502),WF) ,	(C(505),BF)		S4	21
EQUIVALENCE (C(500),WCZ) ,	(C(502),WF) ,	(C(505),BF)		S4	222
EQUIVALENCE (C(506),CROSS)				S4	10
EQUIVALENCE (C(506),CROSS)				S4	21
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S2	65
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S2	348
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S3	82
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	22
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	223
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	S2	66
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	C2	349
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	S3	83
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	22
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	223
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	22
EQUIVALENCE (C(509),SGBIAS)				S4	34
EQUIVALENCE (C(507),CZETA) ,	(C(508),CKSWP) ,	(C(509),SGBIAS)		S4	223
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S2	65
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S2	348
EQUIVALENCE (C(506),	DQ2),	(C(509),	Q2)	S3	82
EQUIVALENCE (C(518),WCN) ,	(C(510),WCL) ,	(C(511),SGSTOT)		S4	23
EQUIVALENCE (C(518),WCN) ,	(C(510),WCL) ,	(C(511),SGSTOT)		S4	224
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	S2	66
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	S2	349
EQUIVALENCE (C(507),	DR2),	(C(510),	R2)	S3	83
EQUIVALENCE (C(518),WCN) ,	(C(510),WCL) ,	(C(511),SGSTOT)		S4	23
EQUIVALENCE (C(518),WCN) ,	(C(510),WCL) ,	(C(511),SGSTOT)		S4	224
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S2	67
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S2	350
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S3	84
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S2	68
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S2	351
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S3	85
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S2	69
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S2	352
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S3	86
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S2	67
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S2	350
EQUIVALENCE (C(512),	DQ3),	(C(515),	Q3)	S3	84
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S2	68
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S2	351
EQUIVALENCE (C(513),	DR3),	(C(516),	R3)	S3	85
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S2	69
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S2	352
EQUIVALENCE (C(514),	DW0),	(C(517),	W0)	S3	86

TABLE 84. (Continued)

EQUIVALENCE (C(518),WCN)	(C(510),WCL)	(C(511),SGSTOT)	S4	23
EQUIVALENCE (C(518),WCN)	(C(510),WCL)	(C(511),SGSTOT)	S4	224
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S2	70
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S2	353
EQUIVALENCE (C(519),BLUR)			S4	11
EQUIVALENCE (C(519),BLUR)			S4	212
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	71
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	354
EQUIVALENCE (C(520),STOT)			S4	41
EQUIVALENCE (C(520),STOT)			S4	292
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S2	72
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S2	355
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S3	87
EQUIVALENCE (C(521),TKDR)			S4	38
EQUIVALENCE (C(521),TKDR)			S4	293
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S2	70
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S2	353
EQUIVALENCE (C(522),BNULL2)			S4	294
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	71
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	354
EQUIVALENCE (C(523),CKNULL)			S4	12
EQUIVALENCE (C(523),CKNULL)			S4	213
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S2	72
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S2	355
EQUIVALENCE (C(520),DWI)	(C(523),WI)		S3	87
EQUIVALENCE (C(524),STOTSW)			S4	13
EQUIVALENCE (C(524),STOTSW)			S4	43
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S4	214
EQUIVALENCE (C(518),DDQ4)	(C(521),DQ4)	(C(524),Q4)	S2	70
EQUIVALENCE (C(525),STOTMX)			S4	353
EQUIVALENCE (C(525),STOTMX)			S4	14
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	215
EQUIVALENCE (C(519),DDR4)	(C(522),DR4)	(C(525),R4)	S2	71
EQUIVALENCE (C(526),RDES)			S4	15
EQUIVALENCE (C(526),RDES)			S4	216
EQUIVALENCE (C(526),BEPYSV)			S2	81
EQUIVALENCE (C(526),BEPYSV)			S2	366
EQUIVALENCE (C(527),HDES)			S3	94
EQUIVALENCE (C(527),HDES)			S4	16
EQUIVALENCE (C(527),HDES)			S4	217
EQUIVALENCE (C(527),DDQ5)	(C(530),DQ5)	(C(533),Q5)	S2	73
EQUIVALENCE (C(527),DDQ5)	(C(530),DQ5)	(C(533),Q5)	S2	356
EQUIVALENCE (C(528),DDR5)	(C(531),DR5)	(C(534),R5)	S2	74
EQUIVALENCE (C(528),DDR5)	(C(531),DR5)	(C(534),R5)	S2	357

TABLE 84. (Continued)

EQUIVALENCE	(C(529),RVIS)				S4	17
EQUIVALENCE	(C(529),RVIS)				S4	37
EQUIVALENCE	(C(529),RVIS)				S4	218
EQUIVALENCE	(C(529),BEPZSV)				S2	82
EQUIVALENCE	(C(529),BEPZSV)				S2	367
EQUIVALENCE	(C(529),BEPZSV)				S3	95
EQUIVALENCE	(C(530),CPT)				S4	18
EQUIVALENCE	(C(530),CPT)				S4	219
EQUIVALENCE	(C(527), DD05)	(C(530)•	DD5)•	(C(533)•	S2	73
EQUIVALENCE	(C(527), DD05)	(C(530)•	DD5)•	(C(533)•	S2	356
EQUIVALENCE	(C(531),ETHR)				S4	19
EQUIVALENCE	(C(531),ETHR)				S4	222
EQUIVALENCE	(C(528), DD05)	(C(531)•	DR5)•	(C(534)•	S2	74
EQUIVALENCE	(C(528), DD05)	(C(531)•	DR5)•	(C(534)•	S2	357
EQUIVALENCE	(C(532),EDES)				S4	20
EQUIVALENCE	(C(532),EDES)				S4	221
EQUIVALENCE	(C(532),TIMESV)				S2	83
EQUIVALENCE	(C(527), DD05)	(C(530)•	DD5)•	(C(533)•	S2	73
EQUIVALENCE	(C(527), DD05)	(C(530)•	DD5)•	(C(533)•	S2	356
EQUIVALENCE	(C(528), DD05)	(C(531)•	DR5)•	(C(534)•	S2	74
EQUIVALENCE	(C(528), DD05)	(C(531)•	DR5)•	(C(534)•	S2	357
EQUIVALENCE	(C(535),JVIS)				S4	35
EQUIVALENCE	(C(535),JVIS)				S4	295
EQUIVALENCE	(C(536),KUTD)				S4	36
EQUIVALENCE	(C(536),KUTD)				S4	296
EQUIVALENCE	(C(536),KUTD)				S4	75
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	06
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	358
EQUIVALENCE	(C(537), DD06)	(C(540)•	DR6)•	(C(543)•	S2	76
EQUIVALENCE	(C(537), DD06)	(C(540)•	DR6)•	(C(543)•	S2	359
EQUIVALENCE	(C(538), INIT)				S4	47
EQUIVALENCE	(C(538), INIT)				S4	238
EQUIVALENCE	(C(539), GSLIM)				S4	24
EQUIVALENCE	(C(539), GSLIM)				S4	42
EQUIVALENCE	(C(539), GSLIM)				S4	225
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	75
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	358
EQUIVALENCE	(C(537), DD06)	(C(540)•	DR6)•	(C(543)•	S2	76
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	75
EQUIVALENCE	(C(536), DD06)	(C(539)•	DD6)•	(C(542)•	S2	358
EQUIVALENCE	(C(537), DD06)	(C(540)•	DR6)•	(C(543)•	S2	76
EQUIVALENCE	(C(537), DD06)	(C(540)•	DR6)•	(C(543)•	S2	359
EQUIVALENCE	(C(545), KQ1)	(C(573)•	WT01)	(C(543)•	S2	13
EQUIVALENCE	(C(545), KQ1)	(C(573)•	WT01)	(C(543)•	S2	280
EQUIVALENCE	(C(545), KQ1)	(C(573)•	WT01)	(C(543)•	S3	14
EQUIVALENCE	(C(546), KQ1)	(C(574)•	WT01)	(C(543)•	S2	14

TABLE 84. (Continued)

EQUIVALENCE (C(546)).	KR1).	(C(574)).	WTR1)	S2	281
EQUIVALENCE (C(546)).	KR1).	(C(574)).	WTR1)	S3	15
EQUIVALENCE (C(547)).	KQ2).	(C(575)).	WTQ2)	S2	15
EQUIVALENCE (C(547)).	KQ2).	(C(575)).	WTQ2)	S2	282
EQUIVALENCE (C(547)).	KQ2).	(C(575)).	WTQ2)	S3	16
EQUIVALENCE (C(548)).	KR2).	(C(576)).	WTR2)	S2	16
EQUIVALENCE (C(548)).	KR2).	(C(576)).	WTR2)	S2	283
EQUIVALENCE (C(548)).	KR2).	(C(576)).	WTR2)	S3	17
EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WGQ1)	S2	17
EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WGQ1)	S2	284
EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WGQ1)	S3	18
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	S2	18
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	S2	285
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	S3	19
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	S2	19
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	S2	286
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	S3	20
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	S2	20
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	S2	287
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	S3	21
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	S2	21
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	S2	288
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	S3	22
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	S2	22
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	S2	289
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	S3	23
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	S2	23
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	S2	290
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	S3	24
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	S2	24
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	S2	291
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	S3	25
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	S2	25
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	S2	292
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	S3	26
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	S2	26
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	S2	293
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	S3	27
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	S2	27
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	S2	294
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	S3	28
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	S2	28
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	S2	295
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	S3	29
EQUIVALENCE (C(561)).	KQ11).	(C(589)).	WRQ1)	S2	29
EQUIVALENCE (C(561)).	KQ11).	(C(589)).	WRQ1)	S2	296

TABLE 84. (Continued)

EQUIVALENCE (C(561)),	K011),	(C(589)),	WRQ1),	S3	30
EQUIVALENCE (C(562)),	KR11),	(C(590)),	WRR1),	S2	30
EQUIVALENCE (C(562)),	KR11),	(C(590)),	WRR1),	S2	297
EQUIVALENCE (C(562)),	KR11),	(C(590)),	WRR1),	S3	31
EQUIVALENCE (C(563)),	K012),	(C(591)),	WRQ2),	S2	31
EQUIVALENCE (C(563)),	K012),	(C(591)),	WRQ2),	S2	298
EQUIVALENCE (C(563)),	K012),	(C(591)),	WRQ2),	S3	32
EQUIVALENCE (C(564)),	KR12),	(C(592)),	WRR2),	S2	32
EQUIVALENCE (C(564)),	KR12),	(C(592)),	WRR2),	S2	299
EQUIVALENCE (C(564)),	KR12),	(C(592)),	WRR2),	S3	33
EQUIVALENCE (C(565)),	J1),	(C(593)),	WRQ3),	S2	33
EQUIVALENCE (C(565)),	J1),	(C(593)),	WRQ3),	S2	300
EQUIVALENCE (C(565)),	J1),	(C(593)),	WRQ3),	S3	34
EQUIVALENCE (C(566)),	J0),	(C(594)),	WRR3),	S2	34
EQUIVALENCE (C(566)),	J0),	(C(594)),	WRR3),	S2	301
EQUIVALENCE (C(566)),	J0),	(C(594)),	WRR3),	S3	35
EQUIVALENCE (C(567)),	FRI),	(C(595)),	WRQ4),	S2	35
EQUIVALENCE (C(567)),	FRI),	(C(595)),	WRQ4),	S2	302
EQUIVALENCE (C(567)),	FRI),	(C(595)),	WRQ4),	S3	36
EQUIVALENCE (C(567)),	FRI),	(C(595)),	WRQ4),	S2	36
EQUIVALENCE (C(568)),	FR0),	(C(596)),	WRR4),	S2	303
EQUIVALENCE (C(568)),	FR0),	(C(596)),	WRR4),	S2	37
EQUIVALENCE (C(568)),	FR0),	(C(596)),	WRR4),	S3	37
EQUIVALENCE (C(569)),	TUI),	(C(597)),	RCL),	S2	37
EQUIVALENCE (C(569)),	TUI),	(C(597)),	RCL),	S2	304
EQUIVALENCE (C(569)),	TUI),	(C(597)),	RCL),	S3	38
EQUIVALENCE (C(570)),	TU0),	(C(598)),	TCL0),	S2	38
EQUIVALENCE (C(570)),	TU0),	(C(598)),	TCL0),	S2	305
EQUIVALENCE (C(570)),	TU0),	(C(598)),	TCL0),	S3	39
EQUIVALENCE (C(571)),	QERG),	(C(599)),	TCLR),	S2	39
EQUIVALENCE (C(571)),	QERG),	(C(599)),	TCLR),	S2	306
EQUIVALENCE (C(571)),	QERG),	(C(599)),	TCLR),	S3	40
EQUIVALENCE (C(572)),	REFG),	(C(600)),	TAU),	S2	40
EQUIVALENCE (C(572)),	REFG),	(C(600)),	TAU),	S2	307
EQUIVALENCE (C(572)),	REFG),	(C(600)),	TAU),	S3	41
EQUIVALENCE (C(545)),	K01),	(C(573)),	WTQ1),	S2	13
EQUIVALENCE (C(545)),	K01),	(C(573)),	WTQ1),	S2	280
EQUIVALENCE (C(545)),	K01),	(C(573)),	WTQ1),	S3	14
EQUIVALENCE (C(546)),	KR1),	(C(574)),	WTR1),	S2	14
EQUIVALENCE (C(546)),	KR1),	(C(574)),	WTR1),	S2	281
EQUIVALENCE (C(546)),	KR1),	(C(574)),	WTR1),	S3	15
EQUIVALENCE (C(547)),	K02),	(C(575)),	WTQ2),	S2	15
EQUIVALENCE (C(547)),	K02),	(C(575)),	WTQ2),	S2	282
EQUIVALENCE (C(547)),	K02),	(C(575)),	WTQ2),	S3	16
EQUIVALENCE (C(548)),	KR2),	(C(576)),	WTR2),	S2	16
EQUIVALENCE (C(548)),	KR2),	(C(576)),	WTR2),	S2	283
EQUIVALENCE (C(548)),	KR2),	(C(576)),	WTR2),	S3	17

TABLE 84. (Continued)

EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WG01)	17
EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WG01)	284
EQUIVALENCE (C(549)).	KQ3).	(C(577)).	WG01)	18
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	18
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	285
EQUIVALENCE (C(550)).	KR3).	(C(578)).	WGR1)	19
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	19
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	286
EQUIVALENCE (C(551)).	KQ5).	(C(579)).	WGQ2)	20
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	20
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	287
EQUIVALENCE (C(552)).	KR5).	(C(580)).	WGR2)	21
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	21
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	288
EQUIVALENCE (C(553)).	KQ6).	(C(581)).	WGQ3)	22
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	22
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	289
EQUIVALENCE (C(554)).	KR6).	(C(582)).	WGR3)	23
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	23
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	290
EQUIVALENCE (C(555)).	KQ7).	(C(583)).	WGQ4)	24
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	24
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	291
EQUIVALENCE (C(556)).	KR7).	(C(584)).	WGR4)	25
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	25
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	292
EQUIVALENCE (C(557)).	KQ8).	(C(585)).	WGQ5)	26
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	26
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	293
EQUIVALENCE (C(558)).	KR8).	(C(586)).	WGR5)	27
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	27
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	294
EQUIVALENCE (C(559)).	KQ10).	(C(587)).	WGQ6)	28
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	28
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	295
EQUIVALENCE (C(560)).	KR10).	(C(588)).	WGR6)	29
EQUIVALENCE (C(561)).	KQ11).	(C(589)).	WGQ1)	29
EQUIVALENCE (C(561)).	KQ11).	(C(589)).	WGQ1)	296
EQUIVALENCE (C(561)).	KQ11).	(C(589)).	WGQ1)	296
EQUIVALENCE (C(562)).	KR11).	(C(590)).	WRR1)	30
EQUIVALENCE (C(562)).	KR11).	(C(590)).	WRR1)	297
EQUIVALENCE (C(562)).	KR11).	(C(590)).	WRR1)	31
EQUIVALENCE (C(563)).	KQ12).	(C(591)).	WGQ2)	31
EQUIVALENCE (C(563)).	KQ12).	(C(591)).	WGQ2)	298
EQUIVALENCE (C(563)).	KQ12).	(C(591)).	WGQ2)	32
EQUIVALENCE (C(564)).	KR12).	(C(592)).	WRR2)	32

TABLE 84. (Continued)

EQUIVALENCE (C(564),	KR12), (C(592),	WRR2)	S2	299
EQUIVALENCE (C(564),	KR12), (C(592),	WRR2)	S3	33
EQUIVALENCE (C(565),	JI), (C(593),	WRQ3)	S2	33
EQUIVALENCE (C(565),	JI), (C(593),	WRQ3)	S2	300
EQUIVALENCE (C(565),	JI), (C(593),	WRQ3)	S3	34
EQUIVALENCE (C(566),	JO), (C(594),	WRR3)	S2	34
EQUIVALENCE (C(566),	JO), (C(594),	WRR3)	S2	301
EQUIVALENCE (C(566),	JO), (C(594),	WRR3)	S3	35
EQUIVALENCE (C(567),	FRI), (C(595),	WRQ4)	S2	35
EQUIVALENCE (C(567),	FRI), (C(595),	WRQ4)	S2	302
EQUIVALENCE (C(567),	FRI), (C(595),	WRQ4)	S3	36
EQUIVALENCE (C(568),	FRO), (C(596),	WRR4)	S2	36
EQUIVALENCE (C(568),	FRO), (C(596),	WRR4)	S2	303
EQUIVALENCE (C(569),	TUI), (C(597),	RCL)	S3	37
EQUIVALENCE (C(569),	TUI), (C(597),	RCL)	S2	37
EQUIVALENCE (C(570),	TUO), (C(598),	TCLG)	S2	304
EQUIVALENCE (C(570),	TUO), (C(598),	TCLG)	S3	38
EQUIVALENCE (C(570),	TUO), (C(598),	TCLG)	S2	38
EQUIVALENCE (C(571),	QER), (C(599),	TCLR)	S2	305
EQUIVALENCE (C(571),	QER), (C(599),	TCLR)	S3	39
EQUIVALENCE (C(571),	QER), (C(599),	TCLR)	S2	39
EQUIVALENCE (C(571),	QER), (C(599),	TCLR)	S2	306
EQUIVALENCE (C(571),	QER), (C(599),	TCLR)	S3	40
EQUIVALENCE (C(600), IZ)			S1	16
EQUIVALENCE (C(572),	REG), (C(600),	TAU)	S2	40
EQUIVALENCE (C(572),	REG), (C(600),	TAU)	S2	307
EQUIVALENCE (C(572),	REG), (C(600),	TAU)	S3	41
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	47
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	50
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	316
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S3	48
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	47
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	50
EQUIVALENCE (C(601),	TARHT), (C(602),	TARWD)	S2	316
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S3	48
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	49
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	79
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	315
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S3	51
EQUIVALENCE (C(604),	FFOV),		S2	51
EQUIVALENCE (C(604),	FFOV),		S2	317
EQUIVALENCE (C(604),	FFOV),		S3	50
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	49
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	79
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S2	315
EQUIVALENCE (C(603),	RBLOCK), (C(605),	IOCS)	S3	51

TABLE 84. (Continued)

EQUIVALENCE	(C(606),	TLAG)				53
EQUIVALENCE	(C(606),	TLAG)				319
EQUIVALENCE	(C(606),	TLAG)				53
EQUIVALENCE	(C(607),	BRKQ)				371
EQUIVALENCE	(C(607),	BRKQ)				99
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	52
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 80
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 318
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 49
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 52
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 80
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 318
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 49
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 52
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 80
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 318
EQUIVALENCE	(C(608),	TDELAY)	(C(609),	THQ),	(C(610),	THTR) 49
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		91
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		376
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		104
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		91
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		376
EQUIVALENCE	(C(611),	KU)	(C(612),	KU)		104
EQUIVALENCE	(C(613),	KBO)	(C(614),	KBI)		92
EQUIVALENCE	(C(613),	KBO)	(C(614),	KBI)		377
EQUIVALENCE	(C(613),	KBO)	(C(614),	KBI)		105
EQUIVALENCE	(C(613),	KBO)	(C(614),	KBI)		92
EQUIVALENCE	(C(613),	KBO)	(C(614),	KBI)		377
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		93
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		378
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		106
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		93
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		378
EQUIVALENCE	(C(615),	KPI)	(C(616),	KPI)		106
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		94
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		379
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		107
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		94
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		379
EQUIVALENCE	(C(617),	KAO)	(C(618),	KOI)		107
EQUIVALENCE	(C(619),	UCC)	(C(620),	USC)		95
EQUIVALENCE	(C(619),	UCC)	(C(620),	USC)		380
EQUIVALENCE	(C(619),	UCC)	(C(620),	USC)		108
EQUIVALENCE	(C(619),	UCC)	(C(620),	USC)		95
EQUIVALENCE	(C(619),	UCC)	(C(620),	USC)		380

TABLE 84. (Continued)

EQUIVALENCE (C(619),	UCC),	(C(620),	USC)	108
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	96
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	381
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	109
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	96
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	381
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	109
EQUIVALENCE (C(621),	UCCG),	(C(622),	USCG)	33
EQUIVALENCE (C(625),	NCASE),	(C(625),	IBL)	370
EQUIVALENCE (C(625),	LCONV),	(C(625),	IBL)	98
EQUIVALENCE (C(625),	LCONV),	(C(625),	IBL)	33
EQUIVALENCE (C(625),	VIB)	(C(625),	IBL)	51
EQUIVALENCE (C(625),	VIB)	(C(625),	IBL)	77
WRITE (6,600) C(630),PITCH				200
C(630)=0.	\$ C(631)=0.			504
IF (ABS(C(630)),LT.ABS(BRLKQ)) C(630)=BRLKQ				504
IF (ABS(C(630)),LT.ABS(BRLKQ)) C(630)=BRLKQ				227
IF (ABS(C(630)),LT.ABS(BRLKQ)) C(630)=BRLKQ				227
IF (ABS(C(630)),LT.ABS(BRLKQ)) C(630)=BRLKQ				78
WRITE (6,600) C(631),YAW				200
C(630)=0.	\$ C(631)=0.			505
IF (ABS(C(631)),LT.ABS(BRLKR)) C(631)=BRLKR				505
IF (ABS(C(631)),LT.ABS(BRLKR)) C(631)=BRLKR				228
IF (ABS(C(631)),LT.ABS(BRLKR)) C(631)=BRLKR				17
IF (ABS(C(631)),LT.ABS(BRLKR)) C(631)=BRLKR				337
EQUIVALENCE (C(650),TIMESV)				71
EQUIVALENCE (C(650),TIMESV)				180
C(655)=C(2000)-C(2664)				338
EQUIVALENCE (C(656), LOSZ)				72
EQUIVALENCE (C(656), LOSZ)				339
EQUIVALENCE (C(662), LOSY)				73
EQUIVALENCE (C(662), LOSY)				114
EQUIVALENCE (C(800),BPHISD)				115
EQUIVALENCE (C(803),BPHIS)				132
EQUIVALENCE (C(804),EZRSDU)				40
C(807) = 0.				133
EQUIVALENCE (C(807),EZRSP)				134
EQUIVALENCE (C(808),EZRSD)				42
C(811) = 0.				135
EQUIVALENCE (C(811),EZRS)				136
EQUIVALENCE (C(812),EYRSDU)				41
C(815) = 0.				137
EQUIVALENCE (C(815),EYRSP)				138
EQUIVALENCE (C(816),EYRSD)				43
C(819) = 0.				139
EQUIVALENCE (C(819),EYRS)				

TABLE 84. (Continued)

EQUIVALENCE (C(0820),EODCRD)				C1	11	
C(823) = 0.				C1	32	
EQUIVALENCE (C(0823),EODCR)				C1	117	
EQUIVALENCE (C(0824),EVNCRD)				C1	118	
C(827) = 0.				C1	33	
EQUIVALENCE (C(0827),EVNCR)				C1	119	
C(827)=0.				C3	22	
EQUIVALENCE (C(827),BLOSS)				C3	46	
EQUIVALENCE (C(828),EZSDO)				C1	120	
\$ C(829)=0.	\$	C(830)=0.	\$	C(833)=0.	\$	C(834)=0.
EQUIVALENCE (C(0829),AKBO)				C1	98	
\$ C(829)=0.	\$	C(830)=0.	\$	C(833)=0.	\$	C(834)=0.
EQUIVALENCE (C(0830),AKBR)				C1	46	
C(831) = 0.				C1	99	
EQUIVALENCE (C(831),EZSP)				C1	34	
C(831)=0.				C1	121	
EQUIVALENCE (C(831),BLRSS)				C3	23	
EQUIVALENCE(C(832),EZSD)				C3	47	
\$ C(829)=0.	\$	C(830)=0.	\$	C(833)=0.	\$	C(834)=0.
EQUIVALENCE (C(0833),AKPO)				C1	122	
\$ C(829)=0.	\$	C(830)=0.	\$	C(833)=0.	\$	C(834)=0.
EQUIVALENCE (C(0834),AKPR)				C1	46	
C(835) = 0.				C1	101	
EQUIVALENCE (C(835),EZS)				C1	35	
EQUIVALENCE (C(836),EYSDO)				C1	123	
\$ C(837)=0.	\$	C(838)=0.		C1	124	
EQUIVALENCE (C(0837),AKOAQ)				C1	47	
\$ C(837)=0.	\$	C(838)=0.		C1	102	
EQUIVALENCE (C(0838),AKOAR)				C1	47	
C(839) = 0.				C1	103	
EQUIVALENCE (C(839),EYSP)				C1	36	
EQUIVALENCE (C(840),EYSD)				C1	125	
EQUIVALENCE (C(841),UCCG)				C1	126	
EQUIVALENCE (C(841),UCCG)				C1	12	
EQUIVALENCE (C(842),USCG)				C1	104	
EQUIVALENCE (C(842),USCG)				C1	13	
C(843) = 0.				C1	105	
EQUIVALENCE (C(843),EYS)				C1	37	
EQUIVALENCE (C(0848),NHSM)				C1	127	
EQUIVALENCE (C(0850),HLIMO)				C1	9	
EQUIVALENCE (C(0851),HLIME)				C1	76	
EQUIVALENCE (C(0852),GBIAS)				C1	77	
EQUIVALENCE (C(0853),RBIAAS)				C1	78	
EQUIVALENCE (C(0854),GBIAS)				C1	79	
EQUIVALENCE (C(855),GY)				C1	80	
EQUIVALENCE (C(0856),BDELTIC)				C1	82	
				C1	145	

TABLE 84. (Continued)

EQUIVALENCE (C(856)+BDELTC)	C3	56
EQUIVALENCE (C(856)+BDELTC)	C4	87
EQUIVALENCE (C(856)+BDELTC)	C5	80
EQUIVALENCE (C(860)+TDY)	C3	31
EQUIVALENCE (C(0861)+WPI)	C1	83
EQUIVALENCE (C(861)+GBIAS)	C3	32
EQUIVALENCE (C(0862)+DPI)	C1	84
EQUIVALENCE (C(0863)+TAUZ)	C1	85
EQUIVALENCE (C(0864)+TAUY)	C1	86
EQUIVALENCE (C(0865)+HLMP)	C1	87
EQUIVALENCE (C(0866)+TDY)	C1	88
EQUIVALENCE (C(0867)+GZ)	C1	81
EQUIVALENCE (C(0868)+EYRR)	C1	150
EQUIVALENCE (C(0869)+WQC)	C1	147
EQUIVALENCE (C(0870)+WRC)	C1	148
EQUIVALENCE (C(870)+HJK)	C3	33
EQUIVALENCE (C(0871)+WQI)	C1	89
EQUIVALENCE (C(0872)+DOI)	C1	90
EQUIVALENCE (C(0875)+BDELPC)	C1	151
EQUIVALENCE (C(0876)+EZRR)	C1	149
EQUIVALENCE (C(877)+TAUL)	C1	91
EQUIVALENCE (C(878)+GBIAS)	C3	34
EQUIVALENCE (C(879)+GBIAS)	C3	35
EQUIVALENCE (C(880)+EZSSD)	C1	128
EQUIVALENCE (C(880)+BXX)	C3	48
EQUIVALENCE (C(881)+BJJ)	C3	49
EQUIVALENCE (C(882)+BKK)	C3	50
C(883) = 0.	C1	38
EQUIVALENCE (C(883)+EZSS)	C1	129
EQUIVALENCE (C(883)+BXXSS)	C3	51
EQUIVALENCE (C(884)+EYSSD)	C1	130
EQUIVALENCE (C(884)+BJJSS)	C3	52
EQUIVALENCE (C(885)+BKKSS)	C3	53
EQUIVALENCE (C(886)+BTHTS)	C3	54
C(887) = 0.	C1	39
EQUIVALENCE (C(887)+EYSS)	C1	131
EQUIVALENCE (C(887)+BPSIS)	C3	55
EQUIVALENCE (C(0888)+BPISDU)	C1	140
EQUIVALENCE (C(890)+HXX)	C3	36
C(891) = 0.	C1	44
EQUIVALENCE (C(0891)+BPISP)	C1	141
EQUIVALENCE (C(0892)+BPISD)	C1	142
C(895) = 0.	C1	45
EQUIVALENCE (C(0895)+BPIS)	C1	143
EQUIVALENCE (C(1000)+RMISST)	MC7	27
C(1100) = BDELTD(1)	C4	115

TABLE 84. (Continued)

C(1100)=BDELT(1)	C5	135
EQUIVALENCE (C(1101),FELECB)	C4	17
EQUIVALENCE (C(1102),FELECB)	C4	18
EQUIVALENCE (C(1103),BSURF1)	A1	17
EQUIVALENCE (C(1103),BDELT1)	C4	13
BDELT(1)=C(1103)	C4	96
C(1103) = BDELT(1)	C4	109
EQUIVALENCE (C(1103),BDELT1)	C5	15
C(1103)=0.	C5	44
BDELT(1)=C(1103)	C5	93
C(1103)=BDELT(1)	C5	129
C(1104) = BDELT(2)	C4	116
C(1104)=BDELT(2)	C5	136
EQUIVALENCE (C(1105),FELECRB)	C4	19
EQUIVALENCE (C(1106),FMECHB)	C4	20
EQUIVALENCE (C(1107),BSURF2)	A1	18
EQUIVALENCE (C(1107),BDELT2)	C4	14
BDELT(2)=C(1107)	C4	97
C(1107) = BDELT(2)	C4	110
EQUIVALENCE (C(1107),BDELT2)	C5	16
C(1107)=0.	C5	45
BDELT(2)=C(1107)	C5	94
C(1107)=BDELT(2)	C5	130
C(1108) = BDELT(3)	C4	117
C(1108)=BDELT(3)	C5	137
EQUIVALENCE (C(1109),FMECHQB)	C4	21
EQUIVALENCE (C(1110),FMECHRB)	C4	22
EQUIVALENCE (C(1111),BSURF3)	A1	19
EQUIVALENCE (C(1111),BDELT3)	C4	15
BDELT(3)=C(1111)	C4	98
C(1111) = BDELT(3)	C4	111
EQUIVALENCE (C(1111),BDELT3)	C5	17
C(1111)=0.	C5	46
BDELT(3)=C(1111)	C5	95
C(1111)=BDELT(3)	C5	131
C(1112) = BDELT(4)	C4	118
C(1112)=BDELT(4)	C5	138
EQUIVALENCE (C(1115),BSURF4)	A1	20
EQUIVALENCE (C(1115),BDELT4)	C4	16
BDELT(4)=C(1115)	C4	99
C(1115) = BDELT(4)	C4	112
EQUIVALENCE (C(1115),BDELT4)	C5	18
C(1115)=0.	C5	47
BDELT(4)=C(1115)	C5	96
C(1115)=BDELT(4)	C5	132
WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),	EXEC	282

TABLE 84. (Continued)

C C(1118),C(1119),C(1120)	EXEC	283
C C(1118),C(1119),C(1120)	EXEC	283
EQUIVALENCE (C(1120),G1)	C5	8
EQUIVALENCE (C(1120),G1)	C5	72
C C(1118),C(1119),C(1120)	EXEC	283
EQUIVALENCE (C(1124),ZN)	C5	9
EQUIVALENCE (C(1124),ZN)	C5	73
EQUIVALENCE (C(1128),W1)	C5	10
EQUIVALENCE (C(1128),W1)	C5	74
EQUIVALENCE (C(1132),G2)	C5	11
EQUIVALENCE (C(1132),G2)	C5	75
EQUIVALENCE (C(1136),WN)	C5	12
EQUIVALENCE (C(1136),WN)	C5	76
EQUIVALENCE (C(1140),OPTACT)	C4	26
EQUIVALENCE (C(1140),OPTACT)	C5	67
C(1141)=0. \$ C(1142)=0. \$ C(1143)=0.	C5	56
EQUIVALENCE (C(1141),BOP)	C5	68
C(1141)=0. \$ C(1142)=0. \$ C(1143)=0.	C5	56
EQUIVALENCE (C(1142),BDO)	C5	69
EQUIVALENCE (C(1143),WDELTL)	C4	7
EQUIVALENCE (C(1143),WDELTL)	C4	83
C(1141)=0. \$ C(1142)=0. \$ C(1143)=0.	C5	56
EQUIVALENCE (C(1143),BDR)	C5	70
EQUIVALENCE (C(1144),GDELTL)	C4	8
EQUIVALENCE (C(1144),GDELTL)	C4	84
EQUIVALENCE (C(1147),HDEL)	C5	13
EQUIVALENCE (C(1147),HDEL)	C5	71
C(1160)=WDS2D(1)	C5	139
C(1163)=0.	C5	48
WDS2 (1)=C(1163)	C5	97
C(1164)=WDS2D(2)	C5	140
C(1167)=0.	C5	49
WDS2 (2)=C(1167)	C5	98
C(1168)=WDS2D(3)	C5	141
C(1171)=0.	C5	50
WDS2 (3)=C(1171)	C5	99
C(1172)=WDS2D(4)	C5	142
C(1175)=0.	C5	51
WDS2 (4)=C(1175)	C5	100
C(1176)=WDS1D(1)	C5	143
C(1179)=0.	C5	52
WDS1 (1)=C(1179)	C5	101
C(1180)=WDS1D(2)	C5	144
C(1183)=0.	C5	53
WDS1 (2)=C(1183)	C5	102
C(1184)=WDS1D(3)	C5	145

TABLE 84. (Continued)

[illegible]

TABLE 84. (Continued)

EQUIVALENCE (C(1232),BDQ)	C5	20
EQUIVALENCE (C(1233),BDN)	A1	65
EQUIVALENCE (C(1233),BDR)	C4	29
EQUIVALENCE (C(1233),BDR)	C5	21
EQUIVALENCE (C(1234),COCM)	A1	43
EQUIVALENCE (C(1235),CDCN)	A1	31
EQUIVALENCE (C(1240),CL2)	A1	44
EQUIVALENCE (C(1241),CL3)	A1	45
EQUIVALENCE (C(1244),CNPV)	A1	32
EQUIVALENCE (C(1245),CYPV)	A1	33
EQUIVALENCE (C(1247),CMP)	A1	46
EQUIVALENCE (C(1248),CNP)	A1	47
EQUIVALENCE (C(1249),CLR)	A1	48
EQUIVALENCE (C(1250),CZP)	A1	66
EQUIVALENCE (C(1251),CYP)	A1	67
EQUIVALENCE (C(1254), DELTB)	C4	23
EQUIVALENCE (C(1254), DELTB)	C4	88
EQUIVALENCE (C(1255),DELT08)	C4	24
EQUIVALENCE (C(1255),DELT08)	C4	89
EQUIVALENCE (C(1256),DELT08)	C4	25
EQUIVALENCE (C(1256),DELT08)	C4	90
EQUIVALENCE (C(1270),BDMO)	A1	69
EQUIVALENCE (C(1271),BDMO)	A1	68
EQUIVALENCE (C(1300),FXBA)	A2	57
EQUIVALENCE (C(1300),FXBA)	D1	262
EQUIVALENCE (C(1301),FYBA)	A2	58
EQUIVALENCE (C(1301),FYBA)	D1	263
EQUIVALENCE (C(1302),FZHA)	A2	59
EQUIVALENCE (C(1302),FZHA)	D1	264
EQUIVALENCE (C(1303),FMXBA)	A2	60
EQUIVALENCE (C(1303),FMXBA)	D2	77
EQUIVALENCE (C(1304),FMYBA)	A2	61
EQUIVALENCE (C(1304),FMYBA)	D2	78
EQUIVALENCE (C(1305),FMZHA)	A2	62
EQUIVALENCE (C(1305),FMZHA)	D2	79
EQUIVALENCE (C(1306),RFAREA)	A2	9
EQUIVALENCE (C(1307),RFLGTH)	A2	10
EQUIVALENCE (C(1308),RDELCG)	A3	10
EQUIVALENCE (C(1308),RDELCG)	A3	117
EQUIVALENCE (C(1313),RFYCG)	A2	63
EQUIVALENCE (C(1314),RFYCG)	A3	96
EQUIVALENCE (C(1315),RFZCG)	A3	97
EQUIVALENCE (C(1316),RPLUG)	A2	98
EQUIVALENCE (C(1317),RAIL)	G5	11
EQUIVALENCE (C(1317),RAIL)	A2	12

TABLE 84. (Continued)

EQUIVALENCE	(C(1320),FMXTH)	A3	11
EQUIVALENCE	(C(1320),FMXTH)	A3	118
EQUIVALENCE	(C(1320),FMXTH)	A2	35
EQUIVALENCE	(C(1321),FMXTH)	A3	12
EQUIVALENCE	(C(1321),FMXTH)	A3	119
EQUIVALENCE	(C(1321),FMXTH)	A2	36
EQUIVALENCE	(C(1321),FMXTH)	A3	13
EQUIVALENCE	(C(1322),FMZTH)	A3	120
EQUIVALENCE	(C(1322),FMZTH)	A2	37
EQUIVALENCE	(C(1323),FMXLUG)	A2	70
EQUIVALENCE	(C(1324),FMXLUG)	A2	71
EQUIVALENCE	(C(1325),FMZLUG)	A2	72
EQUIVALENCE	(C(1332),CPHAS)	A2	14
EQUIVALENCE	(C(1401),BALPHT)	A3	99
EQUIVALENCE	(C(1402),BPHIT)	A3	100
EQUIVALENCE	(C(1403),QNALGN)	A3	101
EQUIVALENCE	(C(1404),PCFTH)	A3	102
EQUIVALENCE	(C(1405),QBURN)	G5	12
EQUIVALENCE	(C(1405),QBURN)	A3	14
EQUIVALENCE	(C(1405),QBURN)	A3	103
EQUIVALENCE	(C(1405),QBURN)	A2	15
EQUIVALENCE	(C(1409),UDWP)	A3	121
EQUIVALENCE	(C(1410),FTHRST)	A3	122
EQUIVALENCE	(C(1411),FTHX)	A3	15
EQUIVALENCE	(C(1411),FTHX)	A3	123
EQUIVALENCE	(C(1411),FTHX)	A2	38
EQUIVALENCE	(C(1412),FTHY)	A3	16
EQUIVALENCE	(C(1412),FTHY)	A3	124
EQUIVALENCE	(C(1412),FTHY)	A2	39
EQUIVALENCE	(C(1413),FTHZ)	A3	17
EQUIVALENCE	(C(1413),FTHZ)	A3	125
EQUIVALENCE	(C(1413),FTHZ)	A2	40
EQUIVALENCE	(C(1414),CISP)	A3	104
EQUIVALENCE	(C(1415),DWT)	A3	18
EQUIVALENCE	(C(1415),DWT)	A3	105
EQUIVALENCE	(C(1416),DWP)	A3	106
EQUIVALENCE	(C(1417),RDCGO)	A3	107
EQUIVALENCE	(C(1418),RDCGF)	A3	19
EQUIVALENCE	(C(1418),RDCGF)	A3	108
EQUIVALENCE	(C(1419),FMIXF)	A3	20
EQUIVALENCE	(C(1419),FMIXO)	A3	109
EQUIVALENCE	(C(1420),FMIYF)	A3	21
EQUIVALENCE	(C(1420),FMIYO)	A3	110
EQUIVALENCE	(C(1421),RLCGO)	A3	111
EQUIVALENCE	(C(1422),RLCG)	A3	126
EQUIVALENCE	(C(1422),RLCG)	A2	41

TABLE 84. (Continued)

LINE	DESCRIPTION	AMOUNT	DATE	ACCOUNT	DEBIT	CREDIT	BALANCE
133	EQUIVALENCE (C(1496),UIMPD)			A3			
38	C(1499) = 0.			A3			
134	EQUIVALENCE (C(1499),UIMP)			A3			
38	EQUIVALENCE (C(1560), SXPD)			G5			
61	EQUIVALENCE (C(1560), SXPD)			SPOT			
5	EQUIVALENCE (C(1561), RSA)			MCARLO			
39	EQUIVALENCE (C(1561), RX)			G5			
62	EQUIVALENCE (C(1561), RX)			SPOT			
40	EQUIVALENCE (C(1562),GSPOTY)			G5			
11	EQUIVALENCE (C(1562),GSPOTY)			SPOT			
63	EQUIVALENCE (C(1562),GSPOTY)			SPOT			
76	EQUIVALENCE (C(1562),GSPOTY)			D1			
41	EQUIVALENCE (C(1563), SXPD)			G5			
48	EQUIVALENCE (C(1563), SXPD)			SPOT			
64	EQUIVALENCE (C(1563), SXPD)			SPOT			
8	EQUIVALENCE (C(1564),YMC)			MCARLO			
20	EQUIVALENCE (C(1564),YMC)			G4			
9	EQUIVALENCE (C(1565),YMC2)			MCARLO			
21	EQUIVALENCE (C(1565),YMC2)			G4			
42	EQUIVALENCE (C(1566), SXP)			G5			
48	EQUIVALENCE (C(1566), SXP)			SPOT			
65	EQUIVALENCE (C(1566), SXP)			SPOT			
20	EQUIVALENCE (C(1567), SXP)			SPOT			
84	EQUIVALENCE (C(1567), SXP)			D1			
208	WRITE(6,500) C(1567), C(1568), C(1577), C(1578)			I0			
208	IF(C(1680).GT.C(1567)) C(1567) = C(1680)			I0			
21	IF(C(1680).GT.C(1567)) C(1567) = C(1680)			SPOT			
85	C(1568) = 0.			D1			
84	C(1568) = 0.			G4			
209	WRITE(6,500) C(1567), C(1568), C(1577), C(1578)			I0			
209	IF(C(1680).LT.C(1568)) C(1568) = C(1680)			I0			
43	IF(C(1680).LT.C(1568)) C(1568) = C(1680)			G5			
66	EQUIVALENCE (C(1570), SYPD)			SPOT			
6	EQUIVALENCE (C(1571), RSY)			MCARLO			
44	EQUIVALENCE (C(1571), RY)			G5			
67	EQUIVALENCE (C(1571), RY)			SPOT			
45	EQUIVALENCE (C(1572),GSPOTZ)			G5			
12	EQUIVALENCE (C(1572),GSPOTZ)			SPOT			
68	EQUIVALENCE (C(1572),GSPOTZ)			SPOT			
77	EQUIVALENCE (C(1572),GSPOTZ)			D1			
46	EQUIVALENCE (C(1573), SYPD)			G5			
48	EQUIVALENCE (C(1573), SYPD)			SPOT			
69	EQUIVALENCE (C(1573), SYPD)			SPOT			
10	EQUIVALENCE (C(1574),ZMC)			MCARLO			
22	EQUIVALENCE (C(1574),ZMC)			G4			

TABLE 84. (Continued)

EQUIVALENCE (C(1575),ZMC2)	MCARLO	11
EQUIVALENCE (C(1575),ZMC2)	G4	23
EQUIVALENCE (C(1576), SYP)	G5	47
C(1563)=0. \$ C(1566)=0. \$ C(1573)=0. \$ C(1576)=0.	SPOT	48
EQUIVALENCE (C(1576), SYP)	SPOT	70
C(1577) = 0.	SPOT	22
C(1577) = 0.	D1	86
WRITE(6,500) C(1567), C(1568), C(1577), C(1578)	G4	84
IF(C(1681).GT.C(1577)) C(1577) = C(1681)	I0	210
IF(C(1681).GT.C(1577)) C(1577) = C(1681)	I0	210
C(1578) = 0.	SPOT	23
C(1578) = 0.	D1	87
WRITE(6,500) C(1567), C(1568), C(1577), C(1578)	G4	84
IF(C(1681).LT.C(1578)) C(1578) = C(1681)	I0	211
IF(C(1681).LT.C(1578)) C(1578) = C(1681)	I0	211
EQUIVALENCE (C(1579), ZETA)	G5	48
EQUIVALENCE (C(1579), ZETA)	SPOT	14
EQUIVALENCE (C(1579), ZETA)	SPOT	71
EQUIVALENCE (C(1579), ZETA)	D1	79
EQUIVALENCE (C(1580), W0)	G5	49
EQUIVALENCE (C(1580), W0)	SPOT	15
EQUIVALENCE (C(1580), W0)	SPOT	72
EQUIVALENCE (C(1580), W0)	D1	80
EQUIVALENCE (C(1581), SIGSPOT)	SPOT	13
EQUIVALENCE (C(1581), SIGSPOT)	D1	78
EQUIVALENCE (C(1600), VXED)	D1	277
EQUIVALENCE (C(1603), VXE)	G2	21
EQUIVALENCE (C(1603), VXE)	G3	11
EQUIVALENCE (C(1603), VXE)	G5	13
EQUIVALENCE (C(1603), VXE)	D1	32
EQUIVALENCE (C(1603), VXE)	D1	278
EQUIVALENCE (C(1604), VYED)	D1	279
EQUIVALENCE (C(1607), VYE)	G2	22
EQUIVALENCE (C(1607), VYE)	G3	12
EQUIVALENCE (C(1607), VYE)	G5	14
EQUIVALENCE (C(1607), VYE)	D1	33
EQUIVALENCE (C(1607), VYE)	D1	280
EQUIVALENCE (C(1608), VZED)	D1	281
EQUIVALENCE (C(1611), VZE)	G2	23
EQUIVALENCE (C(1611), VZE)	G3	13
EQUIVALENCE (C(1611), VZE)	G5	15
EQUIVALENCE (C(1611), VZE)	D1	34
EQUIVALENCE (C(1611), VZE)	D1	282
EQUIVALENCE (C(1612), RXED)	D1	283
EQUIVALENCE (C(1615), RXE)	G5	16
EQUIVALENCE (C(1615), RXE)	D1	29

TABLE 84. (Continued)

EQUIVALENCE (C(1615),RXE)	D1	284
EQUIVALENCE (C(371),RANGE), (C(1615),RXE), (C(1623),RZE)	S4	76
EQUIVALENCE (C(1615),RXE)	S4	252
EQUIVALENCE (C(1616),RYED)	D1	285
EQUIVALENCE (C(1619),RYE)	G5	17
EQUIVALENCE (C(1619),RYE)	D1	30
EQUIVALENCE (C(1619),RYE)	D1	286
EQUIVALENCE (C(1619),RYE)	S4	251
EQUIVALENCE (C(1620),RZED)	D1	287
EQUIVALENCE (C(1623),RZE)	G3	14
EQUIVALENCE (C(1623),RZE)	G5	18
EQUIVALENCE (C(1623),RZE)	D1	31
EQUIVALENCE (C(1623),RZE)	D1	288
EQUIVALENCE (C(371),RANGE), (C(1615),RXE), (C(1623),RZE)	S4	76
EQUIVALENCE (C(1623),RZE)	S4	250
EQUIVALENCE (C(1624),AXBA)	D1	301
EQUIVALENCE (C(1625),AYBA)	D1	302
EQUIVALENCE (C(1626),AZHA)	D1	303
EQUIVALENCE (C(1627),AGRAV)	A2	16
EQUIVALENCE (C(1627),AGRAV)	D1	252
EQUIVALENCE (C(1628),DMASS)	A3	22
EQUIVALENCE (C(1628),DMASS)	A3	127
EQUIVALENCE (C(1628),DMASS)	A2	64
EQUIVALENCE (C(1628),DMASS)	D1	253
EQUIVALENCE (C(1629),ATHRST)	D1	254
EQUIVALENCE (C(1630),ATURN)	D1	255
EQUIVALENCE (C(1631),BGAMT)	D1	256
EQUIVALENCE (C(1632),VDELX)	D1	304
EQUIVALENCE (C(1633),VDELY)	D1	305
EQUIVALENCE (C(1634),VDELZ)	D1	306
EQUIVALENCE (C(1635),RDELX)	G5	19
EQUIVALENCE (C(1635), RDELX)	D1	48
EQUIVALENCE (C(1635),RDELX)	D1	307
EQUIVALENCE (C(1635),RDELX)	G4	16
RANGE=SQRT(C(1635)*C(1635)+C(1636)*C(1636)+C(1637)*C(1637))	S2	218
RANGE=SQRT(C(1635)*C(1635)+C(1636)*C(1636)+C(1637)*C(1637))	S2	218
EQUIVALENCE (C(1636),RDELY)	G5	20
EQUIVALENCE (C(1636), RDELY)	D1	49
EQUIVALENCE (C(1636),RDELY)	D1	308
EQUIVALENCE (C(1636),RDELY)	G4	17
RANGE=SQRT(C(1635)*C(1635)+C(1636)*C(1636)+C(1637)*C(1637))	S2	218
RANGE=SQRT(C(1635)*C(1635)+C(1636)*C(1636)+C(1637)*C(1637))	S2	218
EQUIVALENCE (C(1637),RDELZ)	G5	21
EQUIVALENCE (C(1637), RDELZ)	D1	50
EQUIVALENCE (C(1637),RDELZ)	D1	309
EQUIVALENCE (C(1637),RDELZ)	G4	18

TABLE 84. (Continued)

RANGE= SORT (C(1635)*C(1635)*C(1636)*C(1636)*C(1637)*C(1637)*C(1637))			
RANGE= SORT (C(1635)*C(1635)*C(1636)*C(1636)*C(1637)*C(1637)*C(1637))	S2		218
EQUIVALENCE (C(1638)*VCLSNB)	S2		218
EQUIVALENCE (C(1639)*OPTARG)	01		310
EQUIVALENCE (C(1639)*OPTARG)	01		19
EQUIVALENCE (C(1640)*VTARGD)	01		257
EQUIVALENCE (C(1643)*VTARG)	01		289
EQUIVALENCE (C(1644)*BPSITD)	01		290
EQUIVALENCE (C(1647)*BPSIT)	01		291
EQUIVALENCE (C(1648)*RTXED)	01		292
EQUIVALENCE (C(1651)*RTXE)	01		293
EQUIVALENCE (C(1651)*RTXE)	G5		22
EQUIVALENCE (C(1651)*RTXE)	01		35
EQUIVALENCE (C(1652)*RTYED)	01		294
EQUIVALENCE (C(1655)*RTYE)	01		295
EQUIVALENCE (C(1655)*RTYE)	G5		23
EQUIVALENCE (C(1655)*RTYE)	01		36
EQUIVALENCE (C(1656)*RTZED)	01		296
EQUIVALENCE (C(1659)*RTZE)	01		297
EQUIVALENCE (C(1659)*RTZE)	G5		24
EQUIVALENCE (C(1659)*RTZE)	01		37
EQUIVALENCE (C(1660)*VTXE)	01		298
EQUIVALENCE (C(1661)*VTYE)	01		311
EQUIVALENCE (C(1662)*VTZE)	01		312
EQUIVALENCE (C(1663)*VDXB)	01		313
EQUIVALENCE (C(1664)*VDYB)	01		314
EQUIVALENCE (C(1665)*RHZRO)	01		315
EQUIVALENCE (C(1665)*VDZB)	01		47
EQUIVALENCE (C(1666)*BLOSV)	01		316
EQUIVALENCE (C(1667)*RSLANT)	01		20
EQUIVALENCE (C(1667)*RSLANT)	01		21
EQUIVALENCE (C(1668)*RXO)	S4		64
EQUIVALENCE (C(1668)*RXO)	G5		25
EQUIVALENCE (C(1669)*RYO)	01		38
EQUIVALENCE (C(1669)*RYO)	G5		26
EQUIVALENCE (C(1670)*RZO)	01		39
EQUIVALENCE (C(1670)*RZO)	G5		27
EQUIVALENCE (C(1671)*VXO)	01		40
EQUIVALENCE (C(1671)*VXO)	G5		28
EQUIVALENCE (C(1672)*VYO)	01		41
EQUIVALENCE (C(1672)*VYO)	G5		29
EQUIVALENCE (C(1673)*VZO)	01		42
EQUIVALENCE (C(1673)*VZO)	G5		30
EQUIVALENCE (C(1674)*VMWTE)	01		43
EQUIVALENCE (C(1676)*ANGX)	01		22
EQUIVALENCE (C(1676)*ANGX)	01		317
EQUIVALENCE (C(1676)*ANGX)	S2		331

TABLE 84. (Continued)

EQUIVALENCE (C(1676), ANGX)	S3	65
EQUIVALENCE (C(1677), ANGY)	D1	318
EQUIVALENCE (C(1677), ANGY)	C1	96
EQUIVALENCE (C(1677), ANGY)	S2	332
EQUIVALENCE (C(1677), ANGY)	S3	66
EQUIVALENCE (C(1678), ANGZ)	D1	319
EQUIVALENCE (C(1678), ANGZ)	C1	97
EQUIVALENCE (C(1678), ANGZ)	S2	333
EQUIVALENCE (C(1678), ANGZ)	S3	67
EQUIVALENCE (C(1680), RSJYMC)	G5	31
EQUIVALENCE (C(1680), RSJYMC)	SPOT	8
EQUIVALENCE (C(1680), RSJYMC)	SPOT	54
EQUIVALENCE (C(1680), RSJYMC)	D1	51
IF (C(1680), GT, C(1567)) C(1567) = C(1680)	I0	208
IF (C(1680), GT, C(1567)) C(1567) = C(1680)	I0	208
IF (C(1680), LT, C(1568)) C(1568) = C(1680)	I0	209
IF (C(1680), LT, C(1568)) C(1568) = C(1680)	I0	209
EQUIVALENCE (C(1681), RSJZMC)	G5	32
EQUIVALENCE (C(1681), RSJZMC)	SPOT	9
EQUIVALENCE (C(1681), RSJZMC)	SPOT	55
EQUIVALENCE (C(1681), RSJZMC)	D1	52
EQUIVALENCE (C(1681), ADIVE)	I0	258
IF (C(1681), GT, C(1577)) C(1577) = C(1681)	I0	210
IF (C(1681), GT, C(1577)) C(1577) = C(1681)	I0	210
IF (C(1681), LT, C(1578)) C(1578) = C(1681)	I0	211
IF (C(1681), LT, C(1578)) C(1578) = C(1681)	I0	211
EQUIVALENCE (C(1682), RSPUTX)	G5	33
EQUIVALENCE (C(1682), RSPUTX)	SPOT	56
EQUIVALENCE (C(1683), FSPOTY)	G5	34
EQUIVALENCE (C(1683), RSPUTY)	SPOT	57
EQUIVALENCE (C(1684), RSPUTZ)	G5	35
EQUIVALENCE (C(1700), CFA11D)	SPOT	58
EQUIVALENCE (C(1703), CFA11)	D2	82
EQUIVALENCE (C(1703), CFA11)	G5	51
EQUIVALENCE (C(1703), CFA11)	D1	265
EQUIVALENCE (C(1703), CFA11)	D2	14
EQUIVALENCE (C(1703), CFA11)	D2	83
EQUIVALENCE (C(1704), CFA12D)	D2	84
EQUIVALENCE (C(1707), CFA12)	G5	52
EQUIVALENCE (C(1707), CFA12)	D1	266
EQUIVALENCE (C(1707), CFA12)	D2	15
EQUIVALENCE (C(1707), CFA12)	D2	85
EQUIVALENCE (C(1708), CFA13D)	D2	86
EQUIVALENCE (C(1711), CFA13)	G5	53
EQUIVALENCE (C(1711), CFA13)	D1	267
EQUIVALENCE (C(1711), CFA13)	D2	16

TABLE 84. (Continued)

87	D2	EQUIVALENCE (C(1711),CFA13)
88	D2	EQUIVALENCE (C(1712),CFA21D)
54	G5	EQUIVALENCE (C(1715),CFA21)
268	D1	EQUIVALENCE (C(1715),CFA21)
17	D2	EQUIVALENCE (C(1715),CFA21)
49	D2	EQUIVALENCE (C(1715),CFA21)
90	D2	EQUIVALENCE (C(1716),CFA22D)
55	G5	EQUIVALENCE (C(1719),CFA22)
269	D1	EQUIVALENCE (C(1719),CFA22)
18	D2	EQUIVALENCE (C(1719),CFA22)
91	D2	EQUIVALENCE (C(1719),CFA22)
2	D2	EQUIVALENCE (C(1720),CFA23D)
92	D2	EQUIVALENCE (C(1723),CFA23)
56	G5	EQUIVALENCE (C(1723),CFA23)
42	A2	EQUIVALENCE (C(1723),CFA23)
270	D1	EQUIVALENCE (C(1723),CFA23)
19	D2	EQUIVALENCE (C(1723),CFA23)
93	D2	EQUIVALENCE (C(1723),CFA23)
94	D2	EQUIVALENCE (C(1724),CFA31D)
57	G5	EQUIVALENCE (C(1727),CFA31)
271	D1	EQUIVALENCE (C(1727),CFA31)
20	D2	EQUIVALENCE (C(1727),CFA31)
95	D2	EQUIVALENCE (C(1727),CFA31)
96	D2	EQUIVALENCE (C(1728),CFA32D)
58	G5	EQUIVALENCE (C(1731),CFA32)
272	D1	EQUIVALENCE (C(1731),CFA32)
21	D2	EQUIVALENCE (C(1731),CFA32)
97	D2	EQUIVALENCE (C(1731),CFA32)
98	D2	EQUIVALENCE (C(1732),CFA33D)
59	G5	EQUIVALENCE (C(1735),CFA33)
43	A2	EQUIVALENCE (C(1735),CFA33)
273	D1	EQUIVALENCE (C(1735),CFA33)
22	D2	EQUIVALENCE (C(1735),CFA33)
99	D2	EQUIVALENCE (C(1735),CFA33)
100	D2	EQUIVALENCE (C(1736),CFA33)
95	C1	EQUIVALENCE (C(1736),CFA33)
334	S2	EQUIVALENCE (C(1736),CFA33)
68	S3	EQUIVALENCE (C(1736),CFA33)
34	A3	EQUIVALENCE (C(1737),CFA33)
46	A2	EQUIVALENCE (C(1737),CFA33)
49	A2	EQUIVALENCE (C(1738),CFA33)
23	A3	EQUIVALENCE (C(1739),CFA33)
44	A2	EQUIVALENCE (C(1739),CFA33)
101	D2	EQUIVALENCE (C(1739),CFA33)
146	S1	EQUIVALENCE (C(1739),CFA33)
246	S4	EQUIVALENCE (C(1739),CFA33)
325	S2	EQUIVALENCE (C(1739),CFA33)

TABLE 84. (Continued)

EQUIVALENCE	(C(1739),	WPI	S3
EQUIVALENCE	(C(1740),	WQD	102
EQUIVALENCE	(C(1740),	WQD)	S2
EQUIVALENCE	(C(1740),	WQD)	335
EQUIVALENCE	(C(1737),	FMX),	S3
EQUIVALENCE	(C(1737),	FMX),	A3
EQUIVALENCE	(C(1737),	FMX),	34
EQUIVALENCE	(C(1737),	FMX),	46
CALL L TRANT, DELT, C(1742), DUM, WQ0, IFLG1, 2)			67
EQUIVALENCE	(C(1742),	AMP2),	A3
EQUIVALENCE	(C(1742),	AMP2),	A2
EQUIVALENCE	(C(1743),	WQ	13
EQUIVALENCE	(C(1743),	WQ)	24
EQUIVALENCE	(C(1743),	WQ)	A3
EQUIVALENCE	(C(1743),	WQ)	45
EQUIVALENCE	(C(1743),	WQ)	A2
EQUIVALENCE	(C(1743),	WQ)	D2
EQUIVALENCE	(C(1743),	WQ)	103
EQUIVALENCE	(C(1743),	WQ)	147
EQUIVALENCE	(C(1743),	WQ)	S1
EQUIVALENCE	(C(1743),	WQ)	247
EQUIVALENCE	(C(1743),	WQ)	S4
EQUIVALENCE	(C(1743),	WQ)	109
EQUIVALENCE	(C(1743),	WQ)	C1
EQUIVALENCE	(C(1743),	WQ)	326
EQUIVALENCE	(C(1743),	WQ)	S2
EQUIVALENCE	(C(1743),	WQ)	S3
EQUIVALENCE	(C(1744),	WRD)	60
EQUIVALENCE	(C(1744),	WRD)	104
EQUIVALENCE	(C(1744),	WRD)	D2
EQUIVALENCE	(C(1744),	WRD)	336
EQUIVALENCE	(C(1737),	FMX),	S3
EQUIVALENCE	(C(1737),	FMX),	70
EQUIVALENCE	(C(1737),	FMX),	34
EQUIVALENCE	(C(1737),	FMX),	A3
EQUIVALENCE	(C(1737),	FMX),	46
CALL L TRANT, DELT, C(1746), DUM, WR0, IFLG2, 1)			66
EQUIVALENCE	(C(1742),	AMP2),	A3
EQUIVALENCE	(C(1742),	AMP2),	A2
EQUIVALENCE	(C(1742),	AMP2),	13
EQUIVALENCE	(C(1747),	WR	25
EQUIVALENCE	(C(1747),	WR)	A3
EQUIVALENCE	(C(1747),	WR)	47
EQUIVALENCE	(C(1747),	WR)	A2
EQUIVALENCE	(C(1747),	WR)	105
EQUIVALENCE	(C(1747),	WR)	D2
EQUIVALENCE	(C(1747),	WR)	148
EQUIVALENCE	(C(1747),	WR)	S4
EQUIVALENCE	(C(1747),	WR)	110
EQUIVALENCE	(C(1747),	WR)	C1
EQUIVALENCE	(C(1747),	WR)	327
EQUIVALENCE	(C(1747),	WR)	S2
EQUIVALENCE	(C(1747),	WR)	61
EQUIVALENCE	(C(1747),	WR)	S3
EQUIVALENCE	(C(1748),	FMIX	26
EQUIVALENCE	(C(1748),	FMIX)	A3
EQUIVALENCE	(C(1748),	FMIX)	128
EQUIVALENCE	(C(1748),	FMIX)	A3
EQUIVALENCE	(C(1748),	FMIX)	48
EQUIVALENCE	(C(1748),	FMIX)	A2
EQUIVALENCE	(C(1748),	FMIX)	65
EQUIVALENCE	(C(1748),	FMIX)	A2
EQUIVALENCE	(C(1749),	FMIY)	70
EQUIVALENCE	(C(1749),	FMIY)	D2
EQUIVALENCE	(C(1749),	FMIY)	A3
EQUIVALENCE	(C(1749),	FMIY)	129
EQUIVALENCE	(C(1749),	FMIY)	A3
EQUIVALENCE	(C(1749),	FMIY)	66
EQUIVALENCE	(C(1749),	FMIY)	A2
EQUIVALENCE	(C(1749),	FMIY)	D2
EQUIVALENCE	(C(1750),	FMIZ)	71
EQUIVALENCE	(C(1750),	FMIZ)	D2
EQUIVALENCE	(C(1750),	FMIZ)	A3
EQUIVALENCE	(C(1750),	FMIZ)	28
EQUIVALENCE	(C(1750),	FMIZ)	A3
EQUIVALENCE	(C(1750),	FMIZ)	130
EQUIVALENCE	(C(1750),	FMIZ)	A3
EQUIVALENCE	(C(1750),	FMIZ)	67
EQUIVALENCE	(C(1750),	FMIZ)	A2
EQUIVALENCE	(C(1751),	CRAD)	72
EQUIVALENCE	(C(1751),	CRAD)	D2
EQUIVALENCE	(C(1751),	CRAD)	60
EQUIVALENCE	(C(1751),	CRAD)	G5
EQUIVALENCE	(C(1751),	CRAD)	A3

TABLE 84. (Continued)

EQUIVALENCE (C(1751), CRAD)	A2	50
EQUIVALENCE (C(1751), CRAD)	D1	23
EQUIVALENCE (C(1751), CRAD)	D1	259
EQUIVALENCE (C(1751), CRAD)	D2	73
EQUIVALENCE (C(1751), CRAD)	S2	56
EQUIVALENCE (C(1751), CRAD)	S2	328
EQUIVALENCE (C(1751), CRAD)	S3	62
EQUIVALENCE (C(1751), CRAD)	D1	44
EQUIVALENCE (C(1752), BPHIO)	D2	7
EQUIVALENCE (C(1752), BPHIO)	D1	45
EQUIVALENCE (C(1753), BTHIO)	D2	8
EQUIVALENCE (C(1753), BTHIO)	D1	46
EQUIVALENCE (C(1754), BPSIO)	D2	9
EQUIVALENCE (C(1754), BPSIO)	D2	74
EQUIVALENCE (C(1755), A021)	G5	57
EQUIVALENCE (C(1755), A021)	D1	24
EQUIVALENCE (C(1755), A021)	D2	75
EQUIVALENCE (C(1756), A022)	G5	58
EQUIVALENCE (C(1756), A022)	D1	25
EQUIVALENCE (C(1756), A022)	D2	76
EQUIVALENCE (C(1757), A023)	G5	59
EQUIVALENCE (C(1757), A023)	D1	26
EQUIVALENCE (C(1757), A023)	D2	77
EQUIVALENCE (C(1758), A031)	G5	60
EQUIVALENCE (C(1758), A031)	D1	27
EQUIVALENCE (C(1758), A031)	D2	78
EQUIVALENCE (C(1759), A032)	G5	61
EQUIVALENCE (C(1759), A032)	D1	28
EQUIVALENCE (C(1759), A032)	D2	79
EQUIVALENCE (C(1760), A033)	G5	62
EQUIVALENCE (C(1760), A033)	D1	29
EQUIVALENCE (C(1760), A033)	D2	71
EQUIVALENCE (C(1761), A011)	G5	54
EQUIVALENCE (C(1761), A011)	D1	72
EQUIVALENCE (C(1762), A012)	G5	55
EQUIVALENCE (C(1762), A012)	D1	73
EQUIVALENCE (C(1763), A013)	G5	56
EQUIVALENCE (C(1763), A013)	D1	67
EQUIVALENCE (C(1764), P1)	G5	63
EQUIVALENCE (C(1764), P1)	D1	1
EQUIVALENCE (C(1765), R1)	ROLLGYRO	14
EQUIVALENCE (C(1765), R1)	ROLLGYRO	61
EQUIVALENCE (C(1768), XB01)	G5	67
EQUIVALENCE (C(1768), XB01)	D1	62
EQUIVALENCE (C(1769), YB01)	G5	68
EQUIVALENCE (C(1769), YB01)	D1	63
EQUIVALENCE (C(1770), ZB01)	G5	

TABLE 84. (Continued)

EQUIVALENCE (C(1770), ZB01)	D1	69
EQUIVALENCE (C(1771), XB02)	G5	64
EQUIVALENCE (C(1771), XB02)	D1	70
EQUIVALENCE (C(1772), YB02)	G5	65
EQUIVALENCE (C(1772), YB02)	D1	71
EQUIVALENCE (C(1773), ZB02)	G5	66
EQUIVALENCE (C(1773), ZB02)	D1	72
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	44
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	29
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	44
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	29
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	44
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	29
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	17
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	17
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	A2	53
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	18
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	EXEC	93
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	18
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	AMRK	8
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	EXEC	93
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	18
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	A2	54
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	EXEC	93
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	86
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	110
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MCARLO	127
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	G5	157
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S1	210
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S4	357
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	C3	59
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	AMRK	10
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S2	425
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S2	447
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S3	153
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	S3	171
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	49
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	50
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	51
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	52
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	MC7	53
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	12
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	254
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	13
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	168
EQUIVALENCE (C(1901), ISCALE), (C(1916), YMAX), (C(1931), YMIN)	IO	198

TABLE 84. (Continued)

C	(C(2000),T), (C(2011),KSTEP), (C(2010),STEP),	MC7	12
	EQUIVALENCE (C(2000),	T)	MCARLO	7
	IF (C(2000).LT.TNXST(ITSNDX)) GO TO 1000		MCARLO	128
	INXST(18)=C(2000)+TSRPER(18)		MCARLO	144
	EQUIVALENCE (C(2000),T)		G2	53
	EQUIVALENCE (C(2000),T)	G5	80
	EQUIVALENCE (C(2000),T)	A1	22
	EQUIVALENCE (C(2000),	T)	A3	29
	EQUIVALENCE (C(2000),T)	A3	114
	EQUIVALENCE (C(2000),T)	A2	52
	EQUIVALENCE (C(2000),T)	D1	274
	EQUIVALENCE (C(2000),T)	S1	113
	EQUIVALENCE (C(2000),T)	S4	208
	EQUIVALENCE (C(2000),T)	C1	112
	EQUIVALENCE (C(2000),T)	C3	45
	EQUIVALENCE (C(2000),T)	C3	170
	WRITE (6,14)C(2000),XIN,I,J		C3	190
	WRITE (6,14)C(2000),XIN,J		C3	206
	WRITE (6,14)C(2000),XIN,J		G4	19
	EQUIVALENCE (C(2000),T)	AMRK	6
	EQUIVALENCE (C(2000),	T)	AMRK	135
C	(C(2000),T), (C(2361),NOMOD), (C(2362),XMODNO)	IO	162
C	(C(2000),T), (C(2021),KCONV), (C(2025),TIME) ,	IO	194
	(C(2000),T), (C(2664),DER) , (C(2018),TAPE) ,	EXEC	88
	(C(2000),T), (C(2001),TF) , (C(2003),PCNT)	EXEC	282
	WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),		S2	180
	C(655)=C(2000)-C(2664)		S2	329
	EQUIVALENCE (C(2000),	TIME)	S3	63
	EQUIVALENCE (C(2000),	TIME)	EXEC	88
	EQUIVALENCE (C(2000),T), (C(2001),TF) , (C(2003),PCNT)	IO	181
	OPOINT = 0 \$ PPOINT=C(2002)		IO	160
C	(C(2014),ITCNT) ,	(C(2003),PCNT) , (C(2015),CPP) ,	IO	193
C	(C(2014),ITCNT) ,	(C(2003),PCNT) , (C(2015),CPP) ,	EXEC	88
	(C(2000),T), (C(2001),TF) , (C(2003),PCNT)	IO	164
C	(C(2004),PPNT) ,	(C(2023),OPOINT)	IO	196
C	(C(2005),PPP) ,	(C(2004),PPNT) ,	IO	196
C	(C(2005),PPP) ,	(C(2004),PPNT) ,	MC7	15
C	(C(3167),NOOUT) ,	(C(2022),OPTN10) ,	MC7	16
C	(C(2865),EU) ,	(C(2765),EL) ,	MC7	13
C	(C(2012),LSTEP) ,	(C(2008),PLOTNO) ,	IO	9
C	(C(3067),LISTNO) ,	(C(3117),VALUE) ,	IO	163
C	(C(2008),PLOTNO) ,	(C(2009),NOPLT) ,	IO	195
C	(C(2019),TAPEND) ,	(C(2008),PLOTNO) ,	MC7	13
C	(C(2012),LSTEP) ,	(C(2008),PLOTNO) ,	IO	10
C	(C(2009),NOPLT) ,	(C(2325),VLARLE) ,	IO	163
C	(C(2008),PLOTNO) ,	(C(2009),NOPLT) ,	IO	195
C	(C(2019),TAPEND) ,	(C(2008),PLOTNO) ,	IO	195

TABLE 84. (Continued)

C	EQUIVALENCE	(C(2000),T), (C(2011),KSTEP)	, (C(2010),STEP)	MC7	12
		(C(2010),STEP)			IO	11
	EQUIVALENCE	(C(2010),STEP)	, (C(2011),KSTEP)	, (C(2020),LCONV)	EXEC	89
C		(C(2000),T), (C(2011),KSTEP)	, (C(2010),STEP)	MC7	12
	EQUIVALENCE	(C(2011),KSTEP)			S1	15
	EQUIVALENCE	(C(2011),KSTEP)			S4	75
	EQUIVALENCE	(C(2011),KSTEP)	, (C(2020),LCONV)	, (C(2021),KCONV)	EXEC	80
	EQUIVALENCE	(C(2010),STEP)	, (C(2011),KSTEP)	, (C(2020),LCONV)	EXEC	89
	EQUIVALENCE	(C(2012),LSTEP)	, (C(2008),PLOTNO)	, (C(2009),NOPLOT)	MC7	13
C		(C(2018),TAPE)	, (C(2019),TAPEND)	, (C(2013),DOC)	IO	161
C		(C(2014),ITCNT)	, (C(2003),PCNT)	, (C(2015),CPP)	IO	160
C		(C(2014),ITCNT)	, (C(2003),PCNT)	, (C(2015),CPP)	IO	193
C		(C(2014),ITCNT)	, (C(2003),PCNT)	, (C(2015),CPP)	IO	160
C		(C(2014),ITCNT)	, (C(2003),PCNT)	, (C(2015),CPP)	IO	193
	EQUIVALENCE	(C(2017),DTCNT)	, (C(3167),NOOUT)	, (C(2016),PGCNT)	IO	159
C		(C(2017),DTCNT)	, (C(3167),NOOUT)	, (C(2016),PGCNT)	IO	192
	EQUIVALENCE	(C(2017),DTCNT)	, (C(3167),NOOUT)	, (C(2016),PGCNT)	IO	159
C		(C(2018),TAPE)	, (C(2019),TAPEND)	, (C(2013),DOC)	IO	161
C		(C(2000),T	, (C(2664),DER)	, (C(2018),TAPE)	IO	194
C		(C(2018),TAPE)	, (C(2019),TAPEND)	, (C(2013),DOC)	IO	161
C		(C(2019),TAPEND)	, (C(2008),PLOTNO)	, (C(2009),NOPLOT)	IO	195
*		(C(2020),LCONV)			G4	24
	EQUIVALENCE	(C(2020),LCONV)			AMRK	138
	EQUIVALENCE	(C(2011),KSTEP)	, (C(2020),LCONV)	, (C(2021),KCONV)	EXEC	80
	EQUIVALENCE	(C(2010),STEP)	, (C(2011),KSTEP)	, (C(2020),LCONV)	EXEC	89
	EQUIVALENCE	(C(2020),LCONV)			EXEC	266
	EQUIVALENCE	(C(2020),LCONV)			EXEC	274
	EQUIVALENCE	(C(2020),LCONV)			S2	370
	EQUIVALENCE	(C(2020),LCONV)	, (C(625), IBL)		S3	98
C		(C(2000),T), (C(2021),KCONV)	, (C(2025),TIME)	IO	162
	EQUIVALENCE	(C(2011),KSTEP)	, (C(2021),KCONV)	, (C(2021),KCONV)	EXEC	80
	EQUIVALENCE	(C(2021),KCONV)	, (C(2561),N)	, (C(2662),HMIN)	EXEC	90
C		(C(3167),NOOUT)	, (C(2022),OPTN10)	, (C(2006),REPPLT)	MC7	15
C		(C(2023),OPOINT)	, (C(2025),TIME)	, (C(2325),VLABLE)	MC7	14
C		(C(2004),PPNT)	, (C(2023),OPOINT)		IO	164
C		(C(2023),OPOINT)			IO	197
	EQUIVALENCE	(C(2023),OPOINT)			IO	255
C		(C(2023),OPOINT)	, (C(2025),TIME)	, (C(2325),VLABLE)	MC7	14
C		(C(2000),T	, (C(2021),KCONV)	, (C(2025),TIME)	IO	162
C		(C(2005),PPP)	, (C(2004),PPNT)	, (C(2025),TIME)	IO	196
C		(C(2023),OPOINT)	, (C(2025),TIME)	, (C(2325),VLABLE)	MC7	14
C		(C(2009),NOPLOT)	, (C(2325),VLABLE)	, (C(K)	IO	10
	EQUIVALENCE	(C(2361),NOMOD)	, (C(2362),XMODNO)	, (C(2561),N)	AMRK	50
	EQUIVALENCE	(C(2000),T	, (C(2361),NOMOD)	, (C(2362),XMODNO)	AMRK	135
C		(C(13328),ONAME4)	, (C(2361),NOMOD)	, (C(2362),MODNO)	IO	6

TABLE 84. (Continued)

EQUIVALENCE	(C(2361),NOMOD)		IO	256
EQUIVALENCE	(C(2361),NOMOD)	(C(2362),XMODNO), (C(2561),N)	AMRK	50
EQUIVALENCE	(C(2000),T)	(C(2361),NOMOD)	AMRK	135
C	(C(3328),ONAME4)	(C(2361),NOMOD)	IO	6
C	(C(3168),OUTNO)	(C(2461),NOSUB)	IO	7
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	IO	257
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	4
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	30
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	55
C	(C(3168),OUTNO)	(C(2461),NOSUB)	IO	7
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	4
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	30
EQUIVALENCE	(C(2461),NOSUB)	(C(2462),SUBNO)	EXEC	55
C	(C(2561),N)	(C(2562),IPL)	MC7	11
EQUIVALENCE	(C(2561),N)	(C(2965),VAR)	G2	72
EQUIVALENCE	(C(2561),N)		SPOT	4
EQUIVALENCE	(C(2561),N)		A3	30
EQUIVALENCE	(C(2561),N)		D1	5
EQUIVALENCE	(C(2561),N)		D2	11
EQUIVALENCE	(C(2561),N)		S1	26
EQUIVALENCE	(C(2561),N)		S4	66
EQUIVALENCE	(C(2561),N)		C1	10
EQUIVALENCE	(C(2561),N)		C4	30
EQUIVALENCE	(C(2561),N)		C5	22
EQUIVALENCE	(C(2361),NOMOD)	(C(2362),XMODNO), (C(2561),N)	AMRK	50
EQUIVALENCE	(C(2561),N)	(C(2562),IPL)	AMRK	136
EQUIVALENCE	(C(2021),KCONV)	(C(2561),N)	EXEC	90
EQUIVALENCE	(C(2561),N)	(C(2562),IPL)	S2	84
C	(C(2561),N)	(C(2562),IPL)	MC7	11
EQUIVALENCE	(C(2562),IPL)	(C(2562),IPL)	G2	73
EQUIVALENCE	(C(2562),IPL)		SPOT	5
EQUIVALENCE	(C(2562),IPL)		A3	31
EQUIVALENCE	(C(2562),IPL)		D1	6
EQUIVALENCE	(C(2562),IPL)		D2	12
EQUIVALENCE	(C(2562),IPL)		S1	27
EQUIVALENCE	(C(2562),IPL)		S4	67
EQUIVALENCE	(C(2562),IPL)		C1	11
EQUIVALENCE	(C(2562),IPL)		C4	31
EQUIVALENCE	(C(2562),IPL)		C5	23
EQUIVALENCE	(C(2562),IPL)		AMRK	9
EQUIVALENCE	(C(2561),N)	(C(2562),IPL)	AMRK	136
EQUIVALENCE	(C(2561),N)	(C(2562),IPL)	S2	84
EQUIVALENCE	(C(2662),HMIN)	(C(2663),HMAX)	MC7	10
EQUIVALENCE	(C(2662),DERSV)	(C(2664),DER)	MC7	34
EQUIVALENCE	(C(2662),DERSV)	(C(2664),DER)	S1	29
EQUIVALENCE	(C(2662),DERSV)		S4	68

[illegible]

TABLE 84. (Continued)

EQUIVALENCE (C(2021),KCONV), (C(2561),N), (C(2662),HMIN),	EXEC	90
EQUIVALENCE (C(2662),DERSV)	S2	85
EQUIVALENCE (C(2662),HMIN), (C(2663),HMAX), (C(2664),DER),	MC7	10
EQUIVALENCE (C(2663),HMAX), (C(2664),DER), (C(2765),EL),	EXEC	91
EQUIVALENCE (C(2662),HMIN), (C(2663),HMAX), (C(2664),DER),	MC7	10
EQUIVALENCE (C(2664),DT)	MCARLO	12
GSIGU = SIGU*SQRT(1.89/C(2664))	G2	103
I GSPOTY = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	SPOT	37
I GSPOTZ = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	SPOT	44
EQUIVALENCE (C(2664),DER)	A1	23
I GSPOTY = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	D1	103
I GSPOTZ = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	D1	110
C(2664) = DT / AINT(DT / C(2764))	S1	215
C(2664) = DT / AINT(DT / C(2764))	S4	362
IF(C(2664)-0.01 .LT. 1.E-6)GO TO 10	C3	4
C(2664)=0.01	C3	6
30 IF(AHS(0.01-C(2664)*AINT(0.01/C(2664)+1.E-6)).LT.1.E-6)GO TO 50	C3	13
30 IF(AHS(0.01-C(2664)*AINT(0.01/C(2664)+1.E-6)).LT.1.E-6)GO TO 50	C3	13
C(2664)=0.01/AINT(0.01/C(2664)+1.E-6)	C3	14
C(2664)=0.01/AINT(0.01/C(2664)+1.E-6)	C3	14
WRITE(6,45)C(2664)	C3	15
EQUIVALENCE (C(2664),DER)	C3	15
EQUIVALENCE (C(2664),DELT)	C3	29
EQUIVALENCE (C(2561),N), (C(2562),IPL), (C(2664),DER),	AMRK	7
C(2000),T), (C(2664),DER), (C(2018),TAPE),	AMRK	136
EQUIVALENCE (C(2663),HMAX), (C(2664),DER), (C(2765),EL)	IO	194
IF(C(2664).GT..0005)WRITE(6,112)	EXEC	91
C(655)*C(2000)-C(2664)	S2	127
C(2664)=TAU/AINT(TAU/C(2764))	S2	180
C(2664)=TAU/AINT(TAU/C(2764))	S2	388
C(2664)=DT / AINT(DT / C(2764))	S3	116
C(2664)=DT / AINT(DT / C(2764))	S1	215
C(2664)=TAU/AINT(TAU/C(2764))	S4	362
C(2664)=TAU/AINT(TAU/C(2764))	S2	388
C(2664)=TAU/AINT(TAU/C(2764))	S3	116
C(2665),EU), (C(2765),EL), (C(2007),PTLESS)	MC7	16
EQUIVALENCE (C(2765),NTM)	MCARLO	13
EQUIVALENCE (C(2663),HMAX), (C(2664),DER), (C(2765),EL)	EXEC	91
EQUIVALENCE (C(2775),TM)	MCARLO	14
EQUIVALENCE (C(2785),TRMS2)	MCARLO	15
EQUIVALENCE (C(2795),TRMS)	MCARLO	16
EQUIVALENCE (C(2805),TMU)	MCARLO	17
EQUIVALENCE (C(2815),TVM)	MCARLO	18
EQUIVALENCE (C(2825),TSIG)	MCARLO	19
C(2865),EU), (C(2765),EL), (C(2007),PTLESS)	MC7	16
EQUIVALENCE (C(2865),EU), (C(2965),VAR),	EXEC	92
C(2561),N), (C(2562),IPL), (C(2965),VAR),	MC7	11

TABLE 84. (Continued)

EQUIVALENCE (C(3443),REF)	C3	179
EQUIVALENCE (C(3443),ATD)	I0	51
EQUIVALENCE (C(3448),BIT)	C3	180
EQUIVALENCE (C(3448),BATD)	I0	52
EQUIVALENCE (C(3453),REF)	C3	199
EQUIVALENCE (C(3453),DTA)	I0	53
EQUIVALENCE (C(3457),BIT)	C3	200
EQUIVALENCE (C(3457),BDTA)	I0	54
C(3462)=0.0	C3	19
EQUIVALENCE (C(3462),HOLD)	C3	30
EQUIVALENCE (C(3502),OPTN2)	D1	24
EQUIVALENCE (C(3503),OPTN3)	D2	74
EQUIVALENCE (C(3504),OPTN4)	A2	73
EQUIVALENCE (C(3504),OPTN4)	D1	25
EQUIVALENCE (C(3504),OPTN4)	S1	28
EQUIVALENCE (C(3504),OPTN4)	S4	65
EQUIVALENCE (C(3504),OPTN4)	C1	92
EQUIVALENCE (C(3504),OPTN4)	S2	86
EQUIVALENCE (C(3506),OPTN6)	D1	26
EQUIVALENCE (C(3512),ISGCT), (C(3721),ITCT), (C(3511),RNSTRT)	MC7	19
EQUIVALENCE (C(3511),RANSTT)	MCARLO	26
EQUIVALENCE (C(3511),RANSTT)	S4	253
* (C(3594),SIGUB), (C(3634),ISNDX), (C(3674),IDIST), (C(3511),RNSTRT)	I0	15
EQUIVALENCE (C(3512),ISGCT), (C(3721),ITCT), (C(3511),RNSTRT)	MC7	19
EQUIVALENCE (C(3512),ISGCT)	MCARLO	20
EQUIVALENCE (C(3512),ISGCT)	G2	75
EQUIVALENCE (C(3512),ISGCT)	SPOT	7
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	A3	6
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	A2	20
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	D1	8
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	S1	6
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	S4	69
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	C1	8
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	C4	11
EQUIVALENCE (C(3512),ISGCT), (C(3514),SIGMA), (C(3554),SIGLB),	I0	14
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	S2	90
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	S2	375
EQUIVALENCE (C(3634),ISNDX), (C(3512),ISGCT)	S3	103
EQUIVALENCE (C(3514),SIGMA)	MCARLO	21
EQUIVALENCE (C(3514),SIGMA)	S4	72
EQUIVALENCE (C(3512),ISGCT), (C(3514),SIGMA), (C(3554),SIGLB),	I0	14
EQUIVALENCE (C(3554),SIGLB)	MCARLO	22
EQUIVALENCE (C(3554),SIGLB)	S4	73
EQUIVALENCE (C(3512),ISGCT), (C(3514),SIGMA), (C(3554),SIGLB),	I0	14
EQUIVALENCE (C(3594),SIGUB)	MCARLO	23
EQUIVALENCE (C(3594),SIGUB)	S4	74

TABLE 84. (Continued)

• (C(3594), SIGUR), (C(3634), ISNDX), (C(3674), IDIST), (C(3511), RNSTR)	IO	15
EQUIVALENCE (C(3634), ISNDX)	MCARLO	24
EQUIVALENCE (C(3634), ISNDX)	G2	74
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	SPOT	7
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	A3	6
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	A2	20
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	D1	8
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	S1	6
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	S4	69
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	C1	8
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	C4	11
• (C(3594), SIGUR), (C(3634), ISNDX), (C(3674), IDIST), (C(3511), RNSTR)	IO	15
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	S2	90
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	S2	375
EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	S3	103
EQUIVALENCE (C(3674), IDIST)	MCARLO	25
• (C(3594), SIGUR), (C(3634), ISNDX), (C(3674), IDIST), (C(3511), RNSTR)	IO	15
EQUIVALENCE (C(3512), ISGCT), (C(3721), ITCT), (C(3511), RNSTR)	MC7	19
EQUIVALENCE (C(3721), ITCT)	MCARLO	27
EQUIVALENCE (C(3721), ITCT)	G2	6
EQUIVALENCE (C(3721), ITCT)	G5	77
EQUIVALENCE (C(3721), ITCT)	SPOT	37
EQUIVALENCE (C(3721), ITCT)	SPOT	10
EQUIVALENCE (C(3721), ITCT)	SPOT	60
EQUIVALENCE (C(3721), ITCT)	D1	53
EQUIVALENCE (C(3721), ITCT)	S4	71
EQUIVALENCE (C(3721), ITCT)	S4	237
EQUIVALENCE (C(3721), ITCT)	G4	30
EQUIVALENCE (C(3721), ITCT), (C(3723), TSGMA), (C(3733), TLB)	IO	16
EQUIVALENCE (C(3721), ITCT), (C(3723), TSGMA)	MCARLO	28
EQUIVALENCE (C(3721), ITCT), (C(3723), TSGMA), (C(3733), TLB)	IO	16
EQUIVALENCE (C(3733), TLB)	MCARLO	29
EQUIVALENCE (C(3721), ITCT), (C(3723), TSGMA), (C(3733), TLB)	IO	16
EQUIVALENCE (C(3743), TUB)	MCARLO	30
• (C(3743), TUB), (C(3753), ITNDX), (C(3763), ITDIST), (C(3773), TSPER)	IO	17
EQUIVALENCE (C(3753), ITNDX)	MCARLO	31
EQUIVALENCE (C(3753), ITNDX)	G2	5
EQUIVALENCE (C(3753), ITNDX)	G2	74
EQUIVALENCE (C(3753), ITNDX)	G5	36
EQUIVALENCE (C(3753), ITNDX), (C(3721), ITCT)	SPOT	10
EQUIVALENCE (C(3753), ITNDX), (C(3721), ITCT)	SPOT	59
EQUIVALENCE (C(3753), ITNDX), (C(3721), ITCT)	D1	53
EQUIVALENCE (C(3753), ITNDX)	S4	70
EQUIVALENCE (C(3753), ITNDX)	S4	236
• (C(3743), TUB), (C(3753), ITNDX), (C(3763), ITDIST), (C(3773), TSPER)	IO	17
EQUIVALENCE (C(3763), ITDIST)	MCARLO	32

TABLE 84. (Continued)

* (C(3743),TUB), (C(3753),ITNDX), (C(3763),ITDIST), (C(3773),TSPER), EQUIVALENCE (C(3773), TSPER)	IO	17
* (C(3743),TUB), (C(3753),ITNDX), (C(3763),ITDIST), (C(3773),TSPER), EQUIVALENCE (C(3783),TYPER)	MCARLO	33
* (C(3783),TYPER), (C(3793),TPSIG), (C(3803),TNXST), (C(3813),ITNDX2), EQUIVALENCE (C(3793), TPSIG)	IO	34
* (C(3783),TYPER), (C(3793),TPSIG), (C(3803),TNXST), (C(3813),ITNDX2), EQUIVALENCE (C(3803), TNXST)	MCARLO	18
* (C(3783),TYPER), (C(3793),TPSIG), (C(3803),TNXST), (C(3813),ITNDX2), EQUIVALENCE (C(3813),ITNDX2)	IO	35
* (C(3783),TYPER), (C(3793),TPSIG), (C(3803),TNXST), (C(3813),ITNDX2), EQUIVALENCE (C(3825), NCASE), (C(625), IBL)	MCARLO	18
* (C(3783),TYPER), (C(3793),TPSIG), (C(3803),TNXST), (C(3813),ITNDX2), EQUIVALENCE (C(3825), NCASE)	IO	37
COMMON /C/ C(3830)	MCARLO	18
COMMON /C/ C(3830)	MCARLO	36
COMMON /C/ C(3830)	IO	33
COMMON /C/ C(3830)	MC7	25
COMMON /C/ C(3830)	MC7	7
COMMON /C/ C(3830)	MCARLO	3
COMMON /C/ C(3830)	LABCOM	4
COMMON /C/ C(3830)	LABCOM	5
COMMON /C/ C(3830)	LABCOM	6
COMMON /C/ C(3830)	LABCOM	7
COMMON /C/ C(3830)	SPOT	3
COMMON /C/ C(3830)	SPOT	52
COMMON /C/ C(3830)	A1	3
COMMON /C/ C(3830)	A3	4
COMMON /C/ C(3830)	A3	91
COMMON /C/ C(3830)	A2	4
COMMON /C/ C(3830)	LABCOM	14
COMMON /C/ C(3830)	LABCOM	15
COMMON /C/ C(3830)	D2	4
COMMON /C/ C(3830)	D2	67
COMMON /C/ C(3830)	S1	4
COMMON /C/ C(3830)	S1	112
COMMON /C/ C(3830)	S4	5
COMMON /C/ C(3830)	S4	207
COMMON /C/ C(3830)	C1	5
COMMON /C/ C(3830)	C1	73
COMMON /C/ C(3830)	LABCOM	24
COMMON /C/ C(3830)	LABCOM	25
COMMON /C/ C(3830)	LABCOM	26
COMMON /C/ C(3830)	LABCOM	27
COMMON /C/ C(3830)	LABCOM	28
COMMON /C/ C(3830)	LABCOM	29
COMMON /C/ C(3830)	C4	3
COMMON /C/ C(3830)	C4	79
COMMON /C/ C(3830)	C5	3
COMMON /C/ C(3830)	C5	60
COMMON /C/ C(3830)	LABCOM	34

TABLE 84. (Concluded)

COMMON	/C/	C(3830)	AMRK	3
COMMON	/C/	C(3830)	AMRK	49
COMMON	/C/	C(3830)	AMRK	134
COMMON	/C/	C(3830)	AMRK	226
COMMON	/C/	C(3830)	IO	4
COMMON	/C/	C(3830)	IO	157
COMMON	/C/	C(3830)	IO	189
COMMON	/C/	C(3830)	IO	253
COMMON	/C/	C(3830)	EXEC	3
COMMON	/C/	C(3830)	EXEC	29
COMMON	/C/	C(3830)	EXEC	54
COMMON	/C/	C(3830)	EXEC	79
COMMON	/C/	C(3830)	EXEC	87
COMMON	/C/	C(3830)	EXEC	120
COMMON	/C/	C(3830)	EXEC	265
COMMON	/C/	C(3830)	EXEC	273
COMMON	/C/	C(3830)	S2	3
COMMON	/C/	C(3830)	S2	274
COMMON	/C/	C(3830)	LABCOM	55

V. COMMENTS OR RECOMMENDATIONS

A. Monte Carlo Recommendations

When running parametric studies that involve time series error sources (such as spot jitter and/or wind gusts), it is strongly recommended that the integration stepsize remain fixed for all sets of runs. It is important to maintain the same set of nominal conditions as closely as possible from run set to run set in order to have consistent results for comparison purposes (do not compare a CEP generated at $l = 1'$ with CEP generated at $l = 2'$). While making checkout runs with the Monte Carlo program, it was discovered that the statistical properties of the time series output (spot jitter in particular) changes with changes in integration stepsize. A stepsize of 0.0125 sec produced a spot jitter standard deviation (σ) of 0.92 ft while a stepsize of 0.0100 sec produced a standard deviation of 1.09 ft. Thus, the statistical properties can change as much as $\pm 10\%$. This increases the uncertainty of the results which are already subject to statistical uncertainties due to the finite number of impact points in the CEP calculations.

The statistical properties of the time series output changes with the stepsize because the random number calling frequency changes (the frequency is inherently a function of stepsize due to the digital nature of numerical integration techniques). An attempt to compensate for the effect of calling frequency on the filter output is made through the gain equation, G , of Section III. B. 3. b. The stepsize, t , appears in the radical of this equation as a result of trying to compensate for using discrete white noise as input to the filter instead of continuous white noise.

If the integration stepsize must be changed, it is suggested that a Monte Carlo run be made using the desired stepsize in order to determine what is the RMS of the time series error source. Then, the input standard deviation (SIGSPOT for spot jitter and SIGU for wind gusts) may be changed to produce the desired statistical output. The new value of SIGSPOT or SIGU is computed by dividing the current value of the input SIGSPOT or SIGU by the average RMS output at the end of each run. (For spot jitter, use the average value of the radial RMS output.)

B. Integration Synchronization with Sample Period

Numerical integration must be synchronized with sample period* (τ at ZOH) in order to insure accurate integration. Logic is built into the seeker subroutines to insure that integration and sample period are synchronized. This is accomplished by:

$$t = \tau / \left[\text{AINT}(\tau / t_{\text{INPUT}}) \right] ,$$

where

τ = ZOH sample period (sec)
 Δt_{INPUT} = input integration stepsize (sec)
 $\text{AINT}(X)$ = computer center library function that integerizes the argument (X).
 Δt = computer integration stepsize that the program will use.

The previously mentioned function will always compute an integration stepsize that is equal to or greater than the input stepsize. Since there is an upper bound on the stepsize that can be used to integrate the differential equations in this simulation program, there is the possibility that a stepsize larger than the upper bound will be computed. (Upper bound is approximately 12.5 msec, with the exception of the optical contrast signal seeker model S2 which has an upper bound of approximately 0.5 msec). Therefore, one should insure that a reasonable stepsize is input and verify that a reasonable stepsize is computed. For example, if the sample period is 16.7 msec, then a stepsize of 8.35 msec or less must be input to insure that the computed stepsize is 12.5 msec or less.

VI. C-ARRAY CROSS REFERENCE

Table 84 contains a computer program listing cross reference of the C-array. This table contains the location, in numerical order, of every reference to a C index. The most important feature of this table is that it identifies all variables that are equivalenced to the C array.

The first column contains the Fortran statement in which a C index is used. The second column contains the module or subroutine group name where the C-index is referenced. The third column contains the line number of the module or subroutine group where the C-index reference is located. For example, the first entry in Table 84 is C(11), which is equivalenced to BY. C(11) is referenced at lines 13 and 165 of module S1, and at lines 44 and 287 of module S4.

*A discussion of errors caused by numerical integration of sample data is given in Reference 2.

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1. Terminal Homing Flight Test Vehicle Proposal, North American Rockwell, Columbus, Ohio, May, 1970, Report NR70H-232.
2. O'Hanigan, S. L., Lee, A. W., Jr., and Lewis, C. L., User's Guide for an Optical Contrast Seeker Monte Carlo Terminal Homing Simulation, US Army Missile Command, Redstone Arsenal, Alabama, 14 May 1975, Technical Report RG-75-53.
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5. Lewis, C. L., Lee, A. W., Jr., and Harrison, J. S., User's Guide for a Terminal Homing Monte Carlo Simulation Utilizing a Digital/Linear Laser Seeker, US Army Missile Command, Redstone Arsenal, Alabama, 2 February 1976,
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9. Ball, R. F., Lee, A. W., Jr., and Lewis, C. L., An Engineering and Programming Guide for a Six Degree of Freedom Terminal Homing Simulation Program, US Army Missile Command, Redstone Arsenal, Alabama, 10 October 1973, Technical Report RG-73-22.

Appendix A. ANGULAR ACCELERATION EQUATIONS

The angular acceleration equations implemented in the 6 DOF program (subroutine D2) are

$$\begin{aligned}\omega_{PD} &= \frac{FMXBA}{FMIX} \text{ CRAD} \\ \omega_{QD} &= \frac{FMYBA \cdot \text{CRAD} + (FMIZ - FMIX) \frac{\omega_P \omega_R}{\text{CRAD}}}{FMIY} \\ \omega_{RD} &= \frac{FMZBA \cdot \text{CRAD} + (FMIX - FMIY) \frac{\omega_P \omega_Q}{\text{CRAD}}}{FMIZ},\end{aligned}\tag{A-1}$$

where

ω_{PD} = Angular acceleration about X_B

ω_{QD} = Angular acceleration about Y_B

ω_{RD} = Angular acceleration about Z_B

$FMXBA$ = Applied moment about X_B

$FMYBA$ = Applied moment about Y_B

$FMZBA$ = Applied moment about Z_B

$FMIX$ = Moment of inertia about X_B

$FMIY$ = Moment of inertia about Y_B

$FMIZ$ = Moment of inertia about Z_B .

Equation (A-1) is based on the assumption that (1) $FMITZ = FMIY$ (because of vehicle symmetry about X_B), and (2) the products of inertia are zero (not strictly true, even initially).

Equations (A-1) is derived as follows:

$$\bar{\Delta} = \bar{I} \bar{\omega},$$

where $\bar{\Delta}$ is the angular momentum vector, $\bar{\bar{I}}$ is the inertial tensor, and $\bar{\omega}$ is the angular velocity vector, all in the body coordinate system. Now,

$$\frac{d}{dt} \bar{\Delta} = \frac{d}{dt} (\bar{\bar{I}} \bar{\omega}) = \bar{V} \quad ,$$

i.e., the time derivative of the angular momentum vector equals the torque vector where,

$$\bar{\bar{I}} = \begin{bmatrix} I_{XX} & 0 & 0 \\ 0 & I_{YY} & 0 \\ 0 & 0 & I_{ZZ} \end{bmatrix}_{E_B}$$

$$\bar{\omega} = \frac{1}{\text{CRAD}} \begin{bmatrix} \omega_P \\ \omega_Q \\ \omega_R \end{bmatrix}_{E_B} \quad .$$

So,

$$\bar{\bar{I}} \bar{\omega} = \left(I_{XX}(\omega_P) \bar{X}_B + I_{YY}(\omega_Q) \bar{Y}_B + I_{ZZ}(\omega_R) \bar{Z}_B \right) \frac{1}{\text{CRAD}}$$

where \bar{X}_B , \bar{Y}_B , and \bar{Z}_B are unit vectors in the body system. Thus,

$$\begin{aligned} \frac{d}{dt} (\bar{\bar{I}} \bar{\omega}) &= \frac{1}{\text{CRAD}} \left[I_{XX}(\dot{\omega}_P) \bar{X}_B + I_{XX}(\omega_P) \dot{\bar{X}}_B + I_{YY}(\dot{\omega}_Q) \bar{Y}_B \right. \\ &\quad \left. + I_{YY}(\omega_Q) \dot{\bar{Y}}_B + I_{ZZ}(\dot{\omega}_R) \bar{Z}_B + I_{ZZ}(\omega_R) \dot{\bar{Z}}_B \right] \\ &= M_{\bar{X}} \bar{X}_B + M_{\bar{Y}} \bar{Y}_B + M_{\bar{Z}} \bar{Z}_B \quad , \end{aligned} \quad (\text{A-2})$$

where the assumption is made that

$$\dot{I}_{XX} = \dot{I}_{YY} = \dot{I}_{ZZ} = 0 \quad .$$

The time derivatives of the unit vectors \bar{X}_B , \bar{Y}_B , and \bar{Z}_B are

$$\dot{\bar{X}}_B = \frac{\omega_R \bar{Y}_B - \omega_Q \bar{Z}_B}{\text{CRAD}}$$

$$\dot{\bar{Y}}_B = \frac{\omega_P \bar{Z}_B - \omega_R \bar{X}_B}{\text{CRAD}}$$

$$\dot{\bar{Z}}_B = \frac{\omega_Q \bar{X}_B - \omega_P \bar{Y}_B}{\text{CRAD}}$$

(A-3)

Making these substitutions in Equation (A-3) and collecting terms,

$$\begin{aligned} & \frac{1}{\text{CRAD}} \left\{ \left(I_{XX}(\dot{\omega}_P) - \frac{I_{YY}(\omega_Q)(\omega_R)}{\text{CRAD}} + \frac{I_{ZZ}(\omega_R)(\omega_Q)}{\text{CRAD}} \right) \bar{X}_B \right. \\ & + \left(I_{YY}(\dot{\omega}_Q) + \frac{I_{XX}(\omega_P)(\omega_R)}{\text{CRAD}} - \frac{I_{ZZ}(\omega_R)(\omega_P)}{\text{CRAD}} \right) \bar{Y}_B \\ & + \left(I_{ZZ}(\dot{\omega}_R) - \frac{I_{XX}(\omega_P)(\omega_Q)}{\text{CRAD}} - \frac{I_{YY}(\omega_Q)(\omega_P)}{\text{CRAD}} \right) \bar{Z}_B \left. \right\} \\ & = M_X \bar{X}_B + M_Y \bar{Y}_B + M_Z \bar{Z}_B \end{aligned}$$

Simplifying,

$$\begin{aligned} & \left(I_{XX}(\dot{\omega}_P) + \frac{(I_{ZZ} - I_{YY})(\omega_R)(\omega_Q)}{\text{CRAD}} \right) \bar{X}_B \\ & + \left(I_{YY}(\dot{\omega}_Q) + \frac{(I_{XX} - I_{ZZ})(\omega_P)(\omega_R)}{\text{CRAD}} \right) \bar{Y}_B \\ & + \left(I_{ZZ}(\dot{\omega}_R) + \frac{(I_{YY} - I_{XX})(\omega_P)(\omega_Q)}{\text{CRAD}} \right) \bar{Z}_B \\ & = \text{CRAD} (M_X \bar{X}_B + M_Y \bar{Y}_B - M_Z \bar{Z}_B) \end{aligned}$$

Equating like coefficients and solving for (ω_P) , (ω_Q) , (ω_R) , and noting that $I_{YY} = I_{ZZ}$

$$\dot{\omega}_P = \frac{M_X \cdot \text{CRAD}}{I_{XX}}$$

$$\dot{\omega}_Q = \left(M_Y \cdot \text{CRAD} + \frac{(I_{ZZ} - I_{XX})(\omega_P)(\omega_R)}{\text{CRAD}} \right) \frac{1}{I_{YY}}$$

$$\dot{\omega}_R = \left(M_Z \cdot \text{CRAD} + \frac{(I_{XX} - I_{YY})(\omega_P)(\omega_Q)}{\text{CRAD}} \right) \frac{1}{I_{ZZ}} .$$

Substituting the program names in Equation (4), yields Equation (1).

Appendix B. TIME DERIVATIVES OF THE EARTH TO BODY AXES TRANSFORMATION MATRIX, M

The time derivative of the earth to body axes transformation matrix, $d/dt(M)$ can be obtained as follows:

(1) Let \bar{X}_B , \bar{Y}_B , \bar{Z}_B , and \bar{X}_E , \bar{Y}_E , \bar{Z}_E denote unit vectors in the body and earth system, respectively.

(2) Assume the unit vectors in E_B have angular velocity components about \bar{X}_B , \bar{Y}_B , \bar{Z}_B of ω_P , ω_Q , and ω_R (deg/sec), respectively.

Then the time derivatives of the unit vectors $M^T E_B$, (where M^T denotes the transpose of the matrix, M), written in terms of ω_P , ω_Q , and ω_R are (see Figure B-1 for velocity components):

$$\begin{aligned}\dot{\bar{X}}_B &= \frac{0\bar{X}_B + \omega_R\bar{Y}_B - \omega_Q\bar{Z}_B}{\text{CRAD}} = \begin{bmatrix} 0 \\ \omega_R \\ -\omega_Q \end{bmatrix}_{E_B} \\ \dot{\bar{Y}}_B &= \frac{-\omega_R\bar{X}_B + 0\bar{Y}_B + \omega_P\bar{Z}_B}{\text{CRAD}} = \begin{bmatrix} -\omega_R \\ 0 \\ \omega_P \end{bmatrix}_{E_B} \\ \dot{\bar{Z}}_B &= \frac{\omega_Q\bar{X}_B - \omega_P\bar{Y}_B + 0\bar{Z}_B}{\text{CRAD}} = \begin{bmatrix} \omega_Q \\ -\omega_P \\ 0 \end{bmatrix}_{E_B},\end{aligned}$$

where CRAD is the number of degrees per radian.

Transforming $\dot{\bar{X}}_B$, $\dot{\bar{Y}}_B$, $\dot{\bar{Z}}_B$ into the earth coordinate systems E_E yields

$$\begin{bmatrix} \dot{\bar{X}}_B \\ \dot{\bar{Y}}_B \\ \dot{\bar{Z}}_B \end{bmatrix}_{E_E} = M^T \dot{\bar{X}}_B = \begin{bmatrix} C_{11} & C_{21} & C_{31} \\ C_{12} & C_{22} & C_{32} \\ C_{13} & C_{23} & C_{33} \end{bmatrix} \dot{\bar{X}}_B = \begin{bmatrix} C_{21} & \omega_R - C_{31} & \omega_Q \\ C_{22} & \omega_R - C_{32} & \omega_Q \\ C_{23} & \omega_R - C_{33} & \omega_Q \end{bmatrix}_{E_E}$$

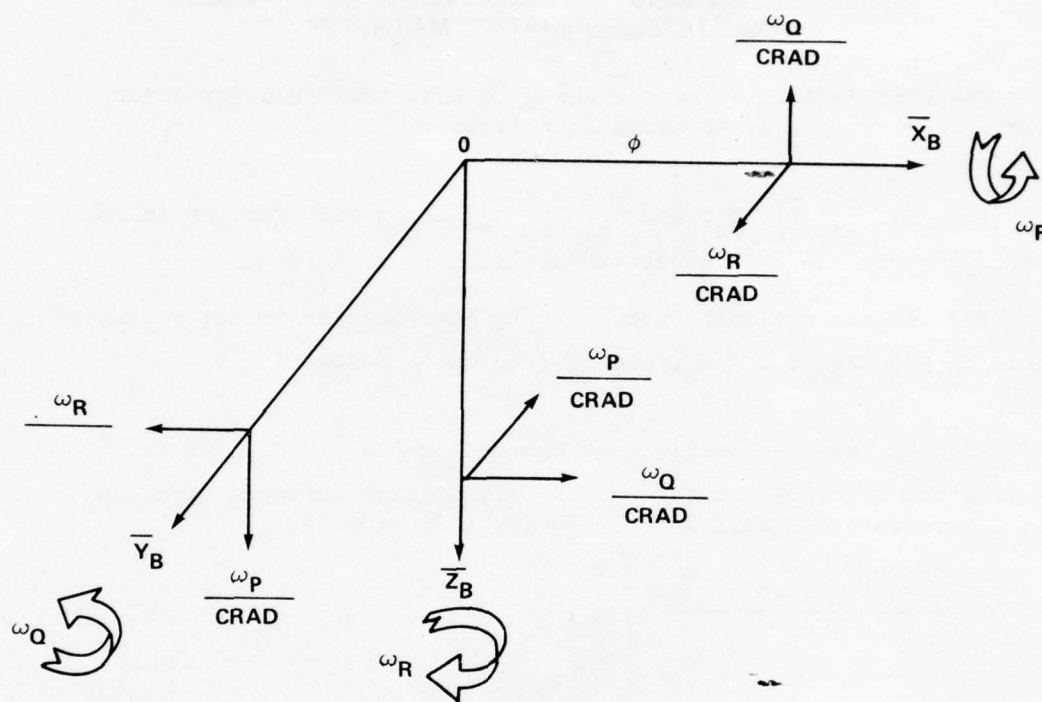


Figure B-1.

$$\begin{bmatrix} \dot{Y}_B \\ \dot{Z}_B \end{bmatrix}_{E_E} = M^T \dot{Y}_B = \begin{bmatrix} -C_{11} \omega_R + C_{31} \omega_P \\ -C_{12} \omega_R + C_{32} \omega_P \\ -C_{13} \omega_R + C_{33} \omega_P \end{bmatrix}_{E_E}$$

$$\begin{bmatrix} \dot{Z}_B \\ \dot{Y}_B \end{bmatrix}_{E_E} = M^T \dot{Z}_B = \begin{bmatrix} C_{11} \omega_Q - C_{21} \omega_P \\ C_{12} \omega_Q - C_{22} \omega_P \\ C_{13} \omega_Q - C_{23} \omega_P \end{bmatrix}_{E_E}$$

But the time derivatives of the unit vectors \bar{x}_B , \bar{y}_B , \bar{z}_B , can also be expressed in the E_E system by first transforming into the E_E system and then taking the time derivatives. Thus,

$$\begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = M^T \bar{X}_B = \begin{bmatrix} c_{11} & c_{21} & c_{31} \\ c_{12} & c_{22} & c_{32} \\ c_{13} & c_{23} & c_{33} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}_{E_B} = \begin{bmatrix} c_{11} \\ c_{12} \\ c_{13} \end{bmatrix}_{E_B}$$

$$\begin{bmatrix} Y_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = M^T \bar{Y}_B = \begin{bmatrix} c_{21} \\ c_{22} \\ c_{23} \end{bmatrix}_{E_B}$$

$$\begin{bmatrix} Z_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = \begin{bmatrix} c_{31} \\ c_{32} \\ c_{33} \end{bmatrix}_{E_B}$$

Written in terms of the unit vectors \bar{X}_E , \bar{Y}_E , and \bar{Z}_E ,

$$\begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = c_{11} \bar{X}_E + c_{12} \bar{Y}_E + c_{13} \bar{Z}_E$$

$$\begin{bmatrix} Y_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = c_{21} \bar{X}_E + c_{22} \bar{Y}_E + c_{23} \bar{Z}_E$$

$$\begin{bmatrix} Z_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = c_{31} \bar{X}_E + c_{32} \bar{Y}_E + c_{33} \bar{Z}_E$$

Since the E_E system is considered fixed; i.e., $\dot{\bar{X}}_E = \dot{\bar{Y}}_E = \dot{\bar{Z}}_E = 0$,

$$\frac{d}{dt} \begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = \dot{c}_{11} \bar{X}_E + \dot{c}_{12} \bar{Y}_E + \dot{c}_{13} \bar{Z}_E = \begin{bmatrix} \dot{c}_{11} \\ \dot{c}_{12} \\ \dot{c}_{13} \end{bmatrix}_{E_E}$$

$$\frac{d}{dt} \begin{bmatrix} Y_B \\ Y_B \\ Z_B \end{bmatrix}_{E_E} = \begin{bmatrix} \dot{c}_{21} \\ \dot{c}_{22} \\ \dot{c}_{23} \end{bmatrix}_{E_E}$$

$$\frac{d}{dt} [Z_B]_{E_E} = \begin{bmatrix} \dot{C}_{31} \\ \dot{C}_{32} \\ \dot{C}_{33} \end{bmatrix}_{E_E}$$

Since the corresponding expression obtained by the two methods represent the same vectors, from 1 and 2, it follows that

$$\dot{C}_{11} = C_{21} \omega_R - C_{31} \omega_Q$$

$$\dot{C}_{12} = C_{22} \omega_R - C_{32} \omega_Q$$

$$\dot{C}_{13} = C_{23} \omega_R - C_{33} \omega_Q$$

$$\dot{C}_{21} = C_{31} \omega_P - C_{11} \omega_R$$

$$\dot{C}_{22} = C_{32} \omega_P - C_{12} \omega_R$$

$$\dot{C}_{23} = C_{33} \omega_P - C_{13} \omega_R$$

$$\dot{C}_{31} = C_{11} \omega_Q - C_{21} \omega_P$$

$$\dot{C}_{32} = C_{12} \omega_Q - C_{22} \omega_P$$

$$\dot{C}_{33} = C_{13} \omega_Q - C_{23} \omega_P$$

Appendix C. ORIENTATION OF BODY AND EARTH AXES

The Euler angles which orient the body axis system with respect to the earth axis system (Figure C-1) are defined as follows:

- 1) A positive rotation (toward Y_E from X_E) of ψ (deg) about the Z_E -axis, giving a system E' (X^1 , Y^1 , Z^1).
- 2) A negative rotation (The X^1 -axis up from the plane of the earth axis system) of θ about the Y^1 -axis, giving a system E'' (X'' , Y'' , Z'').
- 3) A positive rotation (toward Z'' from Y'') of degrees about the X'' -axis, giving the body axis system E_B (X_B , Y_B , Z_B).

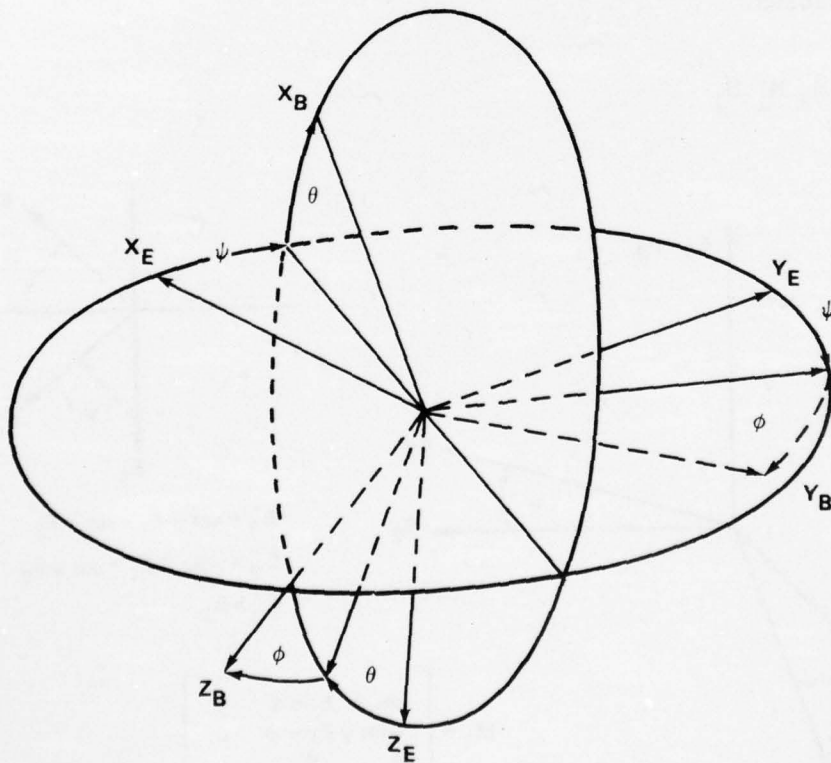


Figure C-1. Euler angles which orient the body axis system with respect to the earth axis system.

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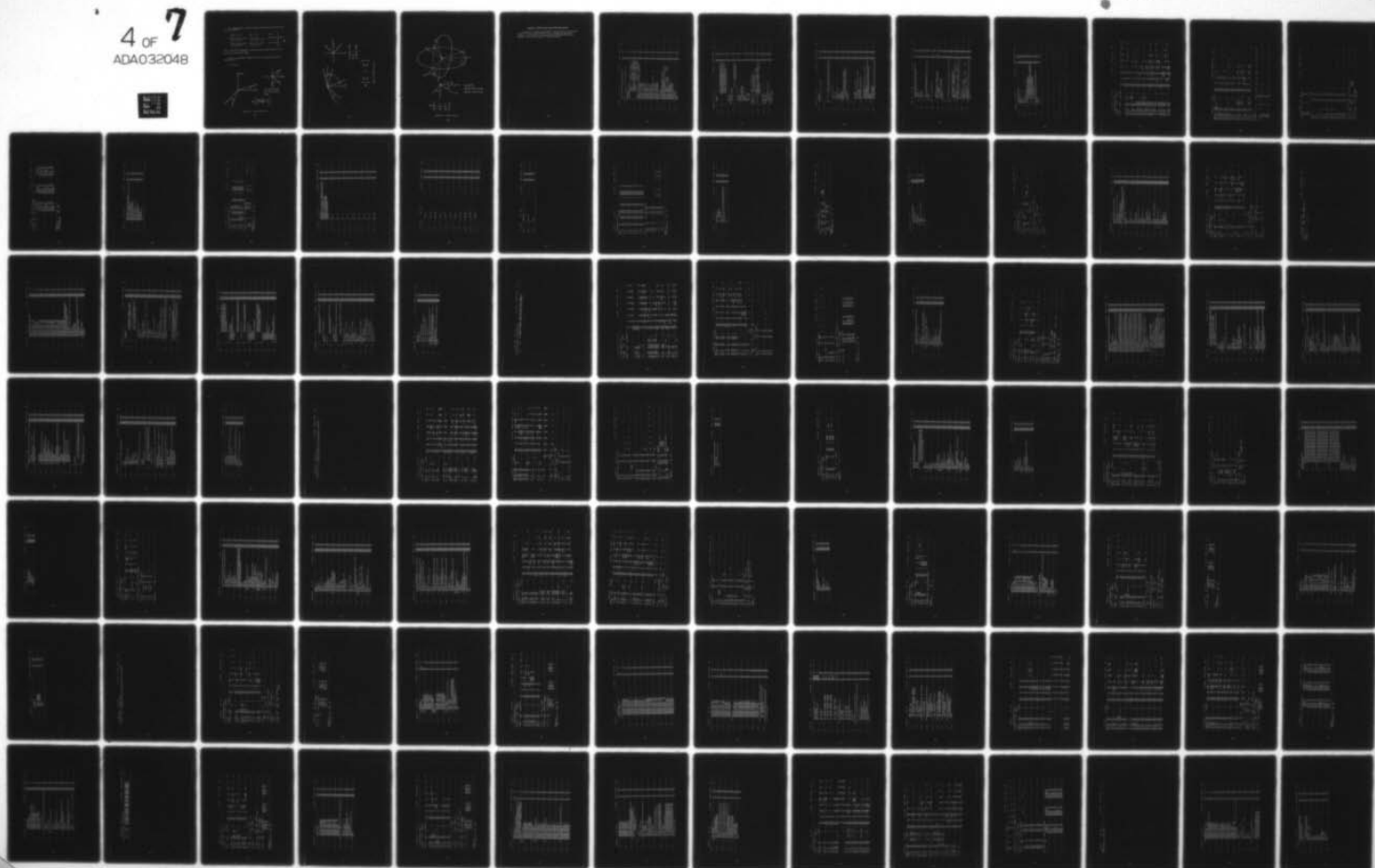
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THAD T-7 MISSILE MONTE-CARLO TERMINAL HOMING SIMULATION UTILIZI--ETC(U)
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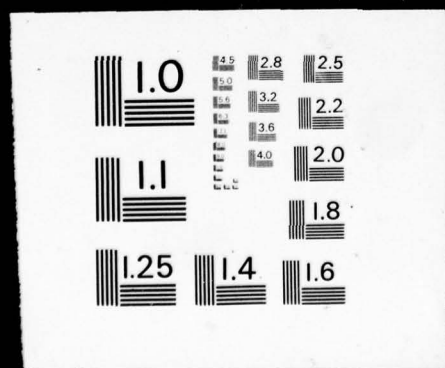
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The transformation, M , from the earth axis system to the body axis system is given by

$$M = \begin{bmatrix} \cos \psi \cos \theta & \sin \psi \cos \theta & -\sin \theta \\ \cos \psi \sin \theta \sin \phi & \cos \psi \cos \theta \sin \phi & \cos \theta \sin \phi \\ -\sin \psi \cos \theta & +\sin \psi \sin \theta \sin \phi & \\ \cos \psi \sin \theta \cos \phi & \sin \psi \sin \theta \cos \phi & \cos \theta \cos \phi \\ +\sin \psi \sin \theta & -\cos \psi \sin \theta & \end{bmatrix} \quad (C-1)$$

Thus, a vector \bar{V}_E expressed in the earth axis system is given in the body axis system as $\bar{V}_B = M\bar{V}_E$.

Then, M , as defined in Equation (C-1) is obtained from matrix multiplication,

$$M = M_3 M_2 M_1$$

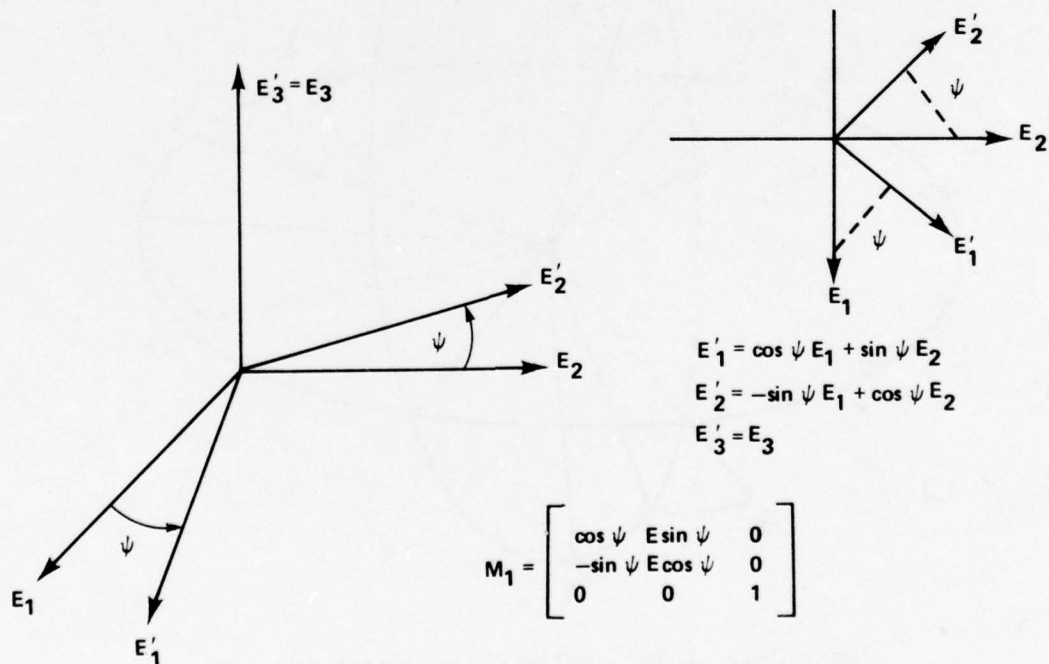
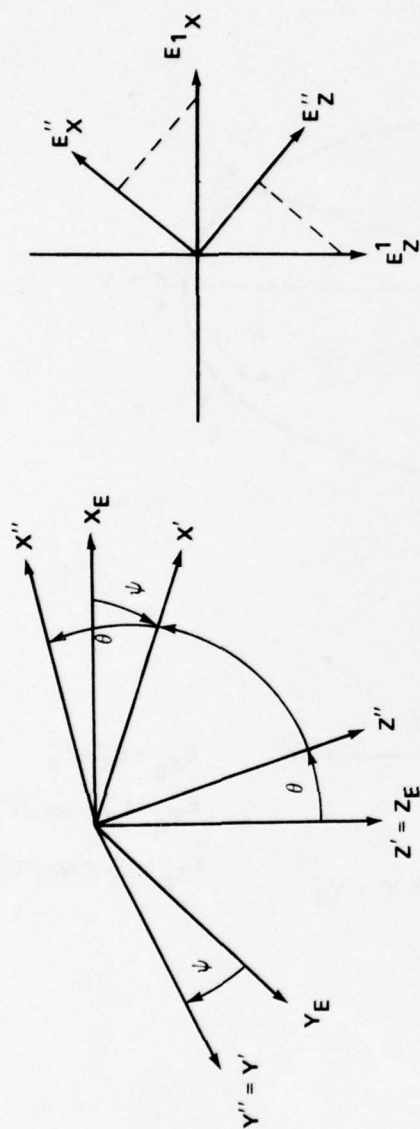


Figure C-2. First rotation, ψ .



$$\begin{aligned} E''_X &= \cos \theta E^1_X - \sin \theta E^1_Z \\ E''_Y &= E^1_Y \\ E''_Z &= \sin \theta E^1_X + \cos \theta E^1_Z \end{aligned}$$

$$M_2 = \begin{bmatrix} \cos \theta & 0 & -\sin \theta \\ 0 & 1 & 0 \\ \sin \theta & 0 & \cos \theta \end{bmatrix}$$

Figure C-3 Second rotation.

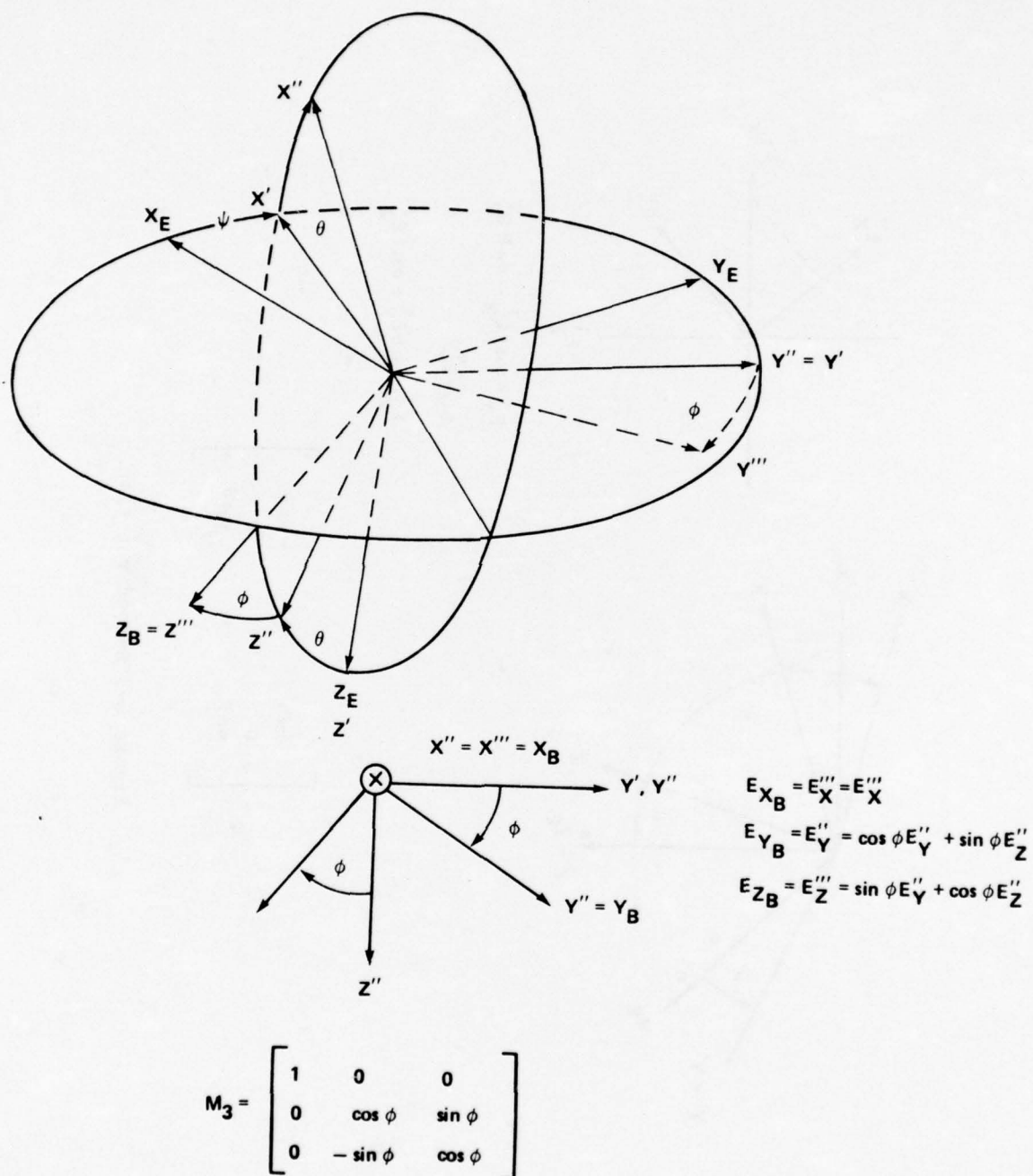


Figure C-4. Third rotation.

Appendix D. MONTE CARLO 6-DOF PROGRAM LISTING

A Fortran IV listing of the THAD T-7 missile version of the Monte Carlo 6 DOF point target terminal homing, all-digital simulation follows. It is currently in operation on MICOM's CDC 6600 digital computer, utilizing the SCOPE 3.4 operating system.

290

PROGRAM MAIN	74/74	OPT=1	FTN **27,155	07/07/75	11.03.44.	PAGE	3
115	1008 CONTINUE					MC7	114
	1009 CALL SUB3					MC7	115
	IF (KSTEP.EQ.1) GO TO 1007					MC7	116
	C					MC7	117
120	C					MC7	118
	C					MC7	119
	C					MC7	120
	C					MC7	121
	C					MC7	122
125	C*****SAVE MISS DISTANCE FOR EACH RUN OF THE MONTE CARLO					MC7	123
	RUN SET*****					MC7	124
	C					MC7	125
	C					MC7	126
	C					MC7	127
130	IF (LCM.ME.1) GO TO 20					MC7	128
	LCM=0					MC7	129
	NP = NP + 1					MC7	130
	X(NP) = NYF					MC7	131
	Y(NP) = KZF					MC7	132
135	MISS(NP) = MISS					MC7	133
	GO TO 21					MC7	134
	20 CONTINUE					MC7	135
	WRITE(6,805)					MC7	136
	805 FORMAT(1H0,///)					MC7	137
140	WRITE(6,822) L					MC7	138
	22 FORMAT(1H0,11X,26H*8*8*8 WARNING RUN NUMBER ,13,					MC7	139
	3 374 DID NOT INTERSECT TARGET PLANE*8*8*8,/,					MC7	140
	3 //26X,38H*8*8 THIS RUN DROPPED FROM DATA SET*8*8)					MC7	141
	WRITE(6,805)					MC7	142
145	21 CONTINUE					MC7	143
	L = L + 1					MC7	144
	C					MC7	145
	C					MC7	146
	C					MC7	147
	C					MC7	148
150	C					MC7	149
	CALL PRODS					MC7	150
	IF (OPT10.GT.9) CALL DUMPO					MC7	151
	CAL= RESET					MC7	152
155	IF (LSTEP.EQ.5.OR.LSTEP.EQ.7.OR.NOPLOT.EQ.0) GOTO5					MC7	153
	CALL TIMEV(DEL)					MC7	154
	WRITE(6,96) DEL					MC7	155
	96 FORMAT(1H1,11X,26H*8*8*8 WARNING RUN NUMBER ,13,					MC7	156
	3 374 DID NOT INTERSECT TARGET PLANE*8*8*8,/,					MC7	157
	3 //26X,38H*8*8 THIS RUN DROPPED FROM DATA SET*8*8)					MC7	158
160	IF (NOPLOT.LE.0) GO TO 99					MC7	159
	TIMEAB(1)=TIME					MC7	160
	IF (INPLO1.GT.0) GO TO 95					MC7	161
	DO 94 KPL0T=1,NPLO1					MC7	162
165	CALL PLOT4 (ISCALE(KPLOTT),XMAX,XMIN,YMAX(KPLOTT),YMIN(KPLOTT),TIME,					MC7	163
	GRAPH4(KPLOTT),POINT,TIMEAB,VLABEL(KPLOTT),IP,ITIME)					MC7	164
	CONTINUE					MC7	165
94	CONTINUE					MC7	166
95	IF (INPLO2.EQ.0) GO TO 98					MC7	167
	KPLOTT=1 - ITIME=1					MC7	168
170	DO 93 KPLOTT=1,NPLO2					MC7	169
	CALL PLOT4 (ISCALE(KPLOTT),XMAX(KPLOTT),YMAX(KPLOTT),YMIN(KPLOTT),TIME,					MC7	170

```

PROGRAM MAIN      7/74  OPT=1      STN +.27,355      07/07/75  11.03.44.      PAGE 4

**VHKKKPL0T(I),GRAPM(I),KKPLOT,GRAPM(I),KKPLOT(I),POINT,
- VLABE(I),KKPLOT(I),VLABE(I),KKPLOT(I),IP,ITIME)
KKPLOT=KKPLOT+2
175 CONTINUE MC7 172
98 CONTINUE MC7 173
IP=0 MC7 174
MC7 175
MC7 176
MC7 177
CALC KST(I) MC7 178
WRITE(I,37) MC7 179
CONTINUE MC7 180
MC7 181
MC7 182
97 FORMAT(14,'18PLOTING ENDED AT F14.7') MC7 183
5 00 10 0100010011002100310041005100610071008100910101, MC7 184
1 1511F MC7 185
1810 CONTINUE MC7 186
MC7 187
C**** MEAN AND STANDARD DEVIATION EXCEED 1
190 MC7 189
C MC7 190
C MC7 191
C MC7 192
100 FORMAT(1M1,13X,'MEAN AND STANDARD DEVIATION'// MC7 193
1 17X'C-LOCATION'3X'MEAN *19X'STD DEV'// EXCEED 2
DO 120 I=1,IMVCT 3
ILUC = IMVNDX(I) MC7 195
WRITE(I,102) ILUC,VMEAN(I),VSD(I) MC7 196
102 FORMAT(10X,15,8X,E15.8,11X,E15.8) MC7 197
120 CONTINUE MC7 198
MC7 199
MC7 200
MC7 201
MC7 202
MC7 203
MC7 204
MC7 205
MC7 206
MC7 207
C*****MONTE CARLO AND DEP LOGIC FOLLOWS***** MC7 208
IF(INP.LT.NCASE.AND.L.LE.(NCASE+5))WRITE(I,107) MC7 209
IF(INP.LT.NCASE.AND.L.LE.(NCASE+5))GO TO 8 MC7 210
807 FORMAT(1M1,31//)* THIS RUN ADDED DUE TO BREAKLOCK,31//) MC7 211
J=3 MC7 212
MC7 213
WRITE(I,100) MC7 214
800 FORMAT(1M1, 96X,10HY-MISS ,10H7-MISS ,10HMISS DIST /, MC7 215
1 10H123H----- MC7 216
2----- MC7 217
3--) MC7 218
DO 801 I=1,NP MC7 219
J=J+1 MC7 220
WRITE(I,802) X(I),Y(I),RMST(I) MC7 221
802 FORMAT(6X,10M1 ,10M1 ,10M1 ,10M1 ,10M1 ,10M1 MC7 222
1,10M1 ,10M1 ,10M1 ,10M1 ,10M1 ,10M1 MC7 223
2 ,1M1,F9.5,2M 1,F9.5,2M 1,F9.5,2M 1) MC7 224
WRITE(I,803) MC7 225
803 FORMAT(6X,123H----- MC7 226
1----- MC7 227
2----- MC7 228
3----- MC7 229

```


VARIABLES	SN	TYPE	RELOCATION	
3665 NPT	17	INTEGER	REFS	
3746 OPJINT	9	INTEGER	REFS	
3757 OPT	54	INTEGER	REFS	171
3745 OPINIO	9	REAL	REFS	
3727 PLOTNO	9	REAL	REFS	152
3676 PLOJIN2	51	REAL	REFS	73
3675 PLOJIN	50	REAL	REFS	91
3722 PLOTZ	29	REAL	REFS	247
3726 PLESS	9	REAL	REFS	
3613 RATIO	237	REAL	REFS	236
3725 REPPLT	9	REAL	REFS	79
3662 RITE	16	REAL	REFS	
3663 RNTA	16	REAL	REFS	
3753 RMISS	24	REAL	REFS	134
3747 RMISST	25	REAL	REFS	221
3673 RN	48	REAL	REFS	DEFINED 134
3666 RNSTRT	18	REAL	REFS	
3674 RNT	49	REAL	REFS	64
3723 RZF	28	REAL	REFS	
3731 STEP	30	REAL	REFS	132
3717 T	9	REAL	REFS	133
3750 TIME	9	REAL	REFS	69
3614 TLAB	41	REAL	REFS	154
3624 VRR	9	REAL	REFS	164
3701 VMEAN	35	REAL	REFS	DEFINED 2*161
3667 VJJ	34	REAL	REFS	134
3611 X	47	REAL	REFS	198
3612 XL	47	REAL	REFS	138
3620 XLMBO	21	REAL	REFS	221
3602 XMAX	164	REAL	REFS	DEFINED 234
3603 XMIN	164	REAL	REFS	DEFINED 235
3614 Y	164	REAL	REFS	247
3673 YMAX	41	REAL	REFS	134
3612 YMIN	41	REAL	REFS	DEFINED 133

FILE NAMES

0 INPUT
2041 OUTPUT
0 Tapes

FILE	WRITES	137	139	143	174	176	193	198	210
2041 Tapes	214	221	225	223	217				

EXTERNALS

NAME	TYPE	ANGS	REFERENCES
ARMK	1	114	
AUXI	0	106	
AUXSUB	0	55	114
CEPAS	7	247	
CUNATV	0	71	
DUMPU	0	152	
EXIT	0	249	
MCARLO	3	45	
ONINPT	0	61	
PLJIT	12	164	171
PROGES	0	151	

EXTERNALS	RENUM	TYPE	ARGS	DEF LINE	REFERENCES
	RENUM				
	RESET		0	153	
	RSTR		1	176	
	SUJL1		0	105	
	SUJL2		0	107	
	SUJL3		0	116	
	TIMEV		1	155	
	ZERO		0	72	

STATEMENT LABELS	DEF LINE	REFERENCES
+158 4	86	83
+182 5	134	154
+187 7	81	73
+190 8	82	211
+177 20	136	189
+205 21	144	135
+206 22	140	139
0 93	175	170
0 94	186	153
+251 95	167	152
+533 96	157	156
+542 97	183	179
+275 98	176	168
+302 99	180	150
+552 100	194	193
+572 102	193	196
0 123	200	196
+613 300	215	214
0 201	231	219
+544 302	222	221
+570 303	220	225
+507 304	246	232
+500 305	138	137
+720 305	239	237
+501 307	212	210
+117 1010	72	194
+120 1031	73	194
+147 1032	105	134
+150 1033	106	194
+151 1034	107	184
+152 1005	108	134
+160 1005	112	154
+161 1007	113	117
+164 1008	115	134
+164 1009	116	134
+321 1010	185	194
0 +608	243	

COMMON BLOCKS	LENGTH	MEMBERS	REAS NAME(LENGTH)
2 /	3650	1	0 C GRAPH (1)
3 /	3650	1	0 C GRAPH (1)

COMMON BLOCKS	LENGTH	MEMBERS	REAS NAME(LENGTH)
236 34	163 109	133	EXT REFS
425 93	170 175	204	EXT REFS
324 123	140 200	128	EXT REFS
334 301	219 231	248	EXT REFS

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)	0 X (100)	100 Y (100)
CEPSS	200			
C				
CEJIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)		
C	3810			
		11 PSIG (1)	20 INVNS4 (1)	21 IPLOT (1)
		22 KSIIG (1)	23 KSIIG (1)	24 CEPSIG (6)
		29 RMISS (1)	298 RMISS (1)	300 L (1)
		30 CSEP (1)	302 RVE (1)	324 IRI (1)
		301 RVE (1)	300 ISCALE (15)	305 VMAX (15)
		399 RMIST (100)	1970 RITE (1)	1971 RKUTTA (1)
		1930 YMIN (15)	1973 NJ (1)	1974 NPT (1)
		1972 KASE (1)	1980 RMT (1)	1981 PLOTIN (1)
		1979 RN (1)	1983 NPLOT (1)	1989 T (1)
		1982 PLOIN2 (1)	2006 PILES3 (1)	2032 OLOFNO (1)
		2005 RZPLT (1)	2009 STEP (1)	2010 KSTEP (1)
		2008 NPLOT (1)	2021 OPTMIB (1)	2022 OPOINT (1)
		2011 LSTEP (1)	2324 VL3LE (30)	2330 N (1)
		2024 TIME (300)	2601 DERSW (1)	2651 HMIN (1)
		2561 IPL (100)	2663 DER (101)	2754 EL (100)
		2662 HMAX (1)	2964 VAR (101)	2939 V50 (10)
		2964 E9 (100)	3019 INVNDX (10)	3029 INVCT (1)
		3009 VMEAN (10)	3510 RMSTRT (1)	3511 ISGCT (1)
		3166 NDOOT (1)	3824 NCASEI (1)	
		3720 ITCT (1)		

STATISTICS	PROGRAM LENGTH	7443	400
BUFFER LENGTH		41028	2114
CM LABELED COMMON LENGTH		75769	4030
CM BLANK COMMON LENGTH		13	1

BLOCK DATA B		
COMMON /CXFUN/CX(18) /CZFUN/CN(24) /BCZFUN/OCN(24) /CNFUN/CN(24)		MC7 268
* /DCZFUN/OCM(24) /CXCFJN/CX(18) /CNZFUN/CN2(24) /CYCFUN/CY2(24)		MC7 269
* /CLZFUN/CL2(24) /CLCFUN/CL3(24)		MC7 270
* /CZCFUN/CN1(24) /CN5(24) /CN3(24) /CN4(24)		MC7 271
* /CNCFUN/CN1(24) /CN2(24) /CN3(24) /CN4(24)		MC7 272
* /CLOFUN/CL1(24) /CL2(24) /CL3(24) /CL4(24)		MC7 273
* /CNPUN/CNP(24) /CLPFUN/CLP(24)		MC7 274
DATA CX /		MC7 275
.		MC7 276
.		MC7 277
.		MC7 278
.		MC7 279
DATA CN		MC7 280
.		MC7 281
.		MC7 282
.		MC7 283
.		MC7 284
.		MC7 285
DATA JCN /		MC7 286
.		MC7 287
.		MC7 288
.		MC7 289
.		MC7 290
.		MC7 291
DATA CM /		MC7 292
.		MC7 293
.		MC7 294
.		MC7 295
DATA OCM /		MC7 296
.		MC7 297
.		MC7 298
.		MC7 299
DATA CXJ /		MC7 300
.		MC7 301
.		MC7 302
DATA CN2 /		MC7 303
.		MC7 304
.		MC7 305
.		MC7 306
DATA CY2 /		MC7 307
.		MC7 308
.		MC7 309
.		MC7 310
DATA CL2 /		MC7 311
.		MC7 312
.		MC7 313
.		MC7 314
.		MC7 315
DATA CL3 /		MC7 316
.		MC7 317
.		MC7 318
.		MC7 319
.		MC7 320
.		MC7 321
DATA CMT /		MC7 322
.		MC7 323
.		MC7 324

60	DATA CM5 /	MC7 325
		MC7 326
		MC7 327
		MC7 328
		MC7 329
		MC7 330
65	DATA CM3 /	MC7 331
		MC7 332
		MC7 333
		MC7 334
		MC7 335
		MC7 336
70	DATA CMN /	MC7 337
		MC7 338
		MC7 339
		MC7 340
		MC7 341
		MC7 342
75	DATA CL1 /	MC7 343
		MC7 344
		MC7 345
		MC7 346
		MC7 347
		MC7 348
80	DATA CL5 /	MC7 349
		MC7 350
		MC7 351
		MC7 352
		MC7 353
		MC7 354
85	DATA CL6 /	MC7 355
		MC7 356
		MC7 357
		MC7 358
		MC7 359
		MC7 360
90	DATA CL4 /	MC7 361
		MC7 362
		MC7 363
		MC7 364
		MC7 365
		MC7 366
95	DATA CL1 /	MC7 367
		MC7 368
		MC7 369
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		MC7 371
		MC7 372
100	DATA CM1 /	MC7 373
		MC7 374
		MC7 375
		MC7 376
		MC7 377
		MC7 378
105	DATA CM3 /	MC7 379
		MC7 380
		MC7 381
110	DATA CMN /	MC7 382
		MC7 383
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		MC7 498
		MC7 499
		MC7 500
		MC7 501

BLOCK DATA B	7474	OPT=1	FTN +.247+355	07/07/75	11.08.49.	PAGE	3
115	DATA CME /			MC7	392		
	.			MC7	393		
	.			MC7	394		
	.			MC7	395		
120	DATA QLP /			MC7	396		
	.			MC7	397		
	.			MC7	398		
	.			MC7	399		
	.			MC7	399		
125	END			MC7	391		
				MC7	392		

SYMBOLIC REFERENCE MAP (R-3)									
VARIABLES	SN	TYPE	RELOCATION	REFS					
0 CLP	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	120		
0 CL1	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	75		
0 CL2	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	45		
0 CL3	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	50		
110 CL4	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	30		
30 CL5	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	30		
60 CL6	REAL	ARRAY	CLPFUN	REFS	2	DEFINED	35		
0 CM	REAL	ARRAY	CMFUN	REFS	2	DEFINED	23		
0 CM1	REAL	ARRAY	CM2FUN	REFS	2	DEFINED	115		
0 CM2	REAL	ARRAY	CM2FUN	REFS	2	DEFINED	95		
30 CM3	REAL	ARRAY	CM2FUN	REFS	2	DEFINED	100		
60 CM4	REAL	ARRAY	CM2FUN	REFS	2	DEFINED	105		
110 CM5	REAL	ARRAY	CM2FUN	REFS	2	DEFINED	110		
0 CN	REAL	ARRAY	CNFUN	REFS	2	DEFINED	13		
0 CN1	REAL	ARRAY	CNFUN	REFS	2	DEFINED	55		
0 CN2	REAL	ARRAY	CNFUN	REFS	2	DEFINED	35		
00 CN3	REAL	ARRAY	CNFUN	REFS	2	DEFINED	95		
110 CN4	REAL	ARRAY	CNFUN	REFS	2	DEFINED	70		
30 CN5	REAL	ARRAY	CNFUN	REFS	2	DEFINED	50		
0 CX	REAL	ARRAY	CXFUN	REFS	2	DEFINED	9		
0 CX1	REAL	ARRAY	CXFUN	REFS	2	DEFINED	33		
0 CX2	REAL	ARRAY	CXFUN	REFS	2	DEFINED	40		
0 UC	REAL	ARRAY	UCFUN	REFS	2	DEFINED	28		
0 UC1	REAL	ARRAY	UCFUN	REFS	2	DEFINED	16		

COMMON BLOCKS - BIAS NAME(LENGTH)									
COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)						
0 CX	16	0 CX	(16)						
0 CM	24	0 CM	(24)						
0 CN	24	0 CN	(24)						
0 CX1	24	0 CX1	(24)						
0 CX2	24	0 CX2	(24)						
0 CX3	24	0 CX3	(24)						
0 CX4	24	0 CX4	(24)						
0 CX5	24	0 CX5	(24)						
0 CX6	24	0 CX6	(24)						
0 CX7	24	0 CX7	(24)						
0 CX8	24	0 CX8	(24)						
0 CX9	24	0 CX9	(24)						
0 CX10	24	0 CX10	(24)						
0 CX11	24	0 CX11	(24)						
0 CX12	24	0 CX12	(24)						
0 CX13	24	0 CX13	(24)						
0 CX14	24	0 CX14	(24)						
0 CX15	24	0 CX15	(24)						
0 CX16	24	0 CX16	(24)						
0 CX17	24	0 CX17	(24)						
0 CX18	24	0 CX18	(24)						
0 CX19	24	0 CX19	(24)						
0 CX20	24	0 CX20	(24)						
0 CX21	24	0 CX21	(24)						
0 CX22	24	0 CX22	(24)						
0 CX23	24	0 CX23	(24)						
0 CX24	24	0 CX24	(24)						
0 CX25	24	0 CX25	(24)						
0 CX26	24	0 CX26	(24)						
0 CX27	24	0 CX27	(24)						
0 CX28	24	0 CX28	(24)						
0 CX29	24	0 CX29	(24)						
0 CX30	24	0 CX30	(24)						
0 CX31	24	0 CX31	(24)						
0 CX32	24	0 CX32	(24)						
0 CX33	24	0 CX33	(24)						
0 CX34	24	0 CX34	(24)						
0 CX35	24	0 CX35	(24)						
0 CX36	24	0 CX36	(24)						
0 CX37	24	0 CX37	(24)						
0 CX38	24	0 CX38	(24)						
0 CX39	24	0 CX39	(24)						
0 CX40	24	0 CX40	(24)						
0 CX41	24	0 CX41	(24)						
0 CX42	24	0 CX42	(24)						
0 CX43	24	0 CX43	(24)						
0 CX44	24	0 CX44	(24)						
0 CX45	24	0 CX45	(24)						
0 CX46	24	0 CX46	(24)						
0 CX47	24	0 CX47	(24)						
0 CX48	24	0 CX48	(24)						
0 CX49	24	0 CX49	(24)						
0 CX50	24	0 CX50	(24)						
0 CX51	24	0 CX51	(24)						
0 CX52	24	0 CX52	(24)						
0 CX53	24	0 CX53	(24)						
0 CX54	24	0 CX54	(24)						
0 CX55	24	0 CX55	(24)						
0 CX56	24	0 CX56	(24)						
0 CX57	24	0 CX57	(24)						
0 CX58	24	0 CX58	(24)						
0 CX59	24	0 CX59	(24)						
0 CX60	24	0 CX60	(24)						
0 CX61	24	0 CX61	(24)						
0 CX62	24	0 CX62	(24)						
0 CX63	24	0 CX63	(24)						
0 CX64	24	0 CX64	(24)						
0 CX65	24	0 CX65	(24)						
0 CX66	24	0 CX66	(24)						
0 CX67	24	0 CX67	(24)						
0 CX68	24	0 CX68	(24)						
0 CX69	24	0 CX69	(24)						
0 CX70	24	0 CX70	(24)						
0 CX71	24	0 CX71	(24)						
0 CX72	24	0 CX72	(24)						
0 CX73	24	0 CX73	(24)						
0 CX74	24	0 CX74	(24)						
0 CX75	24	0 CX75	(24)						
0 CX76	24	0 CX76	(24)						
0 CX77	24	0 CX77	(24)						
0 CX78	24	0 CX78	(24)						
0 CX79	24	0 CX79	(24)						
0 CX80	24	0 CX80	(24)						
0 CX81	24	0 CX81	(24)						
0 CX82	24	0 CX82	(24)						
0 CX83	24	0 CX83	(24)						
0 CX84	24	0 CX84	(24)						
0 CX85	24	0 CX85	(24)						
0 CX86	24	0 CX86	(24)						
0 CX87	24	0 CX87	(24)						
0 CX88	24	0 CX88	(24)						
0 CX89	24	0 CX89	(24)						
0 CX90	24	0 CX90	(24)						
0 CX91	24	0 CX91	(24)						
0 CX92	24	0 CX92	(24)						
0 CX93	24	0 CX93	(24)						
0 CX94	24	0 CX94	(24)						
0 CX95	24	0 CX95	(24)						
0 CX96	24	0 CX96	(24)						
0 CX97	24	0 CX97	(24)						
0 CX98	24	0 CX98	(24)						
0 CX99	24	0 CX99	(24)						
0 CX100	24	0 CX100	(24)						

STATISTICS									
PROGRAM LENGTH	03								
UN LABELED COMMON LENGTH	10523								
	55*								

SYMBOLIC REFERENCE MAP (N=3)

VARIABLES	SN	TYPE	RELOCATION	REFS	2	DEFINED	5
0 NTH		INTEGER	ARRAY NTH	REFS	2	DEFINED	6
0 THA		REAL	THARG	REFS	2	DEFINED	9
0 THF		REAL	THFUN	REFS	2	DEFINED	9

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

NTH	2	0 NTH (2)
THARG	20	0 THA (20)
THFUN	20	0 THF (20)

STATISTICS

PROGRAM LENGTH	03	0
CM LABELED COMMON LENGTH	528	42


```

SUBROUTINE RANUM(SY,START,RN)
  IF (START.EQ.0.) GO TO 10
  CALL KANSET(START)
  START=0.
  5  10 RN=KANF(DUM1)
     IF (RN) 20,30,+0
  20  RN=RN
     RETURN
  30  RN=KANF(DUM2)*SIGN(1.,KANF(DUM3)-.5)
     RETURN
  40  CONTINUE
     RETURN
  END
  
```

RANUM
 RANUM
 RANUM
 RANUM
 RANUM
 RANUM
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 RANUM
 RANUM
 RANUM
 RANUM
 RANUM

SUBROUTINE NAME 74/74 OPT=1

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	10	12
3 NAME	1	5		
VARIABLES	SN	TYPE	RELOCATION	REFS
34 DUM1	REAL	*UNDEF		5
35 DUM2	REAL	*UNDEF		9
36 DUM3	REAL	*UNDEF		7
0 SN	REAL	F.P.		5
0 SN	REAL	F.P.		6
0 START	REAL	F.P.		2
EXTERNALS	TYPE	ARGS	REFERENCES	
NAME	1	3		
FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
NAME	REAL	1 INTRIN	5	2*9
SIZE	REAL	2 INTRIN	9	
STATEMENT LABELS	DEF LINE	REFERENCES		
12 10	5	2		
0 20	7	6		
20 30	9	6		
27 40	11	6		
STATISTICS				
PROGRAM LENGTH	373	31		

```

SUBROUTINE NORMAL(RX,XL,XU,MU,SIGMA,DUMMY)
  DIMENSION FZ(126)
  REAL MU
  DATA DT,DT1,NTP,NPT,SQ2PI/.01,.0,126,0.0,398942283/
  CLS=MU-.5*.SIGMA
  SUS=MU+.5*.SIGMA
  IF(XL.LT.SUS.AND.XU.GT.SLS) GO TO 10
  PRINT 301,CLS,SUS,XL,XU,MU,SIGMA
  FORMAT(11X,'LIMITS FOR NORMAL DISTRIBUTION SHOULD BE BETWEEN',F10.2,
    * AND',F10.2, * --- PROGRAM TERMINATED.'//',F10.2,*,F10.2,*,F10.2,*)
  STOP 123
  10 IF(NPT.NE.0) GO TO 2
  T2=DT1
  FZ(1)=.5
  FC=FZ(1)
  T=T+DT
  FF=SQ2PI*EXP(-.5*T*T)
  CF=FC+FF
  DT2=DT+.5
  NPT=1
  CONTINUE
  T=T+DT
  FZ(NPT)=FC
  FZ(NPT)=FF
  T2=T2+DT1
  IF(NPT.LT.NTP) GO TO 1
  CONTINUE
  2 RN=RANF(R)
  K=RN
  IF(XNLT+.5) X=1.-RN
  IF(X.GT.FZ(NPT)) GO TO 2
  DO 3 I=1,NPT
    IF(X.GT.FZ(I)) GO TO 4
    IF(I.EQ.1) GO TO 4
    X=1.-I
    X=X*DT1
    RX=X*(R-FZ(I-1))*DT1/(FZ(I)-FZ(I-1))
    GO TO 5
  3 CONTINUE
  4 PRINT 100
  FORMAT(13H0 ERROR DISRN)
  STO=
  CONTINUE
  5 CONTINUE
  IF(RN.LT+.5) RX=RX
  RX=SIGMA*RX+MU
  IF(XN.GT.XU) GO TO 2
  IF(XN.LT.XL) GO TO 2
  RETURN
  END

```

SYMBOLIC REFERENCE MAP (K=3)

ENTRY POINTS DEF LINE REFERENCES
J NORMAL 1 55

VARIABLES SN TYPE RELOCATION

125 OT	REAL	REFS	19	22	DEFINED	4	42
126 OT1	REAL	REFS	14	23	DEFINED	41	
207 UT2	REAL	REFS	24	DEFINED	19		
210 F	REAL	REFS	24	DEFINED	23		
204 FC	REAL	REFS	24	DEFINED	16		24
206 FP	REAL	REFS	24	DEFINED	18		
210 F2	REAL	REFS	2	15	35		34.2
213 I	INTEGER	REFS	15	23	DEFINED	36	
213 MU	REAL	REFS	37	34	39	34.2	DEFINED
213 MU	REAL	REFS	3	5	6	52	
130 NPI	INTEGER	REFS	1	27	28	38	35
127 NTP	INTEGER	REFS	4	20	27		
212 K	REAL	REFS	30	DEFINED	4		
211 KN	REAL	REFS	32	37	42	DEFINED	33
211 KN	REAL	REFS	33	234	51	DEFINED	32
211 KN	REAL	REFS	51	52	54	DEFINED	1
211 KN	REAL	REFS	51	52			42
211 KN	REAL	REFS	49				
211 KN	REAL	REFS	5	5	52	DEFINED	1
211 KN	REAL	REFS	7	3	DEFINED	5	
211 KN	REAL	REFS	18	23	DEFINED	4	
211 KN	REAL	REFS	7	3	DEFINED	6	
211 KN	REAL	REFS	2+10	22	2+23	26	DEFINED
211 KN	REAL	REFS	26	23	DEFINED	14	17
211 KN	REAL	REFS	40	41	DEFINED	39	24
211 KN	REAL	REFS	7	3	DEFINED	1	40
211 KN	REAL	REFS	7	3	DEFINED	1	1
211 KN	REAL	REFS	42	DEFINED	41		

FILE NAMES INPUT

WRITES

REFERENCES

LIBRARY

ARG3

TYPE

REAL

EXTERNALS

EXP

REFERENCES

LIBRARY

ARG3

TYPE

REAL

EXTERNALS

EXP

INLINE FUNCTIONS TYPE ARG3 DEF LINE REFERENCES

ABS REAL 1 INTRIN 26

MANF REAL 1 INTRIN 32

STATEMENT LABELS DEF LINE REFERENCES

32 1 21 26 30

34 2 31 13 35

104 3 44 36 37

110 4 48 38

111 5 50 39

17 10 13 7

171 100 FMT 40 45

143 901 FMT 9 8

SUBROUTINE NORMAL				74/74	OPT=1	PROPERTIES	
LJOBS LABEL		INDEX	FROM-TO	LENGTH		OPT	EXITS
73	3	1	36-44	138			
STATISTICS							
PROGRAM LENGTH				4168	270		

```

SUBROUTINE MCARL0(INSTR,MODE,ITSNDX)
COMMON /C/ C(3630)
EQUIVALENCE (C( 80), RLM)
EQUIVALENCE (C(1561), RSM)
EQUIVALENCE (C(1571), RSY)
EQUIVALENCE (C(2000), T)
EQUIVALENCE (C(1594),TMC2)
EQUIVALENCE (C(1565),TMC2)
EQUIVALENCE (C(1574),ZMC2)
EQUIVALENCE (C(1575),ZMC2)
EQUIVALENCE (C(2684), DT)
EQUIVALENCE (C(2765), NTH)
EQUIVALENCE (C(2775), TM)
EQUIVALENCE (C(2785), TRMS2)
EQUIVALENCE (C(2795), TRMS)
EQUIVALENCE (C(2805), TMU)
EQUIVALENCE (C(2815), TMM)
EQUIVALENCE (C(2825), TSIG)
EQUIVALENCE (C(3512), TSIG)
EQUIVALENCE (C(3514), SIGMA)
EQUIVALENCE (C(3594), SIGLB)
EQUIVALENCE (C(3594), SIGUB)
EQUIVALENCE (C(3634), ISNDX)
EQUIVALENCE (C(3674), IDIST)
EQUIVALENCE (C(3511),TRANSF)
EQUIVALENCE (C(3721), ITCT)
EQUIVALENCE (C(3723), TSUM)
EQUIVALENCE (C(3733), TLR)
EQUIVALENCE (C(3743), TUB)
EQUIVALENCE (C(3753), ITNOX)
EQUIVALENCE (C(3763), IDIST)
EQUIVALENCE (C(3773), TSPER)
EQUIVALENCE (C(3783), TYPPEH)
EQUIVALENCE (C(3793), TPGIG)
EQUIVALENCE (C(3813), ITNOX2)
EQUIVALENCE (C(3803), INXST)
DIMENSION SIGMA(40),SIGUB(40),SIGLB(40),ISNDX(40),IDIST(40)
DIMENSION TSUM(10),TLR(10),TUB(10),ITNOX(10),IDIST(10)
*TSPEK(10),TYPPEH(10),TPGIG(10),ITNOX2(10),INXST(10)
DIMENSION SVC(40),SVCT(40),IDIST(7)
DIMENSION INIT(40)
DIMENSION NTH(10), TM(10), TRMS2(10), TRMS(10), TMJ(10), TVM(10),
1 TSIG(10)
DATA CPEHY/10HR /
DATA INIT/40*0/
DATA COEF1/13.0537351/
DATA COEF2/165.4366343/
DATA COEF3/23.10344002/
DATA CPEHY/
DATA (IDIST(1:10),IA=1,71/6,NORMAL,7HUNIFORM,7H2-ORDER,7H
*1-ORDER,7H2-ORDER,7H2-ORDER)
ENSTRT=INXST
I=ITSNDX
IF (MODE.EQ.2) GO TO 300
WRITE(6,2100)
WRITE(6,2103)

```

[illegible]

```

117 C      TEST FLIGHT TIME AGAINST NEXT SAMPLE TIME FOR
118 C      EACH TIME SERIES ERROR SOURCE. FOR THOSE TIME
119 C      SERIES ERROR SOURCES HAVING A NEXT SAMPLING TIME,
120 C      TNSX(I), LESS THAN OR EQUAL TO THE SIMULATION
121 C      TIME, T, DETERMINE THE TIME SERIES ERROR SOURCE
122 C      MONTE CARLO VALUE.
123 C
124 C
125 C      300 IF (ITCT.LE.0) GO TO 1000
126 C      IF (MODE.EQ.4) TNSX(I) = 0.
127 C      IF (C(1378).LE.0.) GO TO 1000
128 C      IF (C(1200).LT.TNSX(I)+TNSX(I)) GO TO 1000
129 C      IS = IISNOX
130 C      ITT = ITTIST(I) + 1
131 C
132 C
133 C      DETERMINE IF THE TIME SERIES PERIOD IS DETERMINISTIC
134 C      (TTPER(I).GT.0) OR STOCHASTIC (TTPER(I).EQ.0).
135 C
136 C      IF (TTPER(I).GT.0.) GO TO 311
137 C
138 C
139 C      INCREMENT THE I3 TH TIME SERIES ERROR SOURCE BY
140 C      THE VALUE OF THE DETERMINISTIC PERIOD, TSPER(I3)
141 C
142 C
143 C      TNSX(I3) = C(2000) + TSPER(I3)
144 C      GO TO 312
145 C
146 C      311 XNU = TNSX(I3) + TSPER(I3)
147 C      XL = INX(I3)
148 C      XU = XNU + TSPER(I3)
149 C      SGMA = TSPG(I3)
150 C      CALL NORM(RX,XL,XU,XNU,SGMA,RNSTRT)
151 C
152 C
153 C      INCREMENT THE I3 TH TIME SERIES ERROR SOURCE BY
154 C      A NORMALLY DISTRIBUTED RANDOM VALUE, WHERE THE
155 C      RANDOM VALUES BOUNDED TO LIE BETWEEN ZERO AND
156 C      TWICE THE PERIOD MEAN VALUE, TSPER(I3).
157 C
158 C
159 C      TNSX(I3) = RX
160 C      312 CONTINUE
161 C      JU = IINX(I3)
162 C      JW = IJW(I3)
163 C      IF (MODE.EQ.4) SVCT(I) = C(JU)
164 C      XNU = SVCT(I)
165 C      IF (JU.NE.JW) XNU = C(JW)
166 C      XL = I3 + I3
167 C      XU = I3 + I3
168 C      SGMA = TSPG(I3)
169 C      1306 IF (ITDST(I3).LE.0) GO TO 1307
170 C      GO TO 1304 + 305 + 306 + 307 + 308 + 309 + 310 + 311 + 312
171 C
172 C      1307 CONTINUE

```


SUBROUTINE	MCARLO	74/74	OPT=1	FTN ++2+7+353	07/0775	11.05.10.	PAGE
	178				MCARLO	178	
			DETERMINE THE NORMALLY DISTRIBUTED IS TH ERROR		MCARLO	174	
			SOURCE MONTE CARLO VALUE		MCARLO	175	
175	C				MCARLO	176	
					MCARLO	177	
			CALL NORM(RX,XL,XU,XMU,SGMA,RNSTR)		MCARLO	178	
			CTIME=RX		MCARLO	179	
			GO TO 303		MCARLO	180	
180	C	304	CONTINUE		MCARLO	181	
					MCARLO	182	
					MCARLO	183	
185	C		DETERMINE THE UNIFORMALLY DISTRIBUTED IS TH ERROR		MCARLO	184	
			SOURCE MONTE CARLO VALUE		MCARLO	185	
					MCARLO	186	
					MCARLO	187	
			CALL RANUM (1., RNSTR, RX)		MCARLO	188	
			ZMU=SVCT(I9)		MCARLO	189	
			IF (JU.NE.14) ZMU=C(JU)		MCARLO	190	
190	C		CTIME = SVCT(I9) + (RX+TFUBST) - T(I9) + T(I9) + T(I9) + T(I9)		MCARLO	191	
			GO TO 303		MCARLO	192	
					MCARLO	193	
					MCARLO	194	
195	C		DETERMINE THE CORRELATED NORMAL IS TH ERROR SOURCE		MCARLO	195	
			MONTE CARLO VALUE		MCARLO	196	
					MCARLO	197	
					MCARLO	198	
					MCARLO	199	
200	C	305	IF (MU2.NE.4) GO TO 330		MCARLO	200	
			GO TO 1000		MCARLO	201	
			CALL NORM(RSX,-3.,3.,0.,1.,RNSTR)		MCARLO	202	
			YMC = (MU(I9)		MCARLO	203	
			YMC2 = TRMS(I9)		MCARLO	204	
			GO TO 303		MCARLO	205	
205	C	340	IF (MU2.NE.4) GO TO 341		MCARLO	206	
			GO TO 1000		MCARLO	207	
			CALL NORM(RSY,-3.,3.,0.,1.,RNSTR)		MCARLO	208	
			ZMC = TMU(I9)		MCARLO	209	
			ZMC2 = TRMS(I9)		MCARLO	210	
210	C	350	IF (MU2.NE.4) GO TO 351		MCARLO	211	
			NTM(I9) = 0		MCARLO	212	
			TM(I9) = 0		MCARLO	213	
			TRMS2(I9) = 0		MCARLO	214	
			GO TO 1000		MCARLO	215	
215	C	351	CALL NORM (RL4,-3.,3.,0.,1.,RNSTR)		MCARLO	216	
			CONTINUE		MCARLO	217	
			NTM(I9) = NTM(I9) + 1		MCARLO	218	
			TM(I9) = TM(I9) + C(JU)		MCARLO	219	
			TRMS2(I9) = (TRMS2(I9) + C(JU)*C(JU))		MCARLO	220	
220	C		CALCULATE TIME SERIES ROOT MEAN SQUARE		MCARLO	221	
			TRMS(I9) = SQRTRMS2(I9)/NTM(I9)		MCARLO	222	
					MCARLO	223	
225	C		CALCULATE TIME SERIES MEAN VALUES		MCARLO	224	
					MCARLO	225	
					MCARLO	226	
					MCARLO	227	
			TMU(I9) = TM(I9)/NTM(I9)		MCARLO	228	
			GO TO 1000		MCARLO	229	

SUBROUTINE	MCARL0	74/74	OPT=1	FTN	..2+7+355	07/07/76	11.05.10.	PAGE	5
230	ENTRY MCARL0 WRITE(6,7440) DO 1001 I=1,ITCF					MCARL0	230		
						MCARL0	231		
	0					MCARL0	232		
	0					MCARL0	233		
235	0					MCARL0	234		
	0					MCARL0	235		
	0					MCARL0	236		
	0					MCARL0	237		
	0					MCARL0	238		
	0					MCARL0	239		
240	0					MCARL0	240		
	0					MCARL0	241		
	1001 CONTINUE 7440 FORMAT(30X,30HMONTE CARLO TIME SERIES VALUES//, 1,20X,7HC-INDEX,5X,4HMEAN,8X,8HVARIANCE,4X,7HSTD DEV,5X,3HMS//) 7443 FORMAT(25X,15,8X,78.3,4X,78.3,4X,78.3,4X,78.3) GO TO 1000					MCARL0	242		
245	0					MCARL0	243		
	0					MCARL0	244		
	0					MCARL0	245		
	0					MCARL0	246		
	0					MCARL0	247		
250	0					MCARL0	248		
	0					MCARL0	249		
	0					MCARL0	250		
	0					MCARL0	251		

SUBROUTINE MCARLU		7474	OPT=1	CTN +.2+74.355	07/0775	11.05.10.	PAGE
CARD NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM				6
235	1	ITCF	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				
239	1	ITCF	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				

SYMBOLIC REFERENCE MAP (N=3)

ENTRY POINTS DEF LINE REFERENCES

3 MCARLC 229 249

VARIABLES IN TYPE A-ARRAY C

VARIABLES	IN	TYPE	A-ARRAY	C	REFS	2	3	4	5	6	7	8
0 C		REAL			9	10	11	12	13	14	15	16
410 GUSF1	*	REAL			17	18	19	20	21	22	23	24
411 GUSF2	*	REAL			25	26	27	28	29	30	31	32
412 GUSF3	*	REAL			33	34	35	36	37	38	39	40
407 CPERY	*	REAL			41	42	43	44	45	46	47	48
3197 OF		REAL			49	50	51	52	53	54	55	56
273 I		INTEGER			57	58	59	60	61	62	63	64
602 13		INTEGER			65	66	67	68	69	70	71	72
7131 I0IST		INTEGER	ARRAY	C	73	74	75	76	77	78	79	80
726 I0IST		INTEGER	ARRAY		81	82	83	84	85	86	87	88
735 INIT		INTEGER	ARRAY		89	90	91	92	93	94	95	96
7061 ISNDX		INTEGER	ARRAY	C	97	98	99	100	101	102	103	104
7210 ITCT		INTEGER	ARRAY	C	105	106	107	108	109	110	111	112
7262 ITDST		INTEGER	ARRAY	C	113	114	115	116	117	118	119	120
7290 ITNDX		INTEGER	ARRAY	C	121	122	123	124	125	126	127	128
7344 ITNDX2		INTEGER	ARRAY	C	129	130	131	132	133	134	135	136
7344 ITNDX2		INTEGER	ARRAY	C	137	138	139	140	141	142	143	144
603 IIT	*	INTEGER			145	146	147	148	149	150	151	152
574 JU		INTEGER			153	154	155	156	157	158	159	160
604 JM		INTEGER			161	162	163	164	165	166	167	168
413 ETST	*	INTEGER			169	170	171	172	173	174	175	176
0 MUJE		INTEGER			177	178	179	180	181	182	183	184
5314 NIM		INTEGER	ARRAY	C	185	186	187	188	189	190	191	192
5066 FANST		REAL			193	194	195	196	197	198	199	200
73 RCM		REAL			201	202	203	204	205	206	207	208
0 RNSTAT		REAL			209	210	211	212	213	214	215	216
5010 RSK		REAL			217	218	219	220	221	222	223	224
5042 RSY		REAL			225	226	227	228	229	230	231	232
575 RK		REAL			233	234	235	236	237	238	239	240
577 SNA		REAL			241	242	243	244	245	246	247	248
5741 SISLO		REAL	ARRAY	C	249	250	251	252	253	254	255	256

VARIABLES	SN	TYPE	RELOCATION	REFS	20	37	79	83	96
3671 SIGMA	REAL	ARRAY	C	REFS	20	37	79	83	96
7011 SIGSUB	REAL	ARRAY	C	REFS	22	37	79	84	96
606 SVC	REAL	ARRAY	C	REFS	40	79	86	94	96
				DEFINED	73				
656 SVCT	REAL	ARRAY	C	REFS	40	163	188	198	162
3717 T	REAL	ARRAY	C	REFS	6				
7224 TFS	REAL	ARRAY	C	REFS	20	39	165	2*190	
3326 TM	REAL	ARRAY	C	REFS	13	42	218	212	218
3384 TMJ	REAL	ARRAY	C	REFS	16	42	201	207	241
				DEFINED	237				
7332 TNXSI	REAL	ARRAY	C	REFS	36	39	127	145	146
				DEFINED	125	143	158		
7320 TP3IG	REAL	ARRAY	C	REFS	34	39	148		
3352 TRXS	REAL	ARRAY	C	REFS	15	42	202	208	2*235
				DEFINED	223				241
3340 TRXS2	REAL	ARRAY	C	REFS	14	42	219	223	213
7212 TSOMA	REAL	ARRAY	C	REFS	27	39	167	198	219
3410 TSIG	REAL	ARRAY	C	REFS	18	42	241	DEFINED	239
7274 TSPER	REAL	ARRAY	C	REFS	32	39	143	145	147
7236 TJB	REAL	ARRAY	C	REFS	29	39	166	198	
3376 TVM	REAL	ARRAY	C	REFS	17	42	239	241	235
7306 TYPPE	REAL	ARRAY	C	REFS	33	39	136	DEFINED	
278 XL	REAL	ARRAY	C	REFS	87	143	177	DEFINED	146
601 XMJ	REAL	ARRAY	C	REFS	47	147	149	177	86
				DEFINED	164				145
600 XU	REAL	ARRAY	C	REFS	87	163	177	DEFINED	166
6033 YMC	REAL	ARRAY	C	REFS	7	DEFINED	201		
3034 YMS2	REAL	ARRAY	C	REFS	8	DEFINED	202		
3045 ZMC	REAL	ARRAY	C	REFS	9	DEFINED	207		
3046 ZMS2	REAL	ARRAY	C	REFS	10	DEFINED	208		
609 ZMJ	REAL	ARRAY	C	REFS	100	149			
				DEFINED	199				

FILE NAMES	MODE	ARITES	56	57	91	94	96	230	241	247
TAPED	FMT									
EXTERNALS	TYPE	ARG3	REFERENCES	177	203	206	215			
NORM	3	97	149							
RANUM	77	187	239							
SST	1 LIBRARY	223								

STATEMENT LABELS	DEF	LINE	REFERENCES	89
71 1	92	80		
116 13	97	79		
30 50	75	71		
21 81	59	55		
45 100	81	76		
63 201	90	81		
117 300	124	54		
219 304	181	159		
234 309	189	189		
270 309	216	179		
137 311	145	136		
192 312	159	144		
237 333	200	198		
240 343	204	199		
241 341	206	204		
260 350	210	199		

SUBROUTINE MCARLO 74/74 OPT=1			
STATEMENT LABELS	DEF LINE	REFERENCES	
265 351	215	210	
342 360	247	2469	
105 737	96	93	
346 1000	249	58	
		246	
		231	
0 1001	242		
		169	
		171	
207 1307	171	158	
403 2100	106	56	
504 2131	109	94	
472 2103	107	57	
512 2135	110	96	
447 2080	90	91	
534 7440	243	230	
547 7443	245	241	
500 3621	245	247	
LOOPS LABEL INDEA FROM-TO LENGTH PROPERTIES EXT REFS			
320 1001	18	231 242	223
COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH) U C (3930)			
EQUIV CLASSES LENGTH MEMBERS - BIAS NAME(LENGTH) U C			
1564 YMC2 (1)	1564 YMC2 (1)	1564 YMC2 (1)	1564 YMC2 (1)
1974 YMC2 (1)	1974 YMC2 (1)	1974 YMC2 (1)	1974 YMC2 (1)
2764 NIM (1)	2764 NIM (1)	2764 NIM (1)	2764 NIM (1)
2794 TRMS (1)	2794 TRMS (1)	2794 TRMS (1)	2794 TRMS (1)
2424 TSIG (1)	2424 TSIG (1)	2424 TSIG (1)	2424 TSIG (1)
3513 S16M4 (40)	3513 S16M4 (40)	3513 S16M4 (40)	3513 S16M4 (40)
3633 ISNOX (40)	3633 ISNOX (40)	3633 ISNOX (40)	3633 ISNOX (40)
3722 ISOMA (10)	3722 ISOMA (10)	3722 ISOMA (10)	3722 ISOMA (10)
3752 ITNOX (10)	3752 ITNOX (10)	3752 ITNOX (10)	3752 ITNOX (10)
3762 TYPERK (10)	3762 TYPERK (10)	3762 TYPERK (10)	3762 TYPERK (10)
3812 ITNOX2 (10)	3812 ITNOX2 (10)	3812 ITNOX2 (10)	3812 ITNOX2 (10)
1568 RSX (1)	1568 RSX (1)	1568 RSX (1)	1568 RSX (1)
1570 RSY (1)	1570 RSY (1)	1570 RSY (1)	1570 RSY (1)
1999 T (1)	1999 T (1)	1999 T (1)	1999 T (1)
2774 TM (1)	2774 TM (1)	2774 TM (1)	2774 TM (1)
2804 TMU (1)	2804 TMU (1)	2804 TMU (1)	2804 TMU (1)
3510 RANSTT (1)	3510 RANSTT (1)	3510 RANSTT (1)	3510 RANSTT (1)
3523 S16M4 (40)	3523 S16M4 (40)	3523 S16M4 (40)	3523 S16M4 (40)
3623 ITDST (40)	3623 ITDST (40)	3623 ITDST (40)	3623 ITDST (40)
3732 TUB (1)	3732 TUB (1)	3732 TUB (1)	3732 TUB (1)
3772 TSPER (1)	3772 TSPER (1)	3772 TSPER (1)	3772 TSPER (1)
3812 INKST (1)	3812 INKST (1)	3812 INKST (1)	3812 INKST (1)

STATISTICS
PROGRAM LENGTH 10058 517
COMMON LENGTH 73563 3430

SUBROUTINE	CEPAS	74/74	UPT=1	FTN .2.74.355	07/07/75	11.05.19.	PAGE	1
5	SUBROUTINE CEPASIMP,INVSIM,IPLOT,XLAMBD,KSSIG,CEPSIG,PSIZE COMMON/CEPAS/X(100),Y(100) DIMENSION CRIT(100) REAL KSSIG INTEGER CEPSIG WRITE(6,2003) 2003 FORMAT(1H,39HCEPAS PARAMETER CONTROL CARD INPUT DATA) WRITE(6,2004)NP,INVSIM,IPLOT,XLAMBD,KSSIG,CEPSIG(IJ),J=1,5) 2004 FORMAT(1X,31HNPJT MISS DISTANCE COORDINATES///) 2005 FORMAT(1X,31H,2(1X,F10.3),5I6) DO 2 1=1,15 IF(CEPSIG(I).GT.0) GO TO 5 CEPSIG(I)=-1 5 CONTINUE NUG=(NP-1)/15 NUG=NUG+1 WRITE(6,2006) 2006 FORMAT(1X,2HX=) WRITE(6,2007)(X(I),I=1,NP) 2007 FORMAT(10(2X,F7.3)) WRITE(6,2008) 2008 FORMAT(1X,2HY=) WRITE(6,2009)(Y(I),I=1,NP) CALL CEPP (X,Y,NP,KSSIG,XLAMBD,INVSIM,CEPSIG,IPLOT,PSIZE) RETURN END							MCARL3 252 MCARL3 253 MCARL3 254 MCARL3 255 MCARL3 256 MCARL3 257 MCARL3 258 MCARL3 259 MCARL3 260 MCARL3 261 MCARL3 262 MCARL3 263 MCARL3 264 MCARL3 265 MCARL3 266 MCARL3 267 MCARL3 268 MCARL3 269 MCARL3 270 MCARL3 271 MCARL3 272 MCARL3 273 MCARL3 274 MCARL3 275 MCARL3 276 MCARL3 277 MCARL3 278 MCARL3 279

SYMBOLIC REFERENCE MAP (K=J)										
ENTRY POINTS		DEF LINE	REFERENCES							
3 CEPAS		1	27							
VARIABLES		SN	TYPE	RELOCATION						
0	CEPASS	INTEGER	ARRAY	F.P.	REFS	1	15	9	14	26
101	CRIT	REAL	*UNDEF		DEFINED	1				
137	I	INTEGER			REFS	4				
					REFS	14				
					REFS	25				21
0	I3VNSM	INTEGER		F.P.	REFS	9	25	DEFINED	1	
0	IPLOT	INTEGER		F.P.	REFS	9	DEFINED	9	1	
150	JJ	INTEGER			REFS	5	3	26	DEFINED	1
0	KSSIG	REAL		F.P.	REFS	9	17	21	25	26
0	NP	INTEGER		F.P.	DEFINED	1				
160	NU2	INTEGER			REFS	10	DEFINED	17	10	
0	PSIZE	REAL	ARRAY	F.P.	REFS	26	DEFINED	1		
0	X	REAL	ARRAY	CEPASS	REFS	2	21	26		
0	XLAMB	REAL	ARRAY	F.P.	REFS	9	25	DEFINED	1	
144	Y	REAL	ARRAY	CEPASS	REFS	2	25	26		
FILE NAMES										
1449	FMT		WRITES	7		9	18	19	21	25
EXTERNALS										
CEPP	TYPE	ARGS	REFERENCES							
9			26							
STATEMENT LABELS										
DEF LINE	REFERENCES									
17 5	15									
134 2000	FMT	20	19	14						
142 2001	FMT	22	21	25						
150 2002	FMT	24	23							
175 2003	FMT	6	7							
125 2004	FMT	12	9							
117 2005	FMT	11	10							
LOOPS LABEL										
INDEX	FROM-TO	LENGTH	PROPERTIES							
15 5	13 16	33	INSTACK							
COMMON BLOCKS										
CEPASS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)							
200		8 X	11000							
STATISTICS										
PROGRAM LENGTH		3253	213							
CM LABELED COMMON LENGTH		3109	200							


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SUBROUTINE CEPP(X,Y,NP,KSSIG,XLAMBDA,IBVNSW,CEPSIG,IPLOT,PSIZE)
  REAL KSSIG
  INTEGER CEPSIG
  DIMENSION ZXX(100),ZYY(100)
  DIMENSION TITLE(6),TITLE2(6)
  DIMENSION ICHI(6)
  DIMENSION OMIS(6,50)
  DIMENSION X(100),Y(100),SORTX(100),DIST(100),CEPSIG(5),ICONREF(5),
  * RCONF(16),RCONF2(6)
  DATA ISKSW/0/
  DATA (CHI2(1,1),I=1,50)/0.0201,0.292,0.072,1.65,2.55,3.57,4.66,
  * 5.81,7.01,8.26,9.54,10.91,12.21,13.6,15.0,16.4,17.8,19.2,20.7,22.2,
  * 23.7,25.1,26.7,28.2,29.7,31.2,32.6,34.1,35.5,37.0,38.4,39.9,41.3,42.8,
  * 44.3,45.7,47.1,48.6,50.0,51.5,53.0,54.5,56.0,57.5,59.0,60.5,62.0,
  * 63.5,65.0,66.5,68.0,70.0/
  DATA (CHI2(2,1),I=1,50)/0.103,0.711,1.64,2.73,3.94,5.23,6.57,
  * 7.95,9.39,10.9,12.5,14.1,15.8,17.5,19.2,21.0,22.7,24.5,26.3,28.1,
  * 29.9,31.7,33.5,35.3,37.1,38.9,40.7,42.5,44.3,46.1,47.9,49.7,51.5,
  * 53.3,55.1,56.9,58.7,60.5,62.3,64.1,65.9,67.7,69.5,71.3,73.1,75.0,
  * 76.8,78.6,80.4,82.2,84.0/
  DATA (CHI2(3,1),I=1,50)/0.211,1.06,2.28,3.49,4.97,6.3,7.79,9.31,
  * 10.5,12.1,14.0,15.7,17.3,19.0,20.6,22.3,24.0,25.6,27.3,29.1,
  * 30.8,32.5,34.2,35.9,37.7,39.4,41.2,42.9,44.7,46.5,48.2,50.0,51.8,
  * 53.5,55.3,57.1,58.9,60.7,62.5,64.3,66.1,67.9,69.7,71.5,73.3,75.1,
  * 76.9,78.7,80.5,82.3,84.2,86.0,87.8,89.6,91.4,93.2,95.0,96.8,98.6,
  * 100.0/
  DATA (CHI2(4,1),I=1,50)/0.446,1.65,3.07,4.59,6.18,7.81,9.4,11.2,
  * 12.9,14.6,16.3,18.0,19.8,21.6,23.4,25.1,26.9,28.7,30.5,32.3,34.2,
  * 36.0,37.8,39.6,41.4,43.2,45.0,46.8,48.6,50.4,52.2,54.0,55.8,57.6,
  * 59.4,61.2,63.0,64.8,66.6,68.4,70.2,72.0,73.8,75.6,77.4,79.2,81.0,
  * 82.8,84.6,86.4,88.2,90.0,91.8,93.6,95.4,97.2,99.0,100.0/
  DATA (CHI2(5,1),I=1,50)/0.713,2.3,3.9,5.5,7.2,8.9,10.6,12.3,14.0,15.7,
  * 17.4,19.1,20.8,22.5,24.2,25.9,27.6,29.3,31.0,32.7,34.4,36.1,37.8,
  * 39.5,41.2,42.9,44.6,46.3,48.0,49.7,51.4,53.1,54.8,56.5,58.2,60.0,
  * 61.7,63.4,65.1,66.8,68.5,70.2,71.9,73.6,75.3,77.0,78.7,80.4,82.1,
  * 83.8,85.5,87.2,88.9,90.6,92.3,94.0,95.7,97.4,99.1,100.0/
  DATA (TITLE(1),I=1,6)/6HCEP CO,6HNFIDEN,6HCE CIR,5HOLE FO,
  * 6H LAMBDA,6HMDA /
  DATA (TITLE2(1),I=1,6)/6HCEP CO,6HNFIDEN,5HCE CIR,5HOLE FO,
  * 5H LAMBDA,5HMDA /
  DATA ICONREF/99,95,90,80,70/
  DATA SORTX/100*0.1/

  ** X= ARRAY OF X-COMPONENT OF MISS DISTANCES
  ** Y= ARRAY OF Y-COMPONENT OF MISS DISTANCES
  ** NP= NUMBER OF POINTS
  ** KSSIG= SIGNIFICANCE LEVEL FOR K-S TEST DESIRED -- SET
  ** NEGATIVE IF NO K-S TEST DESIRED
  ** ALAMBDA= (PROGRAM CEPI) / (MISSILE CEPI) --
  ** SET TO ZERO IF NO ESTIMATE OF PROGRAM CEP IS MADE
  ** IBVNSW=1 IF DESIRE TO USE BIVARIATE NORMAL ASSUMPTION
  ** REGARDLESS OF OUTCOME OF K-S TEST --- SET NOT = 1 TO USE
  ** BIVARIATE NORMAL ONLY IF K-S TEST DOES NOT REJECT
  ** ASSUMPTION OF NORMALITY. IF NOT =1, AND DATA FAILS K-S TEST
  ** FOR NORMALITY, CEP WILL BE
  ** CALCULATED AS THE ARGUMENT OF A GUESS-CONTAINING
  ** ONE-HALF OF THE SAMPLE POINTS.
  ** CEPSIG= SIGNIFICANCE LEVELS AT WHICH CEP CONFIDENCE

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C
C      INTERVALS) PRINT IS DESIRED.  PRELOAD TO NEGATIVE NUMBERS
C      IN CALLING PROGRAM BEFORE ENTERING DESIRED CONFIDENCE LEVELS
C      ENTER AS AN INTEGER (IN PERCENT) -- EG., IF DESIRE
C      R(10.99), R(10.90), AND R(10.70), ENTER (FOR EXAMPLE)
C      CEPSIG(1)=99, CEPSIG(2)=99, AND CEPSIG(3)=70.  NO ORDER
C      NEEDS TO BE OBSERVED.
C      * * * * * PLOT=1 FOR PLOTS OF CEPSIG AND POINTS, NOT=1 OTHERWISE
C
C      KSSIG=0.05
C      NCONF=0
C      EPSLN=.00001
C      69.0 CONTINUE
C      WRITE(10,19)
C      1019 FORMAT(1M1)
C      IF (IMP.LE.0) GO TO 300
C
C      * * * * * CALCULATE SAMPLE SIGMA-X, SIGMA-Y, X-MEAN, AND Y-MEAN
C
C      SUMX2=0.
C      SUMY2=0.
C      XBAR=0.
C      YBAR=0.
C      DO 1 I=1,NP
C      SUMX2=SUMX2 + X(I)**2
C      SUMY2=SUMY2 + Y(I)**2
C      XBAR=XBAR + X(I)
C      YBAR=YBAR + Y(I)
C      1 XBAR = XBAR / NP
C      YBAR = YBAR / NP
C      SXHAT2=(SUMX2 - (XBAR**2)*NP)/(NP - 1)
C      SYHAT2=(SUMY2 - (YBAR**2)*NP)/(NP - 1)
C      SXHAT= SQRT(SXHAT2)
C      SYHAT= SQRT(SYHAT2)
C
C      * * * * * KOLMOGOROV-SMIRNOV TEST FOR NORMALITY
C
C      * * * * * CHECK X
C
C      NI=0
C      CALL KSTEST(X,NP,KSSIG,SUAR,SXHAT,NI)
C      NEX=NI
C
C      * * * * * CHECK Y
C
C      CALL KSTEST(Y,NP,KSSIG,YBAR,SYHAT,NI)
C      NIY=NI
C      IF (NEX.GT.0) WRITE(10,1001)KSSIG
C      1001 FORMAT(1X,10HX-COMPONENT OF MISS DISTANCE FAIL K-S TEST FOR NORMAL
C      *ITY AT F10.5,2X,10HSIGNIFICANCE LEVEL)
C      WRITE(10,1078)
C      IF (NIY.GT.0) WRITE(10,1002)KSSIG
C      1002 FORMAT(1X,10HX-COMPONENT OF MISS DISTANCE FAIL K-S TEST FOR NORMAL
C      *ITY AT F10.5,2X,10HSIGNIFICANCE LEVEL)
C      IF (EVENSW.EQ.1) GO TO 450

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115 IF (INX.GT.0.0) GO TO 400
C * * * DETERMINE CONSTANT XK FOR ELLIPTICAL TO CEP CONVERSION
C
450 SSMIN=AMIN1(SXAT,SYAT)
SSMAX=AMAX1(SXAT,SYAT)
RATIOX=SSMIN/SSMAX
RATIOY=SSMIN/SSMAX
IF (RATIOX.GE.0.3) GO TO 102
XK=0.9488+RATIOX**2 - 0.0495*RATIOX + 0.675
103 CEP=KX*SSMAX
GO TO 121
102 CEP=0.015*SSMIN + 0.562*SSMAX
C * * * CALCULATE CONFIDENCE INTERVALS
C
IF (NF.GT.1) GO TO 545
WRITE(6,1074)
WRITE(6,1073)
WRITE(6,1072)
1112 F0=41.0, F1=HNO CONFIDENCE INTERVALS CALCULATED BECAUSE NUMBER OF
*POINTS NP=15, WHICH IS LESS THAN 21
GO TO 223
545 CONTINUE
121 NCONF=0
140 IF (CEP.SIG(1).LE.0) GO TO 528
ICHI(1)=1
IF (CEP.SIG(2).LE.0) GO TO 4
NCONF=NCONF + 1
IF (CEP.SIG(3).EQ.93) ICHI(1)=1
IF (CEP.SIG(4).EQ.93) ICHI(1)=2
IF (CEP.SIG(5).EQ.90) ICHI(1)=3
IF (CEP.SIG(6).EQ.90) ICHI(1)=4
IF (CEP.SIG(7).EQ.70) ICHI(1)=5
IF (ICHI(1).GT.0) GO TO 44
WRITE(6,1007) CEP, SIG(1)
NCONF=NCONF + 1
44 IF (CEP.SIG(1).LE.0) GO TO 526
* CONTINUE
1007 F0=41.0, F1=HNO CONFIDENCE LEVEL OF 1+2X20 ENTERED WHICH IS NOT TA
*BLD, 2X, 31 HNO CONFIDENCE INTERVAL COMPUTED
526 CEP=CEP
NCONF=NCONF + 1
NUS=NU
NU=NU/2
IF (NCONF.LE.0) GO TO 528
DO 3 I=1, NCONF
J=ICHI(I)
5 NCONF=NU-CEP*SQRT(NU*(1+CEP**2))
IF (KLAMBDA.LT.EPSLN) GO TO 528
257 CEP=CEP/SQRT(1+KLAMBDA**2)
IF (NCONF.LE.0) GO TO 528
DO 3 I=1, NCONF
J=ICHI(I)
6 NCONF=NU-CEP*SQRT(NU*(1+CEP**2))
IF (KLAMBDA.LT.EPSLN) GO TO 528
528 WRITE(6,1010) CEP, NP

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230 C * * * SORT DISTANCES IN INCREASING ORDER
      NO=NP
      ISV=0
      NS=0
      DO 3 I=1,NO
        IF (DIST(I).GE.COMPR) GO TO 3
        ISV=I
        COMPR=DIST(I)
      3 CONTINUE
      NS=NS+1
      SORTX(NS)=COMPR
      DIST(NS)=DIST(ND)
      ND=ND-1
      IF (ND.GT.1) GO TO 402
      NS=NS+1
      SORTX(NS)=DIST(I)
      C * * * DETERMINE IF NUMBER OF POINTS, NP, IS EVEN OR ODD
      ND=NP/2
      NS=NP-2*ND
      IF (NS.EQ.0) GO TO 403
      C * * * NUMBER OF POINTS IS EVEN. SET CEP TO A DISTANCE WHICH IS
      C * * * HALF WAY BETWEEN THE INTERIOR POINT CLOSEST TO THE 50 PER-
      C * * * CENT CIRCLE AND THE EXTERIOR POINT CLOSEST TO THE 50 PER-
      C * * * CENT CIRCLE.
      CEP=(SORTX(ND)+SORTX(ND+1))/2.
      GO TO 404
      C * * * NUMBER OF POINTS IS ODD. SET CEP TO THE MEDIAN DISTANCE.
      C * * *
      403 DEF=CEP*(ND+1)
      404 WRITE(6,1004) CEP
      1004 FORMAT(IX,4HCEP=,F10.5,2X,67HDATA FAILED K-S NORMALITY TEST -- NO
      *CONFIDENCE INTERVAL CALCULATED)
      GO TO 500
      300 WRITE(6,1000)
      1000 FORMAT(IX,2HSUBROUTINE CEP ENTERED WITH NO. POINTS = 0)
      GO TO 520
      C * * * PLOT CEP(3), CONFIDENCE INTERVALS, AND POINTS
      500 DX=50+100*YBAR**2+YBAR**2
      WRITE(6,1078)
      1078 FORMAT(IX,113HCEP,1078)
      1113 FORMAT(IX,17HCEP CENTROID AT (,F5.3,1H,10X,2H)DISTANCE F
      *FROM TARGET CENTER=,F5.3)
      IF (CEP.EQ.0) GO TO 520
      IF (CONF.LC.01) GO TO 501
      DO 27 KOCH=1,NCONE

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	JU=ICV(KOCH) DO 350 KMN=1,NP ZXX(KMN)=X(KMN) 506 ZYY(KMN)=Y(KMN) CALL PLOT(ZXX,ZYY,NP,CEP,ICONREF(JU),RCONF1(KOCH),TITLE1,XBAR, *YBAR,0.,PSIZE) IF (XLAMBDA.LT.EPSLN) GO TO 27 GO 357 KMN=1,NP ZXX(KMN)=X(KMN) ZYY(KMN)=Y(KMN) 517 CALL PLOT(ZXX,ZYY,NP,CEPS,ICONREF(JU),RCONF2(KOCH),TITLE2,XBAR, *YBAR,XLAMBDA,PSIZE) 27 CONTINUE GO TO 320 501 CALL PLOT(X,Y,NP,CEP,0.,0.,TITLE1,XBAR,YBAR,0.,PSIZE) 520 CONTINUE RETURN END	MCARLJ 565 MCARLJ 566 MCARLJ 567 MCARLJ 568 MCARLJ 569 MCARLJ 570 MCARLJ 571 MCARLJ 572 MCARLJ 573 MCARLJ 574 MCARLJ 575 MCARLJ 576 MCARLJ 577 MCARLJ 578 MCARLJ 579 MCARLJ 580 MCARLJ 581 MCARLJ 582
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SUBROUTINE CEPP	7/4/74	OPT=1	FTN 4.2+74.355	07/07/75	11.06.22*	PAGE	7
CARD NR. SEVERITY DETAILS	DIAGNOSIS OF PROBLEM						
40	1	DATA VARIABLE LIST EXCEEDS ITEM LIST, EXCESS VARIABLES NOT INITIALIZED.					

SYMBOLIC REFERENCE MAP (R=J)

330

SUBROUTINE CAPP				7474	OPT=1	FTN +274355				07/07/75	11-05-22	PAGE	9
VARIABLES		SN	TYPE	RELOCATION									
1001	CONF1	REAL	ARRAY	REFS	0	169	192	296	DEFINED	169	163		
1007	CONF2	REAL	ARRAY	REFS	99	212	296	DEFINED	169				
1310	SBR	REAL	ARRAY	REFS	99								
1313	SORTX	REAL	ARRAY	REFS	8	2*251	266	DEFINED	41	242	247		
1314	SORTX	REAL	ARRAY	REFS	121	124	126	DEFINED	120				
1314	SORTX	REAL	ARRAY	REFS	121	125	DEFINED	119					
1276	SORTX2	REAL	ARRAY	REFS	81	87	DEFINED	76	81				
1277	SORTX2	REAL	ARRAY	REFS	82	88	DEFINED	77	82				
1305	SK4AT	REAL	ARRAY	REFS	99	109	120	DEFINED	99				
1303	SK4AT2	REAL	ARRAY	REFS	89	DEFINED	87	DEFINED	99				
1306	SYMAT	REAL	ARRAY	REFS	104	109	120	DEFINED	98				
1304	SYMAT2	REAL	ARRAY	REFS	90	DEFINED	88	DEFINED	98				
1059	TITLE1	REAL	ARRAY	REFS	5	290	300	DEFINED	86				
1053	TITLE2	REAL	ARRAY	REFS	5	291	DEFINED	38					
0	X	REAL	ARRAY	REFS	8	301	DEFINED	99	175	176	228		
1300	XBR	REAL	ARRAY	REFS	288	294	301	DEFINED	1				
1301	YBR	REAL	ARRAY	REFS	289	295	300	DEFINED	1				
1319	ZK	REAL	ARRAY	REFS	84	86	88	104	175	228	277		
1301	ZY	REAL	ARRAY	REFS	200	290	300	DEFINED	79	84	86		
FILE NAMES	MOVE			REFS	4	290	296	DEFINED	208	294	295		
TAPED				REFS	4	290	296	DEFINED	209	295			
WRITES				REFS	70	106	103	110	111	131	132	133	
150				REFS	170	171	175	182	183	184	186	188	
190				REFS	192	194	197	198	200	205	206	207	
209				REFS	210	211	212	213	267	271	278	279	
280				REFS	280	281	282	283	284	285	286	287	

EXTERNALS				TYPE	ARGS	REFERENCES			
KTEST					0	99	104		
FLPUT					11	230	296	300	
SRT	REAL	1	LIBRARY:	59	90	163	165	169	175
									268
									277
INLINE FUNCTIONS				TYPE	ARGS	DEF LINE REFERENCES			
AMAXI	REAL	0	INTRIN			120			
AMIN	REAL	0	INTRIN			119			
STATEMENT LABELS				DEF LINE	REFERENCES				
0	1			30					
0	2			227					
224	3			236		237			
228	4			140		142			
0	5			151					
0	6			157					
0	7			174					
505	27			245		292			
217	44			152		149			
132	102			150		122			
0	103			124					
140	121			138		125			

STATEMENT LABELS	DEF LINE	REFERENCES			
0 237	INACTIVE				
302 300	271	72			
423 400	277	115			
442 402	235	245			
475 403	269	253			
477 404	267	262			
116 420	119	114			
305 500	277	196			
370 501	300	204	214	270	
277 520	301	273	283	299	
225 525	156	152			
277 524	171	136	139	160	166
337 529	190	179			
0 530	INACTIVE				
0 533	INACTIVE				
140 545	137	130			
0 557	295	293			
0 558	269	267			
1225 1000	272	271			
975 1001	107	106			
722 1002	112	111			
1210 1004	268	267			
760 1007	154	150			
1011 1010	172	171			
1026 1011	177	176			
1045 1012	185	184			
1065 1013	189	188			
1075 1014	191	190	210		
1104 1015	193	192	211		
1132 1016	201	200	212		
1152 1017	203	202			
067 1019	71	70			
1123 1076	199	199	110	132	170
			270	273	
747 1112	134	133			
1247 1113	281	280			
1056 1499	187	186	289		
1112 1500	195	194	213		
0 0350	INACTIVE	69			
LJPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	
34 1	1	80 84	73	INSTACK	
132 4	1	140 153	534	EXT REFS	EXT REFS
215 5	1	161 163	128	EXT REFS	EXT REFS
260 6	1	167 169	158	EXT REFS	EXT REFS
302 8	1	174 176	228	EXT REFS	EXT REFS
454 2	1	227 228	138	EXT REFS	EXT REFS
451 3	1	236 240	58	INSTACK	INSTACK
922 27	1	285 298	468	EXT REFS	NOT INNER
930 556	KNN	287 289	38	INSTACK	INSTACK
551 557	KNN	298 295	35	INSTACK	INSTACK
STATISTICS					
PROGRAM LENGTH		27243	1492		

SUBROUTINE NAME	74/74	OPT=1	FTN 1.2,74,355	07/0775	11.05.29.	PAGE
5	SUBROUTINE NORMRX, XL, XU, XMU, SGMA, RNSTRY XLL=XMU+SGMA*XL XU=XMU+SGMA*XJ CALL NURIAL(RX,XLL,XU,XMU,SGMA,RNSTRY) RETURN END					
	MCARLJ 583 MCARLJ 584 MCARLJ 585 MCARLJ 586 MCARLJ 587 MCARLJ 588					

SYMBOLIC REFERENCE MAP (R-J)

ENTRY POINTS DEF LINE REFERENCES
3 NORM 1 5

VARIABLES	SN	TYPE	RELOCATION
0 RNSTRT	REAL	F.P.	
0 KX	REAL	F.P.	
0 SOTA	REAL	F.P.	
0 XL	REAL	F.P.	
30 XLL	REAL	F.P.	
0 XNJ	REAL	F.P.	
0 XU	REAL	F.P.	
31 XUJ	REAL	F.P.	

EXTERNALS TYPE ARGS REFERENCES
NORMAL 5 4

STATISTICS
PROGRAM LENGTH

328 26


```

SUBROUTINE KSTEST(Y,MP,KSSIG,XPAR,SXMT,NIT)
  DIMENSION Y(100),CRIT(100),ISNIGF(100)
  REAL KSSIG
  DATA NZI70/
  DATA NUM70/
  DATA CRIT /375.,842.,708.,162.,565.,521.,486.,437.,432.,410.,391.,
  375.,361.,349.,339.,328.,309.,301.,294.,267.,264.,
  280.,275.,270.,264.,258.,252.,248.,242.,238.,233.,234.,
  232.,230.,227.,224.,221.,218.,215.,212.,210.,207.,205.,
  203.,200.,198.,196.,194.,192.,50*192./
  NV=NP
  NI=0
  PSNIG=KSSIG
  NZI=5
  3011 CONTINUE
  NSG=0
  500 FORMAT(I2)
  NGR=NUM71
  527 KNT=NV
  YMAX=Y(1)
  YS2=Y(1)**2
  YMIN=Y(1)
  YSUM=Y(1)
  DO 1 I=2,NV
    IF(YMAX-Y(I))100,106,101
    100 YMAX=Y(I)
    101 IF(YMIN-Y(I))105,106,102
    102 YMIN=Y(I)
    106 YSUM=YSUM+Y(I)
    1 YS2=YS2+Y(I)**2
  KNT=KNT+1
  S2=(YS2-(YSUM**2)/NV)/NV
  S=SRT(S2)
  YMEAN=YSUM/NV
  WRITE(6,953)NRM
  953 FORMAT(1X,9HCASE NO.=,I4/)
  WRITE(6,917)YMEAN,S
  517 FORMAT(11X,5HMEAN=,F10.4,9HSTD DEV=,F10.4)
  NSTEPS = NV/5
  SSTEP=(YMAX-YMIN)/NSTEPS
  B1=YMIN-SSTEP
  NCUN=0
  OMAR=0
  431 WRITE(6,431)NSTEPS,YMIN,YMAX
  431 FORMAT(1X,7HNSTEPS=,I5,2X,5HYMIN=,F6.3,1X,5HYMAX=,F6.3)
  DO 2 I=1,NSTEPS
    B1=31+SSTEP
    C85=B1+SSTEP
    124 C85=81+SSTEP
    125 IF(1.0,NSTEPS) 32=82+0.00001
  NV=0
  DO 2 J=1,NV
    IF(Y(J)-B1)3,103,103
    103 IF(Y(J)-82)104,3,3
    104 NV=NV+2
    NCUN=NCUN+1
  3 CONTINUE

```

```

63      RNCJ=NCUM
        RELCUM=RCUM/RNV
        YMINUS=URS-YMEAN
        Z=YMINSUN/S
        CAL=Z*TABLE(2,FREQ,NZ)
        U=Z*S(FREQ-RELCUM)
        IF(U-UMAX)120,120,121
        121 DMAX=U
        120 CONTINUE
        2 CONTINUE
        CRITIT=CRIT(NU)/1000.
        WRITEL(601,SDMAX,CRITIT)
        5123 FORMAT(IX,SDMAX=,F10.7,CRIT=,F10.7)
        IF(UMAX-CRITIT)500,500,503
        500 NSG=NSG+1
        510 CONTINUE
        NI=1
        506 CONTINUE
        70      RETURN
        END
MCARD 646
MCARD 647
MCARD 648
MCARD 649
MCARD 650
MCARD 651
MCARD 652
MCARD 653
MCARD 654
MCARD 655
MCARD 656
MCARD 657
MCARD 658
MCARD 659
MCARD 660
MCARD 661
MCARD 662
MCARD 663
MCARD 664
MCARD 665

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SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS J KSTEST	DEF LINE 1	REFERENCES 76	RELOCATION	
VARIABLES	SN	TYPE		
253 B1	REAL	REFS	47	49
251 B2	REAL	REFS	50	54
253 CRIT	REAL	REFS	2	63
252 CRITIT	REAL	REFS	69	71
251 U	REAL	REFS	64	65
247 UMAX	REAL	REFS	64	63
250 PNO	REAL	REFS	62	71
236 A	INTEGER	REFS	25	27
427 ISNIF	INTEGER	REFS	24	28
253 J	INTEGER	REFS	53	54
0 ASSIG	REAL	REFS	3	13
246 NCM	INTEGER	REFS	56	56
0 I1	INTEGER	REFS	1	12
252 NN	INTEGER	REFS	55	55
0 NP	INTEGER	REFS	11	1
250 NS2	INTEGER	REFS	72	72
243 NSTEPS	INTEGER	REFS	40	44
191 NOV	INTEGER	REFS	19	35
220 NV	INTEGER	REFS	19	19
190 NZF	INTEGER	REFS	11	24
250 Q35	REAL	REFS	62	4
235 KLCUM	REAL	REFS	60	48
234 KLCUM	REAL	REFS	63	59
231 KVA	REAL	REFS	99	58
237 KVA1	REAL	REFS	31	34
227 KVIQ	REAL	REFS	32	31
241 S	REAL	REFS	13	47
244 SSTEP	REAL	REFS	37	61
0 SSTAT	REAL	REFS	41	47
240 S2	REAL	REFS	1	32
0 X84R	REAL	REFS	33	DEFINED
0 Y	REAL	REFS	1	20
232 YMAX	REAL	REFS	2	21
242 YMEAN	REAL	REFS	28	30
234 YMIN	REAL	REFS	1	44
250 YMINUSN	REAL	REFS	25	40
239 YSUM	REAL	REFS	37	50
233 YS2	REAL	REFS	27	40
237 Z	REAL	REFS	61	DEFINED

FILE NAMES	MODE	WRITES	REFERENCES
TAPED	FMT	35	37
EXTERNALS	TYPE	ARG3	33
SRT	REAL	1 LIBRARY	62
ZTABLE		3	

SUBROUTINE KSTEST				7/4/74	OPT=1	FTN 4+2+74355		07/07/75	11.05.30.	PAGE	4
IN LINE FUNCTIONS		TYPE	ARGS	DEF LINE REFERENCES							
ABS		REAL	I	INTRIN	63						
STATEMENT LABELS											
		DEF LINE REFERENCES									
0 1		30	24								
0 2		67	46								
107 3		57	52								
		53	53								
0 100	INACTIVE	26	2*25								
30 101		27	25								
0 102	INACTIVE	28	27								
0 103	INACTIVE	54	2*53								
0 104	INACTIVE	55	54								
33 105		29	2*27								
125 120		66	2*64								
0 121	INACTIVE	65	54								
0 124	INACTIVE	48									
0 125	INACTIVE	49									
132 500	FMT NO REFS	17									
0 515	INACTIVE	73									
170 517	FMT	39	37								
0 527	INACTIVE	19									
100 563	FMT	36	35								
143 565		75	71								
0 568	INACTIVE	72	2*71								
0 5011	INACTIVE	15									
203 4331	FMT	45	44								
216 6123	FMT	70	59								
LOOPS LABEL		INDEX	FROM-TO	LENGTH	PROPERTIES						
25 1	I	24 30	128		OPT						
00 2	* I	40 67	443		EXT REFS NOT INNER						
77 2	* J	52 67	319		EXT REFS						
STATISTICS											
PROGRAM LENGTH				5739	379						

SUBROUTINE ZTABLE(2,FREQ,N2)		MCARLO	556
DIMENSION ZCUM(385)		MCARLO	557
DATA (ZCUM(I),I=1,108)		MCARLO	558
5	1 /0000..0040..0080..0120..0160..0199..0233..0279..0319..	MCARLO	559
	A 0359..0398..0438..0478..0517..0557..0595..0636..0675..	MCARLO	560
	B 0714..0753..0793..0832..0871..0910..0948..0987..1026..	MCARLO	561
	C 1095..1133..1171..1210..1249..1287..1325..1364..1402..	MCARLO	562
	D 1466..1503..1540..1578..1616..1654..1691..1729..1767..	MCARLO	563
	E 1736..1772..1808..1844..1879..1915..1950..1985..2019..	MCARLO	564
10	F 2054..2088..2123..2157..2190..2224..2257..2291..2324..	MCARLO	565
	G 2357..2389..2422..2455..2488..2521..2554..2587..2611..	MCARLO	566
	H 2642..2673..2704..2734..2764..2794..2823..2852..2881..	MCARLO	567
	I 2910..2939..2967..2995..3023..3051..3079..3106..3133..	MCARLO	568
	J 3159..3186..3212..3238..3264..3289..3315..3340..3365..	MCARLO	569
15	K 3389..3413..3438..3461..3485..3508..3531..3554..3577..	MCARLO	570
DATA (ZCUM(I),I=109,216)		MCARLO	571
2	/3599..3621..3643..3665..3686..3708..3729..3749..3770..	MCARLO	572
	A 3740..3810..3830..3849..3869..3888..3907..3925..3944..	MCARLO	573
	B 3942..3990..3997..4015..4032..4049..4065..4082..4099..	MCARLO	574
20	C 4115..4131..4147..4162..4177..4192..4207..4222..4236..	MCARLO	575
	D 4231..4255..4275..4292..4306..4319..4332..4345..4357..	MCARLO	576
	E 4370..4382..4394..4406..4418..4429..4441..4452..4463..	MCARLO	577
	F 4474..4484..4495..4505..4515..4525..4535..4545..4554..	MCARLO	578
	G 4564..4573..4582..4591..4599..4608..4615..4625..4633..	MCARLO	579
25	H 4641..4659..4656..4664..4671..4678..4685..4693..4699..	MCARLO	580
	I 4706..4713..4719..4726..4732..4738..4744..4750..4756..	MCARLO	581
	J 4761..4767..4772..4778..4783..4788..4793..4798..4803..	MCARLO	582
	K 4808..4812..4817..4821..4826..4830..4833..4838..4842..	MCARLO	583
30	DATA (ZCUM(I),I=217,385)	MCARLO	584
3	/4846..4850..4854..4857..4861..4864..4869..4871..4875..	MCARLO	585
	A 4876..4881..4884..4887..4890..4893..4895..4898..4901..	MCARLO	586
	B 4904..4908..4909..4911..4913..4916..4918..4922..4925..	MCARLO	587
	C 4925..4927..4929..4931..4932..4934..4935..4938..4940..	MCARLO	588
35	D 4941..4943..4945..4946..4948..4949..4951..4952..4953..	MCARLO	589
	E 4955..4956..4957..4959..4960..4961..4962..4963..4964..	MCARLO	590
	F 4965..4966..4967..4968..4969..4970..4971..4972..4973..	MCARLO	591
	G 4974..4975..4976..4977..4978..4979..4980..4981..4982..	MCARLO	592
	H 4983..4984..4985..4986..4987..4988..4989..4990..4991..	MCARLO	593
	I 4992..4993..4994..4995..4996..4997..4998..4999..5000..	MCARLO	594
40	J 5001..5002..5003..5004..5005..5006..5007..5008..5009..	MCARLO	595
107 ABSZ=ABS(Z)		MCARLO	596
EPS,N1=0.005		MCARLO	597
EPS,N2=0.005		MCARLO	598
45	IF (Z-EP,N1) 110,111,111	MCARLO	599
	111 IF (Z-EP,N1) 110,111,111	MCARLO	600
	112 IF (Z-EP,N2) 112,112,110	MCARLO	601
	GO TO 200	MCARLO	602
50	110 ABSZ=100.*ABSZ	MCARLO	603
	IF (Z-ABSZ)	MCARLO	604
	NZ=1Z	MCARLO	605
	NZ=1Z+0.5	MCARLO	606
	IF (ABSZ-NZ) 101,101,102	MCARLO	607
	102 IF (Z-1Z)	MCARLO	608
	101 IF (1Z-101) 103,104,104	MCARLO	609
55	104 FREQ=1	MCARLO	610
	IF (Z-1Z) FREQ=0.	MCARLO	611
	GO TO 200	MCARLO	612

SUBROUTINE	ZTABLE	74/74	OPT=1	FTN 4.2+74.355	07/07/75	11.05.31.	PAGE
							2
60	103 12=12+1				MCARL3	723	
	FREQ = ZCUM(12)/10000.				MCARL3	724	
	IF (Z=0.1105,105,106				MCARL3	725	
	105 FREQ=0.5-FREQ				MCARL3	726	
	GO TO 200				MCARL3	727	
	106 FREQ=FREQ+0.5				MCARL3	728	
	200 RETURN				MCARL3	729	
65	END				MCARL3	730	


```

2 CONTINUE
NS=NS+1
SORTX(NS)=Y(IY)
Y(IY)=Y(IND)
SORTX(NS)=X(IY)
X(IY)=X(IND)
ND=ND-1
IF (ND.GT.1) GO TO 103
NS=NS+1
SORTX(NS)=Y(1)
Y(1)=Y(1)
SORTX(NS)=X(1)
X(1)=X(1)
XMAX = ABS(XMAX)
XMIN = ABS(XMIN)
XCM = (XMAX+XMIN)/2
YMAX = ABS(SORTX(1))
YMIN = ABS(SORTX(NP1))
YCM = (YMAX+YMIN)/2
106 XCI=ABS(XBAR) + AMAX1(CEP,RCONF)
YCI=ABS(YBAR) + AMAX1(CEP,RCONF)
110 TSPRD=AMAX1(XDEV,YDEV,XCI,YCI)
IF (PSIZE.GT.0) TSPRD=PSIZE/2.
SCAL=2=SCAL/2.
HSPRD=TSPRD
HSCAL=HSPRD/39.
CCIRTP=YBAR + CEP
CCIRB=YBAR - CEP
RCIRTP=YBAR + RCONF
RCIRB=YBAR - RCONF
IF (RCONF.LT.CEPRCIRTP=-100000.
YCEP = CCIRTP + SCAL
YCNF = RCIRTP + SCAL
108 YOSM = 0
TU = TSPRD + SCAL
NJ=1
CALL XLOC(10.,HSPRD,IND,INDX)
190 INDX = INDX
DO 15 I=1,44
TU=TU - SCAL
ELINE(INDX)=ROR.A.MSKK(INDX).O.PLINE(INDX).A..N.YSKK(INDX)
IF (ABS(LT.TU.OR.LTGTSM.GI.0) GO TO 2222
DO 2223 IOP=7,16
2223 PLINE(IOP)=ROR
2222 CONTINUE
IF (CCIRTP.LT.TU.JR.TU.LT.CCIRB) GO TO 5180
YCEP=YCEP - SCAL
ARG=CCP**2 - YCEP**2 + 2*YCEP*YBAR - YBAR**2
IF (ARG.LT.0) GO TO 5180
RAU=SQRT(ARG)
GO TO 5181
5180 CONTINUE
IF (CCIRTP.LT.TU) GO TO 205
IF (ABS(TU - CCIRB).GT.SCAL2) GO TO 205
RAU=0.
5181 CONTINUE
XAL=XBAR - RAJ

```

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SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS J PLOT	DEF LINE I	REFERENCES 158	RELOCATION	
VARIABLES	SN	TYPE		
722 IRSG	REAL	REFS	106	107
726 ARGNF	REAL	REFS	123	124
777 BLWKK	REAL	REFS	31	34
707 CCRBT	REAL	REFS	103	111
706 CCRTP	REAL	REFS	68	103
0 CEP	REAL	REFS	22	75
		REFS	22	76
		REFS	22	83
		REFS	22	87
		REFS	22	105
467 CEPX	REAL	REFS	30	6
470 COMFC	REAL	REFS	41	7
662 CPSCC	REAL	REFS	32	35
476 CPSEM	REAL	REFS	31	141
473 CPR	REAL	REFS	116	113
732 DX	REAL	REFS	162	161
471 EP3LN	* REAL	REFS	8	
709 MS2AL	* REAL	REFS	82	
704 MS2RD	REAL	REFS	144	
661 I	INTEGER	REFS	26	52
		REFS	26	53
		REFS	26	54
		REFS	26	56
		REFS	26	57
0 IC4I	INTEGER	REFS	40	41
655 ICRSM	* INTEGER	REFS	20	
712 ICSM	INTEGER	REFS	137	90
716 INDX	INTEGER	REFS	93	95
		REFS	133	135
		REFS	133	140
		REFS	133	141
		REFS	133	144
		REFS	133	151
721 IOP	INTEGER	REFS	101	100
656 IT2TSM	INTEGER	REFS	99	142
715 IWD	INTEGER	REFS	93	94
		REFS	135	140
		REFS	135	141
		REFS	135	144
		REFS	135	151
720 IYNDX	INTEGER	REFS	293	95
717 IX40	INTEGER	REFS	298	94
670 IY	INTEGER	REFS	60	61
727 J4	INTEGER	REFS	150	154
730 K4	INTEGER	REFS	149	144
731 K4J	INTEGER	REFS	155	153
1271 KSKK	INTEGER	REFS	155	153
		REFS	155	155
		REFS	155	157
		REFS	155	158
		REFS	155	159
		REFS	155	160
		REFS	155	161
		REFS	155	162
		REFS	155	163
		REFS	155	164
		REFS	155	165
		REFS	155	166
		REFS	155	167
		REFS	155	168
		REFS	155	169
		REFS	155	170
		REFS	155	171
		REFS	155	172
		REFS	155	173
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		REFS	155	246
		REFS	155	247
		REFS	155	248
		REFS	155	249
		REFS	155	250
		REFS	155	251
		REFS	155	252
		REFS	155	253
		REFS	155	254
		REFS	155	255
		REFS	155	256
		REFS	155	257
		REFS	155	258
		REFS	155	259
		REFS	155	260
		REFS	155	261
		REFS	155	262
		REFS	155	263
		REFS	155	264
		REFS	155	265
		REFS	155	266
		REFS	155	267
		REFS	155	268
		REFS	155	269
		REFS	155	270
		REFS	155	271
		REFS	155	272
		REFS	155	273
		REFS	155	274
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		REFS	155	286
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		REFS	155	288
		REFS	155	289
		REFS	155	290
		REFS	155	291
		REFS	155	292
		REFS	155	293
		REFS	155	294
		REFS	155	295
		REFS	155	296
		REFS	155	297
		REFS	155	298
		REFS	155	299
		REFS	155	300

STATEMENT LABELS	DEF LINE	REFERENCES
0 15	159	96
0 16	153	148
0 33	158	157
41 100	42	40
74 101	55	52
56 103	50	65
0 105	INACTIVE	
0 110	INACTIVE	
416 201	77	149
420 202	154	147
300 105	155	111
345 207	120	110
361 210	137	128
373 213	142	138
503 1000	146	142
512 1001	25	24
547 1002	27	26
552 1003	37	29
517 1021	38	28
502 1022	163	162
554 1072	159	155
570 1073	39	30
518 1175	45	41
534 1432	199	165
544 1433	31	32
533 1422	36	35
0 1423	102	99
251 5150	101	100
260 5151	109	103
316 5130	113	108
325 5151	126	120
	130	125

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
42 1	* I	43 44	58	EXT REFS
70 2	* I	51 58	159	OPT
217 15	* I	36 159	2113	EXT REFS NOT INNER
231 1223	TOP	100 101	28	INSTACK
400 16	* K	148 153	158	EXT REFS
424 33	KUG	157 158	28	INSTACK

STATISTICS PROGRAM LENGTH 13158 717

SUBROUTINE	XLOC	7/474	OPI=1	FTN 4.2+7.355	07/0775	11.05.40.	PAGE	1
SUBROUTINE XLOC(XVL, NSPRO, IWO, INDXT)								
XD=ABS (HSPRO - XVAL)								
XR=XU/12.*HSPRO								
PK=XK*70.								
KK=KK								
KK=KK								
KMK=XK-KK								
IF (RMOR.GE.0.5) KK=KK+1								
KK1=KK - 1								
IWO=KK1/7								
INDX=KK - 7*IWO								
INDXIND = 7								
RETURN								
END								
5					MCARL3	990		
					MCARL3	901		
					MCARL3	902		
					MCARL3	903		
					MCARL3	904		
					MCARL3	905		
					MCARL3	906		
					MCARL3	907		
					MCARL3	908		
					MCARL3	909		
					MCARL3	910		
					MCARL3	911		
					MCARL3	912		
					MCARL3	913		

SYMBOLIC REFERENCE MAP TR=37

ENTRY POINTS DEF LINE REFERENCES
3 XLOC 1 13

VARIABLES SN TYPE RELOCATION

0	MSRD	REAL	REFS	2	3	DEFINED	1
1	INDX	INTEGER	DEFINED	1	11	DEFINED	1
2	IND	INTEGER	REFS	11	12	DEFINED	1
3	KK	INTEGER	REFS	6	3	DEFINED	18
4	KK1	INTEGER	REFS	10	9	DEFINED	12
5	KK	REAL	REFS	5	7	DEFINED	5
6	KK	REAL	REFS	7	6	DEFINED	4
7	KK	REAL	REFS	8	7	DEFINED	7
8	KK	REAL	REFS	3	8	DEFINED	2
9	KK	REAL	REFS	4	4	DEFINED	3
10	XVAL	REAL	REFS	2	2	DEFINED	1

INLINE FUNCTIONS TYPE XLOC DEF LINE REFERENCES
ABS 1 INTRIN 2

STATISTICS
PROGRAM LENGTH 438 35

CLASS	LENGTH	MEMBERS	NAME(LENGTH)
51	3830	51	VMZE (1)
57		57	WMDM (1)
61		61	SLM (1)
68		68	GSIGU (1)
103		103	VMZE (1)
1006		1006	VYE (1)
3752		3752	ITDUC (10)
53		53	SLU (1)
58		58	SLM (1)
64		64	CAPSIM (1)
69		69	GVATE (1)
181		181	VMZE (1)
1512		1512	VXE (1)
3750		3750	ITCT (1)

STATISTICS

PROGRAM LENGTH 638 SL
CM LABELLED COMMON LENGTH 73669 3830

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SUBROUTINE G21
C**WIND AND GUSTS MODULE
COMMON /C/ C18301
C**INPUT DATA
5 EQUIVALENCE (C120001,T1)
EQUIVALENCE (C1 5014,PTNM )
EQUIVALENCE (C1 5117,PSIM )
EQUIVALENCE (C1 521,VMTE )
C**OUTPUT DATA
10 EQUIVALENCE (C1 1001,VMKE )
EQUIVALENCE (C1 1011,VMYE )
EQUIVALENCE (C1 1021,VMZE )
C**INPUTS FROM OTHER MODULES
15 EQUIVALENCE (C1 541, SIGU)
EQUIVALENCE (C1 561, RLUM)
EQUIVALENCE (C1 581, WNDM01)
EQUIVALENCE (C1 591, SLM01)
EQUIVALENCE (C1 601, RLW)
EQUIVALENCE (C1 621, SLM)
20 EQUIVALENCE (C1 651,28PSIM)
EQUIVALENCE (C1 661,58PSIM)
EQUIVALENCE (C1 681, VMTEH)
EQUIVALENCE (C1 691, GSIGU)
EQUIVALENCE (C12561), N)
25 EQUIVALENCE (C12562), IPL)
EQUIVALENCE (C13634), ISMDX)
EQUIVALENCE (C13512), I3512)
EQUIVALENCE (C13753), ITMDX)
EQUIVALENCE (C13721), ITCT)
30 DIMENSION IPL(100), ISMDX(40), ITNDX(10)
C
VMTE=VMTE
C MONTE CARLO STEADY STATE WIND COMPONENT
DO 500 I = 1, 13512
I00 = I
IF (ISMDX(I),EQ.51) CALL MCARLO (I00M, 1, I00)
IF (ISMDX(I),EQ.52) CALL MCARLO (I00M, 1, I00)
500 CONTINUE
C
VMTE = ABS (VMTE)
SLW = 0.
C MONTE CARLO INITIAL VALUE OF TIME SERIES WIND GUSTS
DO 501 I = 1,ITCT
I00 = I
IF (ITNDX(I),NE.78) GO TO 501
CALL MCARLO ( I00M,4,I00)
WMD40 = 1.
IF (VMTE,GT.0) GO TO 505
SIGU = VMTE/2.9
GO TO 506
505 CONTINUE
506 CONTINUE
VMTE = 2.9 * SIGU
GS150 = SIGU*SQRT(.09/0126641)
BLU = -12.1*SIGU + 475.
IF (VMTE/VMTE,GT.,1) WMD40 = VMTE/VMTEH

```

SUBROUTINE	G2I	74/74	OPT=1	FTN ++274355	07/07/75	11.05.42.	PAGE
							2
60					62	106	
					62	107	
					62	108	
					62	109	
					62	110	
					62	111	
					62	112	
65					62	113	
					62	114	
					62	115	
					62	116	

```

IPLIM = 59
N = N + 1
501 CONTINUE
C
CBPSIM = COSD(BPSIM)
SBPSIM = SIND(BPSIM)
VMX = - VMT*CBPSIM
VMT = - VMT*SBPSIM
VMZE = 0.
RETURN
END

```


SUBROUTINE G2I		74/74	OPT=1	FTN 1.2*74.355	07/07/75	11.05.42.	PAGE	3
CARD NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM					
58	I	IIC1	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.					

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
1 G2I 57

VARIABLES	SN	TYPE	RELOCATION	DEF LINE	REFERENCES
67 BLJ	REAL	C		15	DEFINED 56
62 BPSIM	REAL	C		7	62 53
0 C	REAL	ARRAY	C	12	7 6
				14	13 16
				22	17 18
				23	24 25
				55	26 27
100 COPSIM	REAL	C		62	
115 DUM	REAL	C		37	
104 GSIGU	REAL	C		55	
113 I	INTEGER	C		37	45
				35	46
				34	
114 100	INTEGER	C		37	47
1001 IPL	INTEGER	ARRAY	C	25	47 DEFINED 35
7001 ISNOX	INTEGER	ARRAY	C	25	30 36
7210 ITST	INTEGER	C		26	37
7250 ITNOX	INTEGER	ARRAY	C	29	
9607 I3512	INTEGER	C		28	46
3000 N	INTEGER	C		27	34
				24	59
71 OPTIM	REAL	C		6	
73 ALA	REAL	C		18	
101 SPSPIM	REAL	C		21	63 DEFINED 50
92 SIJU	REAL	C		51	56
95 SLA	REAL	C		14	DEFINED 41
72 SLAD	REAL	C		19	
3717 I	REAL	C		17	
03 VMTE	REAL	C		8	32 49
				65	50 2*57 64
103 VMTEH	REAL	C		22	40 53
143 VMKE	REAL	C		10	DEFINED 32
144 VMYE	REAL	C		11	DEFINED 64
145 VMTE	REAL	C		12	DEFINED 55
71 MNDMU	REAL	C		15	DEFINED 56
				16	DEFINED 48
EXTERNALS	TYPE	ARGS	REFERENCES		
CO3D	REAL	1	92		
MCARLO	REAL	3	36		
SIHQ	REAL	1	37		
SRT	REAL	1	55		
LIBRARY	1				
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES	
ABS	REAL	1	INTRIN	40	
STATEMENT LABELS			DEF LINE	REFERENCES	
0 200			38	34	
55 501			60	44	46
36 505			52	49	
40 505			54	51	
LOOPS LABEL			FROM-TO	LENGTH	PROPERTIES
2 500 * I			34 83	143	EXT REFS
24 501 * I			44 60	343	EXT REFS

COMMON BLOCKS		LENGTH		MEMBERS - BIAS NAME(LENGTH)	
C		3830		0 C 138301	
EQUIV CLASSES		LENGTH		MEMBERS - BIAS NAME(LENGTH)	
C		3830		49 OPTNM (1)	
				53 SIGU (1)	
				58 SLWD (1)	
				64 COPSIM (1)	
				68 GSIGU (1)	
				101 VMZE (1)	
				2561 IPL (100)	
				3720 IFOT (1)	
				50 BPSIM (1)	
				55 BLJ (1)	
				59 RLA (1)	
				65 SOPSIM (1)	
				99 VMKE (1)	
				1999 T (1)	
				3511 I3512 (1)	
				3633 ISNOX (40)	
				31 VMTE (1)	
				37 MNDW0 (1)	
				31 SLW (1)	
				37 VMTEM (1)	
				170 VMTE (1)	
				2530 N (1)	
				3633 ISNOX (40)	

STATISTICS

PROGRAM LENGTH 1168 73
CM LABELED COMMON LENGTH 73663 3839

SUBROUTINE G3	74/74	OPT=1	FTN 4.2+74.355	07/0775	11.05.43.	PAGE	1
SUBROUTINE G3							
C**AIR DATA MODULE G3						G3	2
COMMON /C/ C(388)						G3	3
C**INPUT DATA						LABCON	4
5 EQUIVALENCE (C(0200),RMZRO)						G3	5
C**INPUTS FROM OTHER MODULES						G3	6
EQUIVALENCE (C(0100),VMXE)						G3	7
EQUIVALENCE (C(0101),VMYE)						G3	8
EQUIVALENCE (C(0102),VMZE)						G3	9
10 EQUIVALENCE (C(1603),VXE)						G3	10
EQUIVALENCE (C(1607),VYE)						G3	11
EQUIVALENCE (C(1611),VZE)						G3	12
EQUIVALENCE (C(1623),VZE)						G3	13
C**INPUTS FROM MAIN PROGRAM						G3	14
C**STATE VARIABLE OUTPUTS						G3	15
C**NONE						G3	16
C**OTHER OUTPUTS						G3	17
EQUIVALENCE (C(0200),VMXE)						G3	18
EQUIVALENCE (C(0201),VMYE)						G3	19
EQUIVALENCE (C(0202),VMZE)						G3	20
EQUIVALENCE (C(0203),DYHMC)						G3	21
EQUIVALENCE (C(0204),VMACH)						G3	22
EQUIVALENCE (C(0205),DRHO)						G3	23
EQUIVALENCE (C(0206),VSOUND)						G3	24
EQUIVALENCE (C(0207),VAIRSP)						G3	25
EQUIVALENCE (C(0209),RM)						G3	26
C**CALCULATE PRESENT ALTITUDE						G3	27
RME = FZE*RMZRO						G3	28
C**CALCULATE MISSILE VELOCITY WRT AIR MASS IN EARTH AXES						G3	29
VMXE = VXE-VMXE						G3	30
VMYE = VYE-VMYE						G3	31
VMZE = VZE-VMZE						G3	32
VAIRSP = SQRT(VMXE*VMXE+VMYE*VMYE+VMZE*VMZE)						G3	33
C**AIR DENSITY, SPEED OF SOUND, DYNAMIC PRESSURE, AND VMCH						G3	34
DRHO = (1.0764751/11.0+.3325E-06*RM*RM*RM*.02315E-12)						G3	35
VSOUND = -.00392*RM*1117.3						G3	36
DYHMC = (DRHO*VAIRSP*VAIRSP)/64.344						G3	37
VMACH = VAIRSP/VSOUND						G3	38
RETURN						G3	39
END						G3	40
						G3	41

~~SYMBOLIC REFERENCE MAP (R=5)~~

ENTRY POINTS		DEF LINE		REFERENCES	
1	G3	1	39		
VARIABLES					
D	C	SN	TYPE	RELOCATION	
			REAL	ARRAY	C
		REFS			
		12		5	
		24		13	
314	UR4D	25		15	
		REFS		37	
315	POTMNC	26		DEFINED	
		REFS		37	
316	VAIRSP	27		4935	
		REFS		23	
317	RH4R0	28		36	
		REFS		36	
318	RZ	29		38	
		REFS		DEFINED	
319	WHICH	30		38	
		REFS		DEFINED	
320	VMXAE	31		38	
		REFS		DEFINED	
321	VM4YE	32		38	
		REFS		DEFINED	
322	VMWZE	33		38	
		REFS		DEFINED	
323	V5OUND	34		36	
		REFS		DEFINED	
324	VMXE	35		38	
		REFS		DEFINED	
325	VMXE	36		38	
		REFS		DEFINED	
326	VMXE	37		38	
		REFS		DEFINED	
327	VMZE	38		38	
		REFS		DEFINED	
328	VXE	39		38	
		REFS		DEFINED	
329	VYE	40		38	
		REFS		DEFINED	
330	VZE	41		38	
		REFS		DEFINED	
331	VZE	42		38	
		REFS		DEFINED	
332	VZE	43		38	
		REFS		DEFINED	
333	VZE	44		38	
		REFS		DEFINED	
334	VZE	45		38	
		REFS		DEFINED	
335	VZE	46		38	
		REFS		DEFINED	
336	VZE	47		38	
		REFS		DEFINED	
337	VZE	48		38	
		REFS		DEFINED	
338	VZE	49		38	
		REFS		DEFINED	
339	VZE	50		38	
		REFS		DEFINED	
340	VZE	51		38	
		REFS		DEFINED	
341	VZE	52		38	
		REFS		DEFINED	
342	VZE	53		38	
		REFS		DEFINED	
343	VZE	54		38	
		REFS		DEFINED	
344	VZE	55		38	
		REFS		DEFINED	
345	VZE	56		38	
		REFS		DEFINED	
346	VZE	57		38	
		REFS		DEFINED	
347	VZE	58		38	
		REFS		DEFINED	
348	VZE	59		38	
		REFS		DEFINED	
349	VZE	60		38	
		REFS		DEFINED	
350	VZE	61		38	
		REFS		DEFINED	
351	VZE	62		38	
		REFS		DEFINED	
352	VZE	63		38	
		REFS		DEFINED	
353	VZE	64		38	
		REFS		DEFINED	
354	VZE	65		38	
		REFS		DEFINED	
355	VZE	66		38	
		REFS		DEFINED	
356	VZE	67		38	
		REFS		DEFINED	
357	VZE	68		38	
		REFS		DEFINED	
358	VZE	69		38	
		REFS		DEFINED	
359	VZE	70		38	
		REFS		DEFINED	
360	VZE	71		38	
		REFS		DEFINED	
361	VZE	72		38	
		REFS		DEFINED	
362	VZE	73		38	
		REFS		DEFINED	
363	VZE	74		38	
		REFS		DEFINED	
364	VZE	75		38	
		REFS		DEFINED	
365	VZE	76		38	
		REFS		DEFINED	
366	VZE	77		38	
		REFS		DEFINED	
367	VZE	78		38	
		REFS		DEFINED	
368	VZE	79		38	
		REFS		DEFINED	
369	VZE	80		38	
		REFS		DEFINED	
370	VZE	81		38	
		REFS		DEFINED	
371	VZE	82		38	
		REFS		DEFINED	
372	VZE	83		38	
		REFS		DEFINED	
373	VZE	84		38	
		REFS		DEFINED	
374	VZE	85		38	
		REFS		DEFINED	
375	VZE	86		38	
		REFS		DEFINED	
376	VZE	87		38	
		REFS		DEFINED	
377	VZE	88		38	
		REFS		DEFINED	
378	VZE	89		38	
		REFS		DEFINED	
379	VZE	90		38	
		REFS		DEFINED	
380	VZE	91		38	
		REFS		DEFINED	
381	VZE	92		38	
		REFS		DEFINED	
382	VZE	93		38	
		REFS		DEFINED	
383	VZE	94		38	
		REFS		DEFINED	
384	VZE	95		38	
		REFS		DEFINED	
385	VZE	96		38	
		REFS		DEFINED	
386	VZE	97		38	
		REFS		DEFINED	
387	VZE	98		38	
		REFS		DEFINED	
388	VZE	99		38	
		REFS		DEFINED	
389	VZE	100		38	
		REFS		DEFINED	
390	VZE	101		38	
		REFS		DEFINED	
391	VZE	102		38	
		REFS		DEFINED	
392	VZE	103		38	
		REFS		DEFINED	
393	VZE	104		38	
		REFS		DEFINED	
394	VZE	105		38	
		REFS		DEFINED	
395	VZE	106		38	
		REFS		DEFINED	
396	VZE	107		38	
		REFS		DEFINED	
397	VZE	108		38	
		REFS		DEFINED	
398	VZE	109		38	
		REFS		DEFINED	
399	VZE	110		38	
		REFS		DEFINED	
400	VZE	111		38	
		REFS		DEFINED	
401	VZE	112		38	
		REFS		DEFINED	
402	VZE	113		38	
		REFS		DEFINED	
403	VZE	114		38	
		REFS		DEFINED	
404	VZE	115		38	
		REFS		DEFINED	
405	VZE	116		38	
		REFS		DEFINED	
406	VZE	117		38	
		REFS		DEFINED	
407	VZE	118		38	
		REFS		DEFINED	
408	VZE	119		38	
		REFS		DEFINED	
409	VZE	120		38	
		REFS		DEFINED	
410	VZE	121		38	
		REFS		DEFINED	
411	VZE	122		38	
		REFS		DEFINED	
412	VZE	123		38	
		REFS		DEFINED	
413	VZE	124		38	
		REFS		DEFINED	
414	VZE	125		38	
		REFS		DEFINED	
415	VZE	126		38	
		REFS		DEFINED	
416	VZE	127		38	
		REFS		DEFINED	
417	VZE	128		38	
		REFS		DEFINED	
418	VZE	129		38	
		REFS		DEFINED	
419	VZE	130		38	
		REFS		DEFINED	
420	VZE	131		38	
		REFS		DEFINED	
421	VZE	132		38	
		REFS		DEFINED	
422	VZE	133		38	
		REFS		DEFINED	
423	VZE	134		38	
		REFS		DEFINED	
424	VZE	135		38	
		REFS		DEFINED	
425	VZE	136		38	
		REFS		DEFINED	
426	VZE	137		38	
		REFS		DEFINED	
427	VZE	138		38	
		REFS		DEFINED	
428	VZE	139		38	
		REFS		DEFINED	
429	VZE	140		38	
		REFS		DEFINED	
430	VZE	141		38	
		REFS		DEFINED	
431	VZE	142		38	
		REFS		DEFINED	
432	VZE	143		38	
		REFS		DEFINED	
433	VZE	144		38	
		REFS		DEFINED	
434	VZE	145		38	
		REFS		DEFINED	
435	VZE	146		38	
		REFS		DEFINED	
436	VZE	147		38	
		REFS		DEFINED	
437	VZE	148		38	
		REFS		DEFINED	
438	VZE	149		38	
		REFS		DEFINED	
439	VZE	150		38	
		REFS		DEFINED	
440	VZE	151		38	
		REFS		DEFINED	
441	VZE	152		38	
		REFS		DEFINED	
442	VZE	153		38	
		REFS		DEFINED	
443	VZE	154		38	
		REFS		DEFINED	
444	VZE	155		38	
		REFS		DEFINED	
445	VZE	156		38	
		REFS		DEFINED	
446	VZE	157		38	
		REFS		DEFINED	
447	VZE	158		38	
		REFS		DEFINED	
448	VZE	159		38	
		REFS		DEFINED	
449	VZE	160		38	
		REFS		DEFINED	
450	VZE	161		38	
		REFS		DEFINED	
451	VZE	162		38	
		REFS		DEFINED	
452	VZE	163		38	
		REFS		DEFINED	
453	VZE	164		38	
		REFS		DEFINED	
454	VZE	165		38	
		REFS		DEFINED	
455	VZE	166		38	
		REFS		DEFINED	
456	VZE	167		38	
		REFS		DEFINED	
457	VZE	168		38	
		REFS		DEFINED	
458	VZE	169		38	
		REFS		DEFINED	
459	VZE	170		38	
		REFS		DEFINED	
460	VZE	171		38	
		REFS		DEFINED	
461	VZE	172		38	
		REFS		DEFINED	
462	VZE	173		38	
		REFS		DEFINED	
463	VZE	174		38	
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464	VZE	175		38	
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465	VZE	176		38	
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466	VZE	177		38	
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467	VZE	178		38	
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468	VZE	179		38	
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469	VZE	180		38	
		REFS		DEFINED	
470	VZE	181		38	
		REFS		DEFINED	
471	VZE	182		38	
		REFS		DEFINED	
472	VZE	183		38	
		REFS		DEFINED	
473	VZE	184		38	
		REFS		DEFINED	
474	VZE	185		38	
		REFS		DEFINED	
475	VZE	186		38	
		REFS		DEFINED	
476	VZE	187		38	
		REFS		DEFINED	
477	VZE	188		38	
		REFS		DEFINED	
478	VZE	189		38	

60	EQUIVALENCE IC(1759),CFAS3)	65	59
	EQUIVALENCE IC(1751),CRAO)	65	50
	EQUIVALENCE IC(1760), X801)	65	61
	EQUIVALENCE IC(1769), Y801)	65	62
	EQUIVALENCE IC(1770), Z801)	65	58
	EQUIVALENCE IC(1771), X802)	65	64
	EQUIVALENCE IC(1772), Y802)	65	55
65	EQUIVALENCE IC(1773), Z802)	65	66
	EQUIVALENCE IC(1764), P1)	65	67
	EQUIVALENCE IC(1751), A011)	65	67
	EQUIVALENCE IC(1762), A012)	65	71
70	EQUIVALENCE IC(1763), A013)	65	72
	EQUIVALENCE IC(1755), A021)	65	73
	EQUIVALENCE IC(1756), A022)	65	74
	EQUIVALENCE IC(1757), A023)	65	75
	EQUIVALENCE IC(1758), A031)	65	76
75	EQUIVALENCE IC(1759), A032)	65	77
	EQUIVALENCE IC(1760), A033)	65	78
	EQUIVALENCE IC(2000), I)	65	79
	C**OTHER OUTPUTS	65	80
80	EQUIVALENCE IC(0350),3TMF)	65	81
	EQUIVALENCE IC(0351),BPSI)	65	82
	EQUIVALENCE IC(0352),SPMI)	65	83
	EQUIVALENCE IC(353),RPH1)	65	84
85	EQUIVALENCE IC(354),3TMP)	65	85
	EQUIVALENCE IC(355),BPS1)	65	86
	EQUIVALENCE IC(0356),VTOT)	65	87
	EQUIVALENCE IC(0357),SGAMH)	65	88
	EQUIVALENCE IC(0358),SGAMV)	65	89
90	EQUIVALENCE IC(0363),3THLV)	65	90
	EQUIVALENCE IC(0364),SPSLV)	65	91
	EQUIVALENCE IC(0365),3LAMV)	65	92
	EQUIVALENCE IC(0366),3LAMH)	65	93
	EQUIVALENCE IC(0367),3ALPHA)	65	94
	EQUIVALENCE IC(0368),3ALPHV)	65	95
95	EQUIVALENCE IC(0369),3ALPHI)	65	96
	EQUIVALENCE IC(0370),3PHIP)	65	97
	EQUIVALENCE IC(0371),RANGE)	65	98
	EQUIVALENCE IC(0372),RXGA)	65	99
	EQUIVALENCE IC(0373),RYRA)	65	100
100	EQUIVALENCE IC(0374),RZRA)	65	101
	EQUIVALENCE IC(380),RANGO)	65	102
	EQUIVALENCE IC(390),RXL)	65	103
	EQUIVALENCE IC(391),RYL)	65	104
	EQUIVALENCE IC(392),RZL)	65	105
105	EQUIVALENCE IC(393),BPHZ)	65	106
	C**CALCULATION OF HEADING, PITCH, ROLL EULER ANGLES IN DEGREES	65	107
	BPMI = ATAND(CFAS3,CFAS3)	65	108
110	BTHI = ATAND(-CFA13,SIRT(CFA11*CFAS1+CFAS2*CFAS12))	65	109
	BPSI = ATAND(CFA12,CFA11)	65	110
	C**FREE OFRO MODELS INITIAL SIGNAL ANGLES ARE ZERO	65	111
	C** AUTO PILOT ORBIT RATES	65	112
		65	113
		65	114
		65	115
		65	116
		65	117

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119 C
C ROLL CYRO DRIFT RATES PI, AND R1
DZ801=PI*Z801/CRAD
DZ801=-PI*Z801/CRAD
DZ801=PI*Y801-R1*X801/CRAD
120 C
C
C X801 = DX801/T
Y801 = 1. + DY801/T
Z801 = DZ801/T
125 C
C B12 = A011*CFA21 + A012*CFA22 + A013*CFA23
B13 = A011*CFA31 + A012*CFA32 + A013*CFA33
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VARIABLES	SN	TYPE	RELOCATION	REFS	191	DEFINED	193	DEFINED	182			
446	UV93	REAL		REFS	187	192	193					
447	UV94	REAL		REFS	4							
316	VAIRSP	REAL	C	REFS	207	203	DEFINED	201				
443	VH4U	REAL		REFS	208	DEFINED	202					
444	VH4V	REAL		REFS	207	DEFINED	203					
445	VH4W	REAL		REFS	6	201	202	203				
307	VH4XE	REAL	C	REFS	7	201	202	203				
310	VH4YE	REAL	C	REFS	8	201	202	203				
311	VH4ZE	REAL	C	REFS	86	190	DEFINED	162				
543	VTJTE	REAL	C	REFS	12	2*142	152	179	192			
502	VXE	REAL	C	DEFINED	152				2*197			
436	VXL	* REAL										
308	VXD	REAL	C	REFS	27	149	152					
450	VXP	REAL		REFS	194	195	DEFINED	191				
309	VYE	REAL	C	REFS	13	2*142	153	179	192			
447	VYC	* REAL		DEFINED	153				2*197			
307	VYS	REAL	C	REFS	24	149	153					
451	VYP	REAL		REFS	195	DEFINED	192					
312	VYI	REAL	C	REFS	14	2*142	154	181	197			
440	VZL	* REAL		DEFINED	154							
3210	VZD	REAL	C	REFS	29	150	154					
452	VZP	REAL		REFS	194	DEFINED	193					
3053	W0	REAL	C	REFS	48	3*156	3*170					
3347	X301	REAL	C	REFS	60	113	116	137	DEFINED			
3352	X302	REAL	C	REFS	63				122			
3350	Y301	REAL	C	REFS	61	113	116	137	DEFINED			
3353	Y302	REAL	C	REFS	64				123			
434	Y31	* REAL		REFS	139	DEFINED	136					
3351	Z301	REAL	C	REFS	62	117	118	136	137			
3354	Z302	REAL	C	DEFINED	124							
435	Z31	REAL	C	REFS	65							
3052	ZETA	REAL	C	REFS	139	DEFINED	137					
				REFS	47	165	170					
EXTERNALS	ATANU	TYPE	ARCS	REFERENCES	109	110	139	146	187	194	195	197
MCARLO		REAL	2	108	207	208	242					
SURT		REAL	3	190	165	169						
		REAL	1	LIBRARY	109	142	151	182	193	213		
STATEMENT LABELS	DEF LINE	REFERENCES										
147	20	155										
341	30	171										
201	503	151			241							
155	501	167			167							
LDJMS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT	REFS						
150	500	* I	151 171	348								
CJMPCN BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)									
C	3830	0	C	(3830)								
EQJIV CLASSES	LENGTH	MEMBERS	- BIAS NAME(LENGTH)									
C	3850	199	VH4XE (1)	280	VH4YE (1)	201	VH4ZE (1)					
		206	VAIRSP (1)	349	VTJTE (1)	350	W0 (1)					
		351	3PHI (1)	352	BP41 (1)	353	9TM2 (1)					
		354	BP51 (1)	355	WTOFE (1)	356	9GAMM (1)					

SUBROUTINE G5	74/74	OPT=1	FTN 4.2474355	07/0776	11.05.44.	PAGE 8
EQV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)				
367 BLAHV	(1)	367 BLAHV (1)	367 BLAHV (1)	367 BLAHV (1)	367 BLAHV (1)	
368 BLAPH	(1)	368 BLAPH (1)	368 BLAPH (1)	368 BLAPH (1)	368 BLAPH (1)	
370 RANGE	(1)	370 RANGE (1)	370 RANGE (1)	370 RANGE (1)	370 RANGE (1)	
373 RZ3A	(1)	373 RZ3A (1)	373 RZ3A (1)	373 RZ3A (1)	373 RZ3A (1)	
391 RZL	(1)	391 RZL (1)	391 RZL (1)	391 RZL (1)	391 RZL (1)	
1560 RX	(1)	1560 RX (1)	1560 RX (1)	1560 RX (1)	1560 RX (1)	
1565 SKP	(1)	1565 SKP (1)	1565 SKP (1)	1565 SKP (1)	1565 SKP (1)	
1571 GSPUTZ	(1)	1571 GSPUTZ (1)	1571 GSPUTZ (1)	1571 GSPUTZ (1)	1571 GSPUTZ (1)	
1578 ZETA	(1)	1578 ZETA (1)	1578 ZETA (1)	1578 ZETA (1)	1578 ZETA (1)	
1606 VYE	(1)	1606 VYE (1)	1606 VYE (1)	1606 VYE (1)	1606 VYE (1)	
1618 RYE	(1)	1618 RYE (1)	1618 RYE (1)	1618 RYE (1)	1618 RYE (1)	
1635 RDELY	(1)	1635 RDELY (1)	1635 RDELY (1)	1635 RDELY (1)	1635 RDELY (1)	
1654 RYF	(1)	1654 RYF (1)	1654 RYF (1)	1654 RYF (1)	1654 RYF (1)	
1668 RYO	(1)	1668 RYO (1)	1668 RYO (1)	1668 RYO (1)	1668 RYO (1)	
1671 VYO	(1)	1671 VYO (1)	1671 VYO (1)	1671 VYO (1)	1671 VYO (1)	
1680 RSJZMC	(1)	1680 RSJZMC (1)	1680 RSJZMC (1)	1680 RSJZMC (1)	1680 RSJZMC (1)	
1683 RSJZMC	(1)	1683 RSJZMC (1)	1683 RSJZMC (1)	1683 RSJZMC (1)	1683 RSJZMC (1)	
1710 CFA13	(1)	1710 CFA13 (1)	1710 CFA13 (1)	1710 CFA13 (1)	1710 CFA13 (1)	
1722 CFA23	(1)	1722 CFA23 (1)	1722 CFA23 (1)	1722 CFA23 (1)	1722 CFA23 (1)	
1734 CFA33	(1)	1734 CFA33 (1)	1734 CFA33 (1)	1734 CFA33 (1)	1734 CFA33 (1)	
1755 A022	(1)	1755 A022 (1)	1755 A022 (1)	1755 A022 (1)	1755 A022 (1)	
1758 A032	(1)	1758 A032 (1)	1758 A032 (1)	1758 A032 (1)	1758 A032 (1)	
1761 A012	(1)	1761 A012 (1)	1761 A012 (1)	1761 A012 (1)	1761 A012 (1)	
1764 RI	(1)	1764 RI (1)	1764 RI (1)	1764 RI (1)	1764 RI (1)	
1769 ZB01	(1)	1769 ZB01 (1)	1769 ZB01 (1)	1769 ZB01 (1)	1769 ZB01 (1)	
1772 ZB02	(1)	1772 ZB02 (1)	1772 ZB02 (1)	1772 ZB02 (1)	1772 ZB02 (1)	
3752 IFNOX	(10)	3752 IFNOX (10)	3752 IFNOX (10)	3752 IFNOX (10)	3752 IFNOX (10)	

STATISTICS
PROGRAM LENGTH 4568 302
CM LABELED COMMON LENGTH 73659 3838

		SUBROUTINE SPOTI	SPOT
		COMMON /C/ C(13830)	SPOT
		EQUIVALENCE (C(2562),IPL)	SPOT
		EQUIVALENCE (C(2562),IPL)	SPOT
		DIMENSION IPL(100), ISNOX(40), ITNOX(10)	SPOT
		EQUIVALENCE (C(3634), ISNOX), C(13512), I3512)	SPOT
		EQUIVALENCE (C(11580), RSJZMC)	SPOT
		EQUIVALENCE (C(11581), RSJZMC)	SPOT
		EQUIVALENCE (C(3753), ITNOX), C(37214), ITCT)	SPOT
		EQUIVALENCE (C(11562), SPOTV)	SPOT
		EQUIVALENCE (C(11572), SPOTZ)	SPOT
		EQUIVALENCE (C(11581), SIGSPOT)	SPOT
		EQUIVALENCE (C(11579), ZETA)	SPOT
		EQUIVALENCE (C(11580), W0)	SPOT
15	C	DATA W0,ZETA/3.34,0.745/	SPOT
	C	C DATA W0,ZETA/3.34,0.745/	SPOT
	C	C ZLEGO OUT SPOT JITTER MAX/MIN STORAGE LOCATIONS THAT ARE SAVED IN OUTP	SPOT
20		CTI577 = 0.	SPOT
		C(1564) = 0.	SPOT
		C(1577) = 0.	SPOT
		C(1578) = 0.	SPOT
	C	C PRINTED FROM MODULE G4	SPOT
25	C	C SPOT JITTER MONTE CARLO INITIAL VALUES	SPOT
	C	RSJZMC = 0.	SPOT
		RSJZMC = 0.	SPOT
		DO 500 IOL=1,ITCT	SPOT
30		ITSNOX = IOL	SPOT
		IF (ITNOX(IOL).NE.1600) GO TO 502	SPOT
		IPL(IOL)=1560	SPOT
		IPL(IOL)=1563	SPOT
		N=N+2	SPOT
35		IF (SIGSPOT.NE.0.)	SPOT
		1 GSFOY = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	SPOT
		CALL MGAUTO(RMSSTR,ITISNOX)	SPOT
		502 IF (ITNOX(IOL).NE.1600) GO TO 500	SPOT
40		IPL(IOL)=1570	SPOT
		IPL(IOL)=1573	SPOT
		N=N+2	SPOT
		IF (SIGSPOT.NE.0.)	SPOT
		1 GSFOY = .707*SIGSPOT/SQRT(W0/4./ZETA * C(2664))	SPOT
45		CALL MGAUTO(RMSSTR,ITISNOX)	SPOT
	C	500 CONTINUE	SPOT
		C(1564)=0. \$ C(1566)=0. \$ C(1573)=0. \$ C(1576)=0.	SPOT
		RETURN	SPOT
		END	SPOT

SUBROUTINE SPOTI		7474	OPT=1	FTW 4.2*74355	07/07/75 11.05.52.	PAGE 2
CARD NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM			
32	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.			
33	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.			
39	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.			
40	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.			

		SUBROUTINE SPOT COMMON /C/ C(3830)	SPOT 51
			SPOT 52
			SPOT 53
5		EQUIVALENCE (C(1580),RSJYMC)	SPOT 54
		EQUIVALENCE (C(1581),RSJYMC)	SPOT 55
		EQUIVALENCE (C(1582),RSPOTX)	SPOT 56
		EQUIVALENCE (C(1583),RSPOTY)	SPOT 57
		EQUIVALENCE (C(1584),RSPOTZ)	SPOT 58
10		EQUIVALENCE (C(1585),ITNOK)	SPOT 59
		EQUIVALENCE (C(1586),ITCT)	SPOT 60
		EQUIVALENCE (C(1587),SXPDD)	SPOT 61
		EQUIVALENCE (C(1588),RX)	SPOT 62
		EQUIVALENCE (C(1589),SXPOT)	SPOT 63
15		EQUIVALENCE (C(1590),SXPDI)	SPOT 64
		EQUIVALENCE (C(1591),SXPDI)	SPOT 65
		EQUIVALENCE (C(1592),SYPODI)	SPOT 66
		EQUIVALENCE (C(1593),RM)	SPOT 67
		EQUIVALENCE (C(1594),SXPOTZ)	SPOT 68
20		EQUIVALENCE (C(1595),SYP)	SPOT 69
		EQUIVALENCE (C(1596),ZETA)	SPOT 70
		EQUIVALENCE (C(1597),W0)	SPOT 71
		DIMENSION ITNOX(10)	SPOT 72
25		C LINE OF SIGHT OF LASER SPOT WITH MONTE CARLO SPOT JITTER INCLUDED	SPOT 73
			SPOT 74
			SPOT 75
		DO 500 I = 1, ITCT	SPOT 76
		IDO = I	SPOT 77
		IF (ITNOX(I).NE.1580) GO TO 501	SPOT 78
30		RSJYMC = GSPOTY*SXP	SPOT 79
		CALL MCARLO (DUM,2,IDO)	SPOT 80
		SXPDD = W0+W0*(RY-2.*ZETA+SXPDI/W0 - SXP)	SPOT 81
		501 IF (ITNOX(I).NE.1581) GO TO 500	SPOT 82
		RSJYMC = GSPOTZ*SYP	SPOT 83
35		CALL MCARLO (DUM,2,IDO)	SPOT 84
		SYPDD = W0+W0*(RY - 2.*ZETA+SYPDI/W0 - SYP)	SPOT 85
		500 CONTINUE	SPOT 86
		RETURN	SPOT 87
		END	SPOT 88

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
1 SPOT 37

VARIABLES	SN	TYPE	RELLOCATION	DEF LINE	REFERENCES	EXT REFS
0 C		REAL	C	2	10	
47 DUM		REAL		11	12	
5031 GSPOTY		REAL		19	20	
5043 GSPOTZ		REAL	C	30	31	
49 I		INTEGER		13	23	
40 IDO		INTEGER		10	31	
7210 ITCT		INTEGER	C	27	29	26
7250 IYNDX		INTEGER	C	30	31	27
5217 RSJYMC		REAL	C	10	25	32
5250 RSJZMC		REAL	C	9	21	
5221 RSPOTX		REAL	C	4	DEFINED	29
5222 RSPOTY		REAL	C	5	DEFINED	33
5223 RSPOTZ		REAL	C	6		
5030 RX		REAL	C	8		
5042 NY		REAL	C	12	31	
5035 SXP		REAL	C	17	35	
5032 SXQ		REAL	C	15	23	31
5027 SXPOU		REAL	C	14	31	
5047 SYP		REAL	C	11	DEFINED	31
5044 SYPO		REAL	C	20	33	35
5041 SYPOU		REAL	C	19	35	
5033 W0		REAL	C	16	DEFINED	35
5032 ZETA		REAL	C	22	3431	3435
EXTERNALS		TYPE	ANGS	DEF LINE	REFERENCES	
MCARLO			3	30	34	

STATEMENT LABELS	DEF LINE	REFERENCES
34 503	30	26
20 501	32	28

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
3 503	1	20 36	343		

COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3650	0 C	(3030)

ENTRY CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3650	1559 SXPOU (1)	1551 GSPOTY (1)
		1562 SXPO (1)	1559 SYPOU (1)
		1570 SY (1)	1572 SXPO (1)
		1575 SYP (1)	1579 W0 (1)
		1679 RSJYMC (1)	1591 RSPOTY (1)
		1682 RSPOTY (1)	3720 ITCT (1)
		3752 IYNDX (10)	

STATISTICS	PUJGMAM LENGTH	508	40
ON LARGEST COMMON LENGTH	73663	3430	

SUBROUTINE A1	74/74	OPT=1	FTN 4.2+74.355	07/07/75	11.05.55.	PAGE 3
115	CNP = CNP+CON*USPPI CNP = CNP+USPPI C**CALCULATION OF SURFACE COEFFICIENTS BDL = (-3SURFI+BSURF2+BSURF3+BSURF4)/4. BDM = (-BSURFI+BSURF2+BSURF3+BSURF4)/4. BDN = (-BSURFI+BSURF2+BSURF3+BSURF4)/4. XINTER=0. CALL TABL3 (BALPHP,BDM,VHACH,CLA,CDF,MCO,XINTER,44,ZQ,CZQ) XINTER=0. CALL TABL3 (BALPHP,BDM,VHACH,CLA,CDF,MCO,XINTER,44,CYR,CYR) XINTER=0. CALL TABL3 (BALPHP,BDM,VHACH,CLA,MDF,MCO,XINTER,44,CHR,CHR) XINTER=0. CALL TABL3 (BALPHP,BDM,VHACH,CLA,MDF,MCO,XINTER,44,CNQ,CNQ) XINTER=0. CALL TABL3 (BALPHP,BDL,VHACH,CLA,DLF,MCO,XINTER,44,CLO,CLO) CZE=(CNP+CZO+UCPHI*BDM-CYR*USPPI+BDM) CZE=(CNP+CZO+UCPHI*BDM-CZO*USPPI+BDM) CLT=CRCLO+BDLT CLMP=(CNP+CNO+UCPHI*BDM-CHR*USPPI+BDM) CLNP=(CNP+CHR+UCPHI*BDM+CNO*USPPI+BDM) CY = CYP+UCPHI-CZE*USPPI CZ = -CZE*UCPHI-CYP*USPPI CM = CLMP+UCPHI+CLNP+JSPMI CN = CLNP+UCPHI-CLMP+USPPI RETURN END					
120						
125						
130						
135						
140						

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000
VARIABLES	SN	TYPE	RELOCATION																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							

[illegible]

EXTERNALS		TYPE		ARGS		REFERENCES		DEF LINE		REFERENCES	
		REAL		1		83		85		87	
COSD		REAL		1		83		85		87	
SIND		REAL		7		94		98		99	
TABLE				8		96		111		112	
TABL2						110		124		126	
TABL3				9		122				130	
										106	
										107	
										108	
										109	
INLINE FUNCTIONS		TYPE		ARGS		DEF LINE		REFERENCES			
		REAL		1		INTRIN		88		89	
STATEMENT LABELS										90	
0 1		INACTIVE		7 8						91	
										92	
COMMON BLOCKS		LENGTH		MEMBERS		BIAS NAME(LENGTH)					
C		3830		0 C		(3830)					
NOS		18		0 NCX		(6)				5 NCN	
				12 MCD		(6)				10 NC3	
				0 DKA		(9)					
CXARG		9		0 D24		(10)					
CZARG		10		0 D24		(10)					
CXARG		8		0 D24		(10)					
CLDARG		14		0 D24		(10)					
CXFUN		18		0 D24		(10)					
CZFUN		24		0 D24		(10)					
DCZFUN		24		0 D24		(10)					
CHFUN		24		0 D24		(10)					
DCMFUN		24		0 D24		(10)					
CXOFUN		8		0 D24		(10)					
CZOFUN		24		0 D24		(10)					
CY2FUN		24		0 D24		(10)					
CL2FUN		24		0 D24		(10)					
CL3FUN		24		0 D24		(10)					
CZ3FUN		92		0 D24		(10)					
CXOFUN		92		0 D24		(10)					
CL3FUN		42		0 D24		(10)					
CXOFUN		24		0 D24		(10)					
CL3FUN		24		0 D24		(10)					
EQUIV CLASSES		LENGTH		MEMBERS		BIAS NAME(LENGTH)					
C		3830									
				203 VMACH		(1)				357 BALPH	
				368 BALPH		(1)				1102 SUBEL	
				1106 SSURF2		(1)				1114 SSURF4	
				1202 CX		(1)				1204 CZ	
				1205 CLP		(1)				1207 GMR	
				1208 CL		(1)				1210 CN	
				1211 G40		(1)				1213 GMP	
				1214 G2		(1)				1217 G2	
				1218 G2		(1)				1220 GMDQM	
				1221 G42		(1)				1223 CYQ	
				1224 31-00P		(1)				1226 G42	
				1227 CLMP		(1)				1229 BOEFL	
				1230 30L		(1)				1232 90N	
				1233 COCM		(1)				1239 CL2	
				1240 CL3		(1)				1244 GYPU	
				1246 CMP		(1)				1248 CLR	
				1249 G4P		(1)				1250 30M0	
				1270 30NO		(1)				1253 DER	

07/07/75 11:05:55

FTN 4.2+7.355

OPT=1

74/74

SUBROUTINE A1

STATISTICS

PROGRAM LENGTH	3479	359
CM LABELED COMMON LENGTH	105178	4431

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SUBROUTINE A31
C**INITIALIZATION FOR ENGINE MODULE
COMMON /C/ C(3838)
DIMENSION IPL(100), ISNOX(40)
EQUIVALENCE (C(3634), ISNOX), (C(3512), I3512)
EQUIVALENCE (C(367), BALPHA)
EQUIVALENCE (C(368), BALPHY)
EQUIVALENCE (C(370), RPHIP)
EQUIVALENCE (C(1308), ROELCG)
EQUIVALENCE (C(1320), FMXTH)
EQUIVALENCE (C(1321), FMYTH)
EQUIVALENCE (C(1322), FMZTH)
EQUIVALENCE (C(1457), GR40)
EQUIVALENCE (C(1411), FTHX)
EQUIVALENCE (C(1412), FTHY)
EQUIVALENCE (C(1413), FTHZ)
EQUIVALENCE (C(1415), JMT)
EQUIVALENCE (C(1418), ROCCGF)
EQUIVALENCE (C(1419), MIXE)
EQUIVALENCE (C(1420), FMYF)
EQUIVALENCE (C(1628), CMASS)
EQUIVALENCE (C(1739), MP)
EQUIVALENCE (C(1743), MQ)
EQUIVALENCE (C(1747), MR)
EQUIVALENCE (C(1748), MIX)
EQUIVALENCE (C(1749), FMIY)
EQUIVALENCE (C(1750), FMIZ)
EQUIVALENCE (C(2000), I)
EQUIVALENCE (C(2501), N)
EQUIVALENCE (C(2562), IPL)
EQUIVALENCE (C(1731), GR40)
EQUIVALENCE (C(626), V13)
EQUIVALENCE (C(1737), FMK), (C(1741), FMY), (C(1745), FMZ)
DATA IFLG1, IFLG2 / 0, /
IPL(N) = 1436
N = N+1
C(1739) = 0.
C
IF (GR40 .GT. 0.) GO TO 10
GR40 = 57.295773
FMK = 0.
FMY = 0.
FMZ = 0.
MQ = 0.
MR = 0.
BALPHA = 0.
BALPHY = 0.
RPHIP = 0.
C
C MONTGOMERY THRUST DIRECTION ERRORS
C
GO 3 I = 1, I3512
IOC = I
IF (ISNOX(I) .EQ. 1313) CALL MCARLO (DUM, I, IOC)
IF (ISNOX(I) .EQ. 1314) CALL MCARLO (DUM, I, IOC)
IF (ISNOX(I) .EQ. 1315) CALL MCARLO (DUM, I, IOC)
IF (ISNOX(I) .EQ. 1401) CALL MCARLO (DUM, I, IOC)
IF (ISNOX(I) .EQ. 1402) CALL MCARLO (DUM, I, IOC)

```

```

00 MONTE CARLO TYPE=ROLL,PATCH AND VAN RATES
   IF(LSNOX(1).EQ.1730)CALL MCARLO(0,0,0,1,100)
   IF(LSNOX(1).EQ.1740)IFLG2=0
   IF(LSNOX(1).EQ.1742)IFLG1=0
   CONTINUE
60      3
05      3
      IF(FLG1.EQ.160 TO 3
      CALL LRAN(1,DELTC(1740),0,0,0,IFLG2,1)
      CALL LRAN(1,DELTC(1742),0,0,0,IFLG1,2)
      WQ=WQ/FM1YF
      *CRAO
      WR=WR/FM1YF
      CONTINUE
70      3
      IF(FLG1=1
      IF(FLG2=1
      RETURN
      10 CONTINUE
      F1RST=0.
      F1RND=0.
      F1M1=0.
      F1M2=0.
      F1M3=0.
      F1M4=0.
      F1M5=0.
      F1M6=0.
      F1M7=0.
      F1M8=0.
      F1M9=0.
      F1M10=0.
      F1M11=0.
      F1M12=0.
      F1M13=0.
      F1M14=0.
      F1M15=0.
      F1M16=0.
      F1M17=0.
      F1M18=0.
      F1M19=0.
      F1M20=0.
      F1M21=0.
      F1M22=0.
      F1M23=0.
      F1M24=0.
      F1M25=0.
      F1M26=0.
      F1M27=0.
      F1M28=0.
      F1M29=0.
      F1M30=0.
      F1M31=0.
      F1M32=0.
      F1M33=0.
      F1M34=0.
      F1M35=0.
      F1M36=0.
      F1M37=0.
      F1M38=0.
      F1M39=0.
      F1M40=0.
      F1M41=0.
      F1M42=0.
      F1M43=0.
      F1M44=0.
      F1M45=0.
      F1M46=0.
      F1M47=0.
      F1M48=0.
      F1M49=0.
      F1M50=0.
      F1M51=0.
      F1M52=0.
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      F1M54=0.
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      F1M356=0.
      F1M357=0.
      F1M358=0
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AD-A032 048

ARMY MISSILE RESEARCH DEVELOPMENT AND ENGINEERING LAB--ETC F/G 16/4
THAD T-7 MISSILE MONTE-CARLO TERMINAL HOMING SIMULATION UTILIZI--ETC(U)
JUL 76 C L LEWIS, W R HOOKER, A W LEE

UNCLASSIFIED

RG-7T-2

NL

5 of 7
ADA032048



Resolution test chart showing patterns of vertical and horizontal lines with numerical values: 1.0, 1.1, 1.25, 1.4, 1.6, 1.8, 2.0, 2.2, 2.5, 2.8, 3.2, 3.6, 4.0, 4.5, 5.0, 5.6, 6.3, 7.1, 8.0, 9.0, 10.

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES 85
1 A31 72

VARIABLES SN TYPE RELOCATION

550	BALPHA	REAL			REFS	9	DEFINED	45	
557	BALPHA	REAL			REFS	7	DEFINED	46	
561	BALPHA	REAL			REFS	8	DEFINED	47	
0	C			ARRAY	REFS	3	2*5	6	7
					REFS	11	12	13	14
					REFS	19	20	21	22
					REFS	27	28	29	30
					REFS	66	DEFINED	37	38
3326	CRAD	REAL			REFS	31	67	68	DEFINED
146	DLT	REAL			REFS	65			48
3133	DMASS	REAL			REFS	21	DEFINED	91	
145	DUM	REAL			REFS	53	54	55	
					REFS	66		56	57
					REFS	17		58	59
2006	DMT	REAL			REFS	25	DEFINED	43	
3323	FMIX	REAL			REFS	19			
2012	FMIX	REAL			REFS	26	DEFINED	84	85
3324	FMIX	REAL			REFS	20	67	68	
2013	FMIX	REAL			REFS	27	DEFINED	85	
3325	FMIX	REAL			REFS	33	DEFINED	41	
3310	FMIX	REAL			REFS	10	DEFINED	78	
2447	FMIX	REAL			REFS	33	DEFINED	41	
3314	FMIX	REAL			REFS	11	DEFINED	79	
2450	FMIX	REAL			REFS	33	DEFINED	41	
3320	FMIX	REAL			REFS	12	DEFINED	80	
2451	FMIX	REAL			REFS	74			
151	FT18ST	REAL			REFS	14	DEFINED	75	
2002	FT1X	REAL			REFS	15	DEFINED	76	
2003	FT1Y	REAL			REFS	16	DEFINED	77	
2004	FT1Z	REAL			REFS	52	53	54	
148	I	INTEGER			REFS	61	DEFINED	51	55
					REFS	53		56	57
144	IOO	INTEGER			REFS	52		58	59
					REFS	65	DEFINED	34	78
135	IFLGI	INTEGER			REFS	62	DEFINED	34	78
136	IFLGI	INTEGER			REFS	4	30	35	
2001	IPL	INTEGER			REFS	4		59	56
2001	ISNOX	INTEGER			REFS	60		61	57
					REFS	59		61	
2007	IS312	INTEGER			REFS	29	35	36	DEFINED
2000	N	INTEGER			REFS	13	89		86
2074	QBARN	REAL			REFS	18	82		
2011	RO2GF	REAL			REFS	9	DEFINED	82	
2433	RO2GF	REAL			REFS	28	65	66	
3717	T	REAL			REFS	32	64	65	
1161	V19	REAL			REFS	22	DEFINED	42	
3312	MP	REAL			REFS	23	DEFINED	43	67
3316	M2	REAL			REFS	66	67		
150	MOO	REAL			REFS	24	DEFINED	44	68
3322	MS	REAL			REFS	65		68	
147	MR0	REAL			REFS				

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SUBROUTINE A3	74/74	OPT=1	FTN 4.2474355	07/07/75	11-05-59*	PAGE	1
SUBROUTINE A3							
C**ENGINE ROUTINE							
COMMON /C/ C(3838)							
5	C	COMMON/NTM/NTM(2) /THRG/THA(20) /THUN/TF(20)				A3	89
	C					A3	90
	C					A3	91
	C					A3	92
	C					A3	93
	C					A3	94
	C					A3	95
	C					A3	96
	C					A3	97
10	C					A3	98
	C					A3	99
	C					A3	100
	C					A3	101
	C					A3	102
	C					A3	103
	C					A3	104
	C					A3	105
	C					A3	106
	C					A3	107
	C					A3	108
	C					A3	109
	C					A3	110
	C					A3	111
	C					A3	112
25	C					A3	113
	C					A3	114
	C					A3	115
	C					A3	116
	C					A3	117
	C					A3	118
	C					A3	119
	C					A3	120
	C					A3	121
	C					A3	122
	C					A3	123
	C					A3	124
	C					A3	125
	C					A3	126
	C					A3	127
	C					A3	128
	C					A3	129
	C					A3	130
	C					A3	131
	C					A3	132
	C					A3	133
	C					A3	134
	C					A3	135
	C					A3	136
	C					A3	137
	C					A3	138
	C					A3	139
	C					A3	140
	C					A3	141
	C					A3	142
	C					A3	143
	C					A3	144
	C					A3	145

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	79	86
1 A3	1	49		
VARIABLES SN TYPE RELOCATION				
2570 BRCPMT REAL	C		REFS 11	54
2571 RP41T REAL	C		REFS 12	55
0 C	ARRAY C		REFS 3	9
			14	10
			15	17
			22	19
			23	20
			25	21
			29	32
			33	33
			35	39
			37	40
			45	41
2605 CISP REAL	C		REFS 16	70
3133 OMAS REAL	C		REFS 39	72
2607 DMZ REAL	C		REFS 18	71
2606 DMT REAL	C		REFS 47	2*75
3123 FMIX REAL	C		REFS 40	75
2612 FMIXO REAL	C		REFS 21	75
3124 FMIX REAL	C		REFS 41	77
3125 FMIXO REAL	C		REFS 22	77
3125 FMIX REAL	C		REFS 42	77
2447 FMIX REAL	C		REFS 30	64
2450 FMIX REAL	C		REFS 31	65
2451 FMIX REAL	C		REFS 32	66
2601 FTARST REAL	C		REFS 34	54
			79	55
2602 FT4X REAL	C		REFS 35	59
2603 FT4Y REAL	C		REFS 36	59
2604 FT4Z REAL	C		REFS 37	58
0 NT4 INTEGER	ARRAY	MTN	REFS 5	50
2573 PCFTM REAL	C		REFS 14	89
2574 QBJRN REAL	C		REFS 15	89
2572 QNALGN REAL	C		REFS 13	52
2611 R02CF REAL	C		REFS 20	73
2610 R02CO REAL	C		REFS 13	2*73
2433 R02COG REAL	C		REFS 29	79
2440 R02CO REAL	C		REFS 8	59
2441 R02CO REAL	C		REFS 9	59
2442 R02CO REAL	C		REFS 10	57
2615 RL3G REAL	C		REFS 30	70
2614 RL3GO REAL	C		REFS 23	70
2717 T REAL	C		REFS 26	81
0 THA REAL	THARG		REFS 5	50
0 THF REAL	THFUN		REFS 5	50
2600 UDAP REAL	C		REFS 33	72
			70	73
			75	76
2732 UI4P REAL	C		REFS 46	70
2727 UIMPD REAL	C		REFS 45	50
115 USINA REAL			REFS 55	50
114 XF REAL			REFS 56	50
FILE NAMES	MODE			
TAPE6	FMT			
		WRITES	81	

SUBROUTINE A3				74/74	OPT=1
EXTERNALS	TYPE	ARGS	REFERENCES		
COSD	REAL	1	54	96	
SIND	REAL	1	53	55	
TABLE		7	50		
STATEMENT LABELS					
0 10	INACTIVE	53	52		
35 20		61	2+52		
37 30		67	50		
105 103	FMT	92	91		
COMMON BLOCKS					
C	LENGTH	3830	MEMBERS - BIAS NAME(LENGTH)		
			0 5 (3830)		
MTA	2		0 MTA 124		
THRG	20		0 TMA 120		
THFUN	20		0 TAP 120		
EQUIV CLASSES					
C	LENGTH	3830	MEMBERS - BIAS NAME(LENGTH)		
			1307 RDELG (1)		
			1314 RFZCG (1)		
			1321 FMZTH (1)		
			1402 QNALGM (1)		
			1408 UIMP (1)		
			1411 FTHV (1)		
			1414 DMT (1)		
			1417 RDCG (1)		
			1420 RLGG (1)		
			1498 UIMP (1)		
			1527 DMAS (1)		
			1749 FMIZ (1)		
			1312 RFYCG (1)		
			1319 FMATM (1)		
			1400 BALPMT (1)		
			1403 PCFTH (1)		
			1409 FTHST (1)		
			1412 FTHZ (1)		
			1415 DWP (1)		
			1416 FMIX (1)		
			1421 RLGG (1)		
			1498 UIMP (1)		
			1527 DMAS (1)		
			1749 FMIZ (1)		
			1313 RFYCG (1)		
			1319 FMATM (1)		
			1401 BALPMT (1)		
			1404 QBUSM (1)		
			1410 FTHX (1)		
			1413 CISP (1)		
			1415 RDCG (1)		
			1419 FMIX (1)		
			1421 RLGG (1)		
			1498 UIMP (1)		
			1527 DMAS (1)		
			1749 FMIZ (1)		
			1313 RFYCG (1)		
			1319 FMATM (1)		
			1401 BALPMT (1)		
			1404 QBUSM (1)		
			1410 FTHX (1)		
			1413 CISP (1)		
			1415 RDCG (1)		
			1419 FMIX (1)		
			1421 RLGG (1)		
			1498 UIMP (1)		
			1527 DMAS (1)		
			1749 FMIZ (1)		

STATISTICS
PROGRAM LENGTH 1208 86
CM LABELED COMMON LENGTH 74408 3872

SUBROUTINE A2		BODY AXES	
C**AEKG FORCE AND MOMENT MODULE			
COMMON /C/ C(3630)			
101 FORMAT (1H0.4X,21HFRONT LUG CLEARS RAIL.5X,3HT =,1PE10.2,5X,			
9HREL VEL =,1PE10.2,5X,14HPITCH MOMENT =,1PE10.2)			
5	C		
C**INPUT DATA			
		EQUIVALENCE (C(1306),RFAREA)	A2
		EQUIVALENCE (C(1307),REFLOTH)	A2
		EQUIVALENCE (C(1316),RLUG)	A2
		EQUIVALENCE (C(1317),RAIL)	A2
		EQUIVALENCE (C(1742), AMPZ), (C(1746), AMP1)	A2
		EQUIVALENCE (C(1332),CPH43)	A2
		EQUIVALENCE (C(1405),CRUPN)	A2
		EQUIVALENCE (C(1527),AGRAV)	A2
15	C		
C**INPUTS FROM OTHER MODULES			
DIMENSION ISNDX(40)			
		EQUIVALENCE (C(1363), ISNDX), (C(3512), IS512)	A2
		EQUIVALENCE (C(1203),PDYNMC)	A2
		EQUIVALENCE (C(1204),VMACH)	A2
		EQUIVALENCE (C(1207),VAIRSPI)	A2
		EQUIVALENCE (C(1301),STHT)	A2
		EQUIVALENCE (C(1301),RANGO)	A2
		EQUIVALENCE (C(11203),SK)	A2
		EQUIVALENCE (C(11204),ZY)	A2
		EQUIVALENCE (C(11205),ZP)	A2
		EQUIVALENCE (C(11206),CLP)	A2
		EQUIVALENCE (C(11207),CMQ)	A2
		EQUIVALENCE (C(11208),CMR)	A2
		EQUIVALENCE (C(11209),CL)	A2
		EQUIVALENCE (C(11210),CN)	A2
		EQUIVALENCE (C(11211),CN)	A2
		EQUIVALENCE (C(11201),FMXTH)	A2
		EQUIVALENCE (C(11321),FMYTH)	A2
		EQUIVALENCE (C(11322),FMYTH)	A2
		EQUIVALENCE (C(11411),FTHX)	A2
		EQUIVALENCE (C(11412),FTHY)	A2
		EQUIVALENCE (C(11413),FTZ)	A2
		EQUIVALENCE (C(11422),FLCG)	A2
		EQUIVALENCE (C(11723),2FA23)	A2
		EQUIVALENCE (C(11735),2FA33)	A2
		EQUIVALENCE (C(11739),MP)	A2
		EQUIVALENCE (C(11743),4Q)	A2
		EQUIVALENCE (C(11737), FMX), (C(1741), FMY), (C(1745), FMY)	A2
		EQUIVALENCE (C(11747),4R)	A2
		EQUIVALENCE (C(11748), FMX)	A2
		EQUIVALENCE (C(11781), MPTD)	A2
		EQUIVALENCE (C(11751), GRA9)	A2
		EQUIVALENCE (C(1526), V13)	A2
		EQUIVALENCE (C(12888),F)	A2
		EQUIVALENCE (C(11972),RKUTTA)	A2
		EQUIVALENCE (C(11975),NPT)	A2
50	C		
C**OUTPUTS			
		EQUIVALENCE (C(1300),FX3A)	A2
		EQUIVALENCE (C(1301),FV3A)	A2
55	C		
C**OUTPUTS			
		EQUIVALENCE (C(1300),FX3A)	A2
		EQUIVALENCE (C(1301),FV3A)	A2


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60 EQUIVALENCE (C(1307),FZBA )
EQUIVALENCE (C(1303),FMXBA )
EQUIVALENCE (C(1304),FMYBA )
EQUIVALENCE (C(1305),FMZBA )
EQUIVALENCE (C(1308),ROELCG )
EQUIVALENCE (C(1328),DMASS )
EQUIVALENCE (C(1348),FMIX )
EQUIVALENCE (C(1749),FMY )
EQUIVALENCE (C(1750),FMIZ )

65 C**JUNK OUTPUTS
EQUIVALENCE (C(1323),FMXLUG )
EQUIVALENCE (C(1324),FMZLUG )
EQUIVALENCE (C(1325),FMZLUG )
EQUIVALENCE (C(1350),OPTN )

70 C**FORCE VECTOR COMPONENTS
UQS = FOMMC*REAREA
UQSL = UQS*REFLTH

75 C
FMA = UQS*(-OX)*FTHX
FMY = UQS*CY*FTHY
FMB = UQS*SZ*FTHZ

80 C
C**ZERO MOMENTS (NOTE: FACTOR OF 2.0 IN DAMPING COEFFICIENT)
UL2V = 0.
IF (VAIRSP .GT. 0.) UL2V = RFLGTM/12.*VAIRSP
FMA3A = (CL + CLP*UL2V*MP) * UQSL + FMXTH
FMY3A = (CM + CMQ*UL2V*MQ) * UQSL + FZBA*ROELCG + FMYTH
FMZ3A = (CN + CNR*UL2V*MR) * UQSL - FZBA*ROELCG + FMZTH

85 C
C**MOMENTS AND FORCES DUE TO LUGS
IF (LOPTN4 .GT. 0.) AND. (RANGO .LE. RAIL*RLUG) ) GO TO 70
UFZL2=FZLUG
FYLUG = 0.
FZLUG = 0.
FMXLUG = 0.
FMYLUG = 0.
FMZLUG = 0.
IF (FLW2 .GT. 0.) GO TO 74
FMX=0.
FMY=0.
FMZ=0.
DO 6 I=1,13512
100 I=0
IF (ISNDX(I).EQ.1743) CALL MCARL(I,OUN+1,100)
IF (ISNDX(I).EQ.1747) CALL MCARL(I,OUN+1,100)
CONTINUE
C(13) = 1.
WRITE(I,100) MP,MR,MS
104 FORMAT(1H,50X,'TIPOFF RATES--ROLL = *F6.1,* PITCH = *F6.1,
* YAW = *F6.1)
ELG2 = 1.
WRITE(I,102) T,VAIRSP,UFZL2
WRITE(I,103) RANGO
103 FORMAT(1H,30H
102 REAR LUG CLEARS RAIL T = *F6.4,
* 10HREL VEL = *F6.3,10H RAIL FORCE = *F6.2)

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SUBROUTINE A2	74/74	OPT=1	FTN 4.2+74355	07/07/76	11.06.01.	PAGE	3
119	GO TO 74					116	
	70 IF (RANGC .LE. RAIL) GO TO 72					117	
	RZOD=0.					118	
	FYLUG = -(FYBA + DMAS*AGRAV*(CFA23 + FYZBA*					119	
	* RLCG*DMAS*FMI2/11. + DMAS*RLCG*RLCG/FMI2)					120	
120	FZLUG = -(FZBA + DMAS*AGRAV*(CFA33-RZODI + FYZBA*					121	
	* RLCG*DMAS*FMI2/11. + DMAS*RLCG*RLCG/FMI2)					122	
	FHALUG = - FHXBA					123	
	FMYLUG = FZLUG*RLCG					124	
	FMYLUG = FZLUG*RLCG					125	
125	IF (FLG1 .GT. 0.) GO TO 74					126	
	FLG1 = 1.					127	
	WRITE(10,103) RANGC					128	
	WRITE(10,103) RANGC					129	
						130	
130						131	
						132	
						133	
						134	
						135	
135						136	
						137	
						138	
						139	
140	DTUG=0.06					140	
	FHX=HPTD*FMI2/CRAO/DTUG					141	
	CONTINUE					142	
						143	
						144	
145						145	
	GO TO 74					146	
	72 CONTINUE					147	
	RZOD=0.					148	
	FYLUG = -(FYBA + DMAS*AGRAV*(CFA23)					149	
150	FZLUG = -(FZBA + DMAS*AGRAV*(CFA33-RZODI)					150	
	FMYLUG = FZLUG*RLCG					151	
	FMYLUG = FZLUG*RLCG					152	
	FZLUG = FZLUG*RLCG					153	
	FZLUG = FZLUG*RLCG					154	
155	FLG2=0.					155	
	74 CONTINUE					156	
	C**TOTAL FORCE AND MOMENTS					157	
	FYBA = FYBA + FYLUG					158	
	FZBA = FZBA + FZLUG					159	
160	FHXBA = FHXBA + FMYLUG					160	
	FMYBA = FMYBA + FMYLUG					161	
	FYZBA = FYZBA + FMYLUG					162	
						163	
						164	
165	C**LAUNCH TRANSIENTS MOMENTS (1-YA,2-PITCH,3-ROLL MOMENTS)					165	
	IF (FLG2 .GT. 0.160 TO 75					166	
	IF (FLG2 .GT. 0.160 TO 75					167	
	CALL LIRANT,DEL,AMP2,FMY,10.1.2)					168	
	CALL LIRANT,DEL,AMP2,FMY,10.1.2)					169	
170	CONTINUE					170	
	FHXBA=FHXBA+FHX					171	
						172	

SUBROUTINE A2	74/74	OPT=1	FTN 4.2+74.355	07/07/76	11.06.01.	PAGE 4
175	C	PM3A=PM3A+PMZ FM3A=FM3A+FMZ		A2 A2 A2 A2 A2	174 174 175 176 177	
		REURN				
		END				

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES
1 A2	1	175
VARIABLES	SN TYPE	RELOCATION
3132 AGRAV	REAL	C
3321 AMPI	REAL	15
3315 ANP2	REAL	12
335 BTH1	REAL	169
0 C	REAL	23
	ARRAY	C
	REAL	3
	REAL	9
	REAL	20
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VARIABLES	SN	TYPE	RELOCATION	REFS	DEF	106	110	111	127	128
2004 FT4Z	REAL	C		REFS	56	DEFINED	78			
2423 FX3A	REAL	C		REFS	97	110	149	150		
2424 FX3A	REAL	C		DEFINED	79	154				
343 FYUG	REAL	C		REFS	124	150	DEFINED	93	110	149
2425 F23A	REAL	C		REFS	150	120	150	159		
344 FZUG	REAL	C		DEFINED	80	159	DEFINED	94	120	150
345 I	INTEGER	C		REFS	92	123	159	DEFINED	100	
346 I33	INTEGER	C		REFS	101	102	103	101		
7061 I5N0X	INTEGER	C		REFS	102	103	DEFINED	101		
3667 I3512	INTEGER	C		REFS	18	104	102	103		
3668 INT	INTEGER	C		REFS	19	100				
3657 OPTN4	REAL	C		REFS	53					
312 P0YHMC	REAL	C		REFS	72	91				
2574 Q3JRN	REAL	C		REFS	20	75				
2444 RAIL	REAL	C		REFS	14					
273 RAVGO	REAL	C		REFS	11	91	116			
2433 R0LUG	REAL	C		REFS	24	91	111	116	120	
2431 RFAREA	REAL	C		REFS	62	65	97			
2432 RFLGTH	REAL	C		REFS	8	73				
2663 R0JTTA	REAL	C		REFS	9	75	94			
2615 RL2G	REAL	C		REFS	52					
2443 RLJG	REAL	C		REFS	40	3*110	3*120	123	124	
350 R730	REAL	C		REFS	10	91	3*110	123	124	
317 T	REAL	C		REFS	120	150	3*110	117	140	
341 UFZL2	REAL	C		REFS	51	110	127	160	169	
340 UL2V	REAL	C		REFS	110	DEFINED	92	DEFINED	83	94
336 U35	REAL	C		REFS	85	65	87	DEFINED	88	75
337 U35L	REAL	C		REFS	76	73	79	DEFINED	76	
310 V4IR3P	REAL	C		REFS	85	85	87	DEFINED	127	
1161 V13	REAL	C		REFS	22	2434	110			
313 V44CM	REAL	C		REFS	50	167				
3312 MP	REAL	C		REFS	21					
3311 MPTO	REAL	C		REFS	43	85	106			
3310 M1	REAL	C		REFS	40	140				
353 M20	REAL	C		REFS	44	85	106			
332 M4	REAL	C		REFS	160					
355 M0	REAL	C		REFS	46	87	106			
FILE NAMES	MODE									
TAPES	FMT			WRITES	106	110	111	127	128	

EXTERNALS	TYPE	ARGS	DEF LINE	REFERENCES
LTRAN	7	3		150
MCARLO	3			102

STATEMENT LABELS	INACTIVE	DEF LINE	REFERENCES
0	141		
0	104		100
103 70	110		91
146 72	147		116
104 74	150		98
204 75	170		166
230 101	142		127
305 102	113		110
402 103	111		128

STATEMENT LABELS		DEF LINE REFERENCES	
257	104	107	105
LUPS LABEL INDEX		FROM-TO	LENGTH
56	0	100	104
COMMON BLOCKS		MEMBERS - BIAS NAME(LENGTH)	EXT REFS
0	0	0	3830
EQUIV CLASSES		MEMBERS - BIAS NAME(LENGTH)	
0	0	0	3830
202 PDYMC (1)		203 VMCH (1)	216 VAIRSP (1)
349 BTMT (1)		379 RANGD (1)	625 VIB (1)
1202 CX (1)		1203 CY (1)	1204 CZ (1)
1205 CLP (1)		1206 CMQ (1)	1207 CNR (1)
1208 CL (1)		1209 CM (1)	1210 CN (1)
1299 FKBA (1)		1300 FYBA (1)	1301 FZBA (1)
1302 FMBA (1)		1303 FM3A (1)	1304 FM2BA (1)
1305 RFAREA (1)		1306 RFLGTH (1)	1307 RDELGC (1)
1315 RLUG (1)		1316 RAIL (1)	1317 FMTH (1)
1320 FMTH (1)		1321 FM2TH (1)	1322 FM1MC (1)
1323 FM1UG (1)		1324 FMZUG (1)	1331 CPBAS (1)
1404 QSDRN (1)		1410 FTHA (1)	1411 FTHB (1)
1412 FTHZ (1)		1421 RLGS (1)	1616 ACBAW (1)
1627 DMRSS (1)		1722 CR23 (1)	1734 CR35B (1)
1736 FMX (1)		1737 MPTD (1)	1738 MP (1)
1740 FMY (1)		1741 AMPD (1)	1742 MQ (1)
1744 FMZ (1)		1745 AMPL (1)	1746 MR (1)
1747 FMX (1)		1748 FMY (1)	1749 FMZ (1)
1750 GRAD (1)		1771 RKUTTA (1)	1974 MPT (1)
1999 T (1)		3503 OPTN4 (1)	3511 I3512 (1)
3633 ISNOX (140)			

STATISTICS	
PROGRAM LENGTH	3568
CH LABELED COMMON LENGTH	73668
	3830

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SUBROUTINE LTRAN(T,DE,T,AMP,Y,YG,Z,LOGK)
  DIMENSION A(5,3),PHI(5,3),M(5,3)
  DATA IMAX,AE/4,-1./
  DATA (A(I,1),I=1,5)/1.,.9.,.12.,.26.,0./
  DATA (A(I,2),I=1,5)/1.,.9.,.12.,.26.,0./
  DATA (A(I,3),I=1,5)/1.,.9.,.12.,.26.,0./
  IF(TFUGGT.0160-10.12)
    ZC=0.
  M=5.28*11.
  DO 1 I=1,IMAX
    CALL KANNU(CO.,RNSTR,RN)
    PHI(I,K)=3.14*RN
    M(I,K)=I*M
  10  CONTINUE
  15  C ZC IS INTEGRATION CONSTANT FOR Z
    B=M(I,K)*T*PHI(I,K)
    ZC=ZC+A(I,K)*(AE*SIN(B)-M(I,K)*COS(B))/(AE**2+M(I,K)**2)
    1  CONTINUE
    YC=AMP*EXP(AE*T)*ZC
  17  CONTINUE
    Z=0.
    DO 2 I=1,IMAX
      Z=Z+A(I,K)*SIN(M(I,K)*T*PHI(I,K))
    2  CONTINUE
    Y=AMP*EXP(AE*T)*Z
  25  RETURN
  END

```

ENTRY POINTS	DEF LINE	REFERENCES
1	1	1
2	2	2
3	3	3
4	4	4
5	5	5
6	6	6
7	7	7
8	8	8
9	9	9
10	10	10
11	11	11
12	12	12
13	13	13
14	14	14
15	15	15
16	16	16
17	17	17
18	18	18
19	19	19
20	20	20
21	21	21
22	22	22
23	23	23
24	24	24
25	25	25
26	26	26
27	27	27
28	28	28
29	29	29
30	30	30
31	31	31
32	32	32
33	33	33
34	34	34
35	35	35
36	36	36
37	37	37
38	38	38
39	39	39
40	40	40
41	41	41
42	42	42
43	43	43
44	44	44
45	45	45
46	46	46
47	47	47
48	48	48
49	49	49
50	50	50
51	51	51
52	52	52
53	53	53
54	54	54
55	55	55
56	56	56
57	57	57
58	58	58
59	59	59
60	60	60
61	61	61
62	62	62
63	63	63
64	64	64
65	65	65
66	66	66
67	67	67
68	68	68
69	69	69
70	70	70
71	71	71
72	72	72
73	73	73
74	74	74
75	75	75
76	76	76
77	77	77
78	78	78
79	79	79
80	80	80
81	81	81
82	82	82
83	83	83
84	84	84
85	85	85
86	86	86
87	87	87
88	88	88
89	89	89
90	90	90
91	91	91
92	92	92
93	93	93
94	94	94
95	95	95
96	96	96
97	97	97
98	98	98
99	99	99
100	100	100

ENTRY POINTS	DEF LINE	REFERENCES
J LIRAN	I	ZS
VARIABLES	SN TYPE	RELOCATION
110 A	REAL	ARRY
101 A2	REAL	REFS 2+15
100 AM	REAL	REFS 18
114 B	REAL	F.P.
0 DELT	REAL	REFS 2+16
111 I	INT-GER	*UNUSED
0 IFLS	INTEGER	DEFINED 1
100 IMAX	INTEGER	REFS 7
0 K	INTEGER	F.P.
115 PHI	REAL	ARRY
113 RW	REAL	REFS 11
112 RNRSTR	REAL	REFS 11
0 T	REAL	F.P.
154 M	REAL	ARRY
110 H	REAL	REFS 13
0 Y	REAL	DEFINED 1
0 ZC	REAL	F.P.
115 Z	REAL	REFS 22
107 ZC	REAL	REFS 16
EXTERNALS	TYPE	ARGS REFERENCES
CUS	REAL	1 LIBRARY 16
KRL	REAL	1 LIBRARY 18
RANNUM	SIN	3 11
SIN	REAL	1 LIBRARY 16
STATEMENT LABELS	DEF LINE	REFERENCES
0 1	17	10
0 2	23	21
47 17	19	7
LJDS LABEL	INDEX	FROM-TO LENGTH PROPERTIES EXT REFS
12 1	*	18 17 300
51 2	*	21 23 153
51 2	*	21 23 153

SURROUTINE D11		TRANSLATIONAL DYNAMICS INITIALIZATION MODULE FOR D1		COMMON /C/ C(383)		EQUIVALENCE (C(2561),N)		EQUIVALENCE (C(2562),IPL)		DIMENSION IPL(100), ISMOX(40), ITNOX(10)		EQUIVALENCE (C(1363), ISMOX, C(1391), ITNOX)		C		C** INPUT DATA		EQUIVALENCE (C(1001),MKE)		EQUIVALENCE (C(1011),MKE)		EQUIVALENCE (C(1021),MZE)		EQUIVALENCE (C(1031),MZE)		EQUIVALENCE (C(1041),MZE)		EQUIVALENCE (C(1051),MZE)		EQUIVALENCE (C(1061),MZE)		EQUIVALENCE (C(1071),MZE)		EQUIVALENCE (C(1081),MZE)		EQUIVALENCE (C(1091),MZE)		EQUIVALENCE (C(1101),MZE)		EQUIVALENCE (C(1111),MZE)		EQUIVALENCE (C(1121),MZE)		EQUIVALENCE (C(1131),MZE)		EQUIVALENCE (C(1141),MZE)		EQUIVALENCE (C(1151),MZE)		EQUIVALENCE (C(1161),MZE)		EQUIVALENCE (C(1171),MZE)		EQUIVALENCE (C(1181),MZE)		EQUIVALENCE (C(1191),MZE)		EQUIVALENCE (C(1201),MZE)		EQUIVALENCE (C(1211),MZE)		EQUIVALENCE (C(1221),MZE)		EQUIVALENCE (C(1231),MZE)		EQUIVALENCE (C(1241),MZE)		EQUIVALENCE (C(1251),MZE)		EQUIVALENCE (C(1261),MZE)		EQUIVALENCE (C(1271),MZE)		EQUIVALENCE (C(1281),MZE)		EQUIVALENCE (C(1291),MZE)		EQUIVALENCE (C(1301),MZE)		EQUIVALENCE (C(1311),MZE)		EQUIVALENCE (C(1321),MZE)		EQUIVALENCE (C(1331),MZE)		EQUIVALENCE (C(1341),MZE)		EQUIVALENCE (C(1351),MZE)		EQUIVALENCE (C(1361),MZE)		EQUIVALENCE (C(1371),MZE)		EQUIVALENCE (C(1381),MZE)		EQUIVALENCE (C(1391),MZE)		EQUIVALENCE (C(1401),MZE)		EQUIVALENCE (C(1411),MZE)		EQUIVALENCE (C(1421),MZE)		EQUIVALENCE (C(1431),MZE)		EQUIVALENCE (C(1441),MZE)		EQUIVALENCE (C(1451),MZE)		EQUIVALENCE (C(1461),MZE)		EQUIVALENCE (C(1471),MZE)		EQUIVALENCE (C(1481),MZE)		EQUIVALENCE (C(1491),MZE)		EQUIVALENCE (C(1501),MZE)		EQUIVALENCE (C(1511),MZE)		EQUIVALENCE (C(1521),MZE)		EQUIVALENCE (C(1531),MZE)		EQUIVALENCE (C(1541),MZE)		EQUIVALENCE (C(1551),MZE)		EQUIVALENCE (C(1561),MZE)		EQUIVALENCE (C(1571),MZE)		EQUIVALENCE (C(1581),MZE)		EQUIVALENCE (C(1591),MZE)		EQUIVALENCE (C(1601),MZE)		EQUIVALENCE (C(1611),MZE)		EQUIVALENCE (C(1621),MZE)		EQUIVALENCE (C(1631),MZE)		EQUIVALENCE (C(1641),MZE)		EQUIVALENCE (C(1651),MZE)		EQUIVALENCE (C(1661),MZE)		EQUIVALENCE (C(1671),MZE)		EQUIVALENCE (C(1681),MZE)		EQUIVALENCE (C(1691),MZE)		EQUIVALENCE (C(1701),MZE)		EQUIVALENCE (C(1711),MZE)		EQUIVALENCE (C(1721),MZE)		EQUIVALENCE (C(1731),MZE)		EQUIVALENCE (C(1741),MZE)		EQUIVALENCE (C(1751),MZE)		EQUIVALENCE (C(1761),MZE)		EQUIVALENCE (C(1771),MZE)		EQUIVALENCE (C(1781),MZE)		EQUIVALENCE (C(1791),MZE)		EQUIVALENCE (C(1801),MZE)		EQUIVALENCE (C(1811),MZE)		EQUIVALENCE (C(1821),MZE)		EQUIVALENCE (C(1831),MZE)		EQUIVALENCE (C(1841),MZE)		EQUIVALENCE (C(1851),MZE)		EQUIVALENCE (C(1861),MZE)		EQUIVALENCE (C(1871),MZE)		EQUIVALENCE (C(1881),MZE)		EQUIVALENCE (C(1891),MZE)		EQUIVALENCE (C(1901),MZE)		EQUIVALENCE (C(1911),MZE)		EQUIVALENCE (C(1921),MZE)		EQUIVALENCE (C(1931),MZE)		EQUIVALENCE (C(1941),MZE)		EQUIVALENCE (C(1951),MZE)		EQUIVALENCE (C(1961),MZE)		EQUIVALENCE (C(1971),MZE)		EQUIVALENCE (C(1981),MZE)		EQUIVALENCE (C(1991),MZE)		EQUIVALENCE (C(2001),MZE)		EQUIVALENCE (C(2011),MZE)		EQUIVALENCE (C(2021),MZE)		EQUIVALENCE (C(2031),MZE)		EQUIVALENCE (C(2041),MZE)		EQUIVALENCE (C(2051),MZE)		EQUIVALENCE (C(2061),MZE)		EQUIVALENCE (C(2071),MZE)		EQUIVALENCE (C(2081),MZE)		EQUIVALENCE (C(2091),MZE)		EQUIVALENCE (C(2101),MZE)		EQUIVALENCE (C(2111),MZE)		EQUIVALENCE (C(2121),MZE)		EQUIVALENCE (C(2131),MZE)		EQUIVALENCE (C(2141),MZE)		EQUIVALENCE (C(2151),MZE)		EQUIVALENCE (C(2161),MZE)		EQUIVALENCE (C(2171),MZE)		EQUIVALENCE (C(2181),MZE)		EQUIVALENCE (C(2191),MZE)		EQUIVALENCE (C(2201),MZE)		EQUIVALENCE (C(2211),MZE)		EQUIVALENCE (C(2221),MZE)		EQUIVALENCE (C(2231),MZE)		EQUIVALENCE (C(2241),MZE)		EQUIVALENCE (C(2251),MZE)		EQUIVALENCE (C(2261),MZE)		EQUIVALENCE (C(2271),MZE)		EQUIVALENCE (C(2281),MZE)		EQUIVALENCE (C(2291),MZE)		EQUIVALENCE (C(2301),MZE)		EQUIVALENCE (C(2311),MZE)		EQUIVALENCE (C(2321),MZE)		EQUIVALENCE (C(2331),MZE)		EQUIVALENCE (C(2341),MZE)		EQUIVALENCE (C(2351),MZE)		EQUIVALENCE (C(2361),MZE)		EQUIVALENCE (C(2371),MZE)		EQUIVALENCE (C(2381),MZE)		EQUIVALENCE (C(2391),MZE)		EQUIVALENCE (C(2401),MZE)		EQUIVALENCE (C(2411),MZE)		EQUIVALENCE (C(2421),MZE)		EQUIVALENCE (C(2431),MZE)		EQUIVALENCE (C(2441),MZE)		EQUIVALENCE (C(2451),MZE)		EQUIVALENCE (C(2461),MZE)		EQUIVALENCE (C(2471),MZE)		EQUIVALENCE (C(2481),MZE)		EQUIVALENCE (C(2491),MZE)		EQUIVALENCE (C(2501),MZE)		EQUIVALENCE (C(2511),MZE)		EQUIVALENCE (C(2521),MZE)		EQUIVALENCE (C(2531),MZE)		EQUIVALENCE (C(2541),MZE)		EQUIVALENCE (C(2551),MZE)		EQUIVALENCE (C(2561),MZE)		EQUIVALENCE (C(2571),MZE)		EQUIVALENCE (C(2581),MZE)		EQUIVALENCE (C(2591),MZE)		EQUIVALENCE (C(2601),MZE)		EQUIVALENCE (C(2611),MZE)		EQUIVALENCE (C(2621),MZE)		EQUIVALENCE (C(2631),MZE)		EQUIVALENCE (C(2641),MZE)		EQUIVALENCE (C(2651),MZE)		EQUIVALENCE (C(2661),MZE)		EQUIVALENCE (C(2671),MZE)		EQUIVALENCE (C(2681),MZE)		EQUIVALENCE (C(2691),MZE)		EQUIVALENCE (C(2701),MZE)		EQUIVALENCE (C(2711),MZE)		EQUIVALENCE (C(2721),MZE)		EQUIVALENCE (C(2731),MZE)		EQUIVALENCE (C(2741),MZE)		EQUIVALENCE (C(2751),MZE)		EQUIVALENCE (C(2761),MZE)		EQUIVALENCE (C(2771),MZE)		EQUIVALENCE (C(2781),MZE)		EQUIVALENCE (C(2791),MZE)		EQUIVALENCE (C(2801),MZE)		EQUIVALENCE (C(2811),MZE)		EQUIVALENCE (C(2821),MZE)		EQUIVALENCE (C(2831),MZE)		EQUIVALENCE (C(2841),MZE)		EQUIVALENCE (C(2851),MZE)		EQUIVALENCE (C(2861),MZE)		EQUIVALENCE (C(2871),MZE)		EQUIVALENCE (C(2881),MZE)		EQUIVALENCE (C(2891),MZE)		EQUIVALENCE (C(2901),MZE)		EQUIVALENCE (C(2911),MZE)		EQUIVALENCE (C(2921),MZE)		EQUIVALENCE (C(2931),MZE)		EQUIVALENCE (C(2941),MZE)		EQUIVALENCE (C(2951),MZE)		EQUIVALENCE (C(2961),MZE)		EQUIVALENCE (C(2971),MZE)		EQUIVALENCE (C(2981),MZE)		EQUIVALENCE (C(2991),MZE)		EQUIVALENCE (C(3001),MZE)		EQUIVALENCE (C(3011),MZE)		EQUIVALENCE (C(3021),MZE)		EQUIVALENCE (C(3031),MZE)		EQUIVALENCE (C(3041),MZE)		EQUIVALENCE (C(3051),MZE)		EQUIVALENCE (C(3061),MZE)		EQUIVALENCE (C(3071),MZE)		EQUIVALENCE (C(3081),MZE)		EQUIVALENCE (C(3091),MZE)		EQUIVALENCE (C(3101),MZE)		EQUIVALENCE (C(3111),MZE)		EQUIVALENCE (C(3121),MZE)		EQUIVALENCE (C(3131),MZE)		EQUIVALENCE (C(3141),MZE)		EQUIVALENCE (C(3151),MZE)		EQUIVALENCE (C(3161),MZE)		EQUIVALENCE (C(3171),MZE)		EQUIVALENCE (C(3181),MZE)		EQUIVALENCE (C(3191),MZE)		EQUIVALENCE (C(3201),MZE)		EQUIVALENCE (C(3211),MZE)		EQUIVALENCE (C(3221),MZE)		EQUIVALENCE (C(3231),MZE)		EQUIVALENCE (C(3241),MZE)		EQUIVALENCE (C(3251),MZE)		EQUIVALENCE (C(3261),MZE)		EQUIVALENCE (C(3271),MZE)		EQUIVALENCE (C(3281),MZE)		EQUIVALENCE (C(3291),MZE)		EQUIVALENCE (C(3301),MZE)		EQUIVALENCE (C(3311),MZE)		EQUIVALENCE (C(3321),MZE)		EQUIVALENCE (C(3331),MZE)		EQUIVALENCE (C(3341),MZE)		EQUIVALENCE (C(3351),MZE)		EQUIVALENCE (C(3361),MZE)		EQUIVALENCE (C(3371),MZE)		EQUIVALENCE (C(3381),MZE)		EQUIVALENCE (C(3391),MZE)		EQUIVALENCE (C(3401),MZE)		EQUIVALENCE (C(3411),MZE)		EQUIVALENCE (C(3421),MZE)		EQUIVALENCE (C(3431),MZE)		EQUIVALENCE (C(3441),MZE)		EQUIVALENCE (C(3451),MZE)		EQUIVALENCE (C(3461),MZE)		EQUIVALENCE (C(3471),MZE)		EQUIVALENCE (C(3481),MZE)		EQUIVALENCE (C(3491),MZE)		EQUIVALENCE (C(3501),MZE)		EQUIVALENCE (C(3511),MZE)		EQUIVALENCE (C(3521),MZE)		EQUIVALENCE (C(3531),MZE)		EQUIVALENCE (C(3541),MZE)		EQUIVALENCE (C(3551),MZE)		EQUIVALENCE (C(3561),MZE)		EQUIVALENCE (C(3571),MZE)		EQUIVALENCE (C(3581),MZE)		EQUIVALENCE (C(3591),MZE)		EQUIVALENCE (C(3601),MZE)		EQUIVALENCE (C(3611),MZE)		EQUIVALENCE (C(3621),MZE)		EQUIVALENCE (C(3631),MZE)		EQUIVALENCE (C(3641),MZE)		EQUIVALENCE (C(3651),MZE)		EQUIVALENCE (C(3661),MZE)		EQUIVALENCE (C(3671),MZE)		EQUIVALENCE (C(3681),MZE)		EQUIVALENCE (C(3691),MZE)		EQUIVALENCE (C(3701),MZE)		EQUIVALENCE (C(3711),MZE)		EQUIVALENCE (C(3721),MZE)		EQUIVALENCE (C(3731),MZE)		EQUIVALENCE (C(3741),MZE)		EQUIVALENCE (C(3751),MZE)		EQUIVALENCE (C(3761),MZE)		EQUIVALENCE (C(3771),MZE)		EQUIVALENCE (C(3781),MZE)		EQUIVALENCE (C(3791),MZE)		EQUIVALENCE (C(3801),MZE)		EQUIVALENCE (C(3811),MZE)		EQUIVALENCE (C(3821),MZE)		EQUIVALENCE (C(3831),MZE)		EQUIVALENCE (C(3841),MZE)		EQUIVALENCE (C(3851),MZE)		EQUIVALENCE (C(3861),MZE)		EQUIVALENCE (C(3871),MZE)		EQUIVALENCE (C(3881),MZE)		EQUIVALENCE (C(3891),MZE)		EQUIVALENCE (C(3901),MZE)		EQUIVALENCE (C(3911),MZE)		EQUIVALENCE (C(3921),MZE)		EQUIVALENCE (C(3931),MZE)		EQUIVALENCE (C(3941),MZE)		EQUIVALENCE (C(3951),MZE)		EQUIVALENCE (C(3961),MZE)		EQUIVALENCE (C(3971),MZE)		EQUIVALENCE (C(3981),MZE)		EQUIVALENCE (C(3991),MZE)		EQUIVALENCE (C(4001),MZE)		EQUIVALENCE (C(4011),MZE)		EQUIVALENCE (C(4021),MZE)		EQUIVALENCE (C(4031),MZE)		EQUIVALENCE (C(4041),MZE)		EQUIVALENCE (C(4051),MZE)		EQUIVALENCE (C(4061),MZE)		EQUIVALENCE (C(4071),MZE)		EQUIVALENCE (C(4081),MZE)		EQUIVALENCE (C(4091),MZE)		EQUIVALENCE (C(4101),MZE)		EQUIVALENCE (C(4111),MZE)		EQUIVALENCE (C(4121),MZE)		EQUIVALENCE (C(4131),MZE)		EQUIVALENCE (C(4141),MZE)		EQUIVALENCE (C(4151),MZE)		EQUIVALENCE (C(4161),MZE)		EQUIVALENCE (C(4171),MZE)		EQUIVALENCE (C(4181),MZE)		EQUIVALENCE (C(4191),MZE)		EQUIVALENCE (C(4201),MZE)		EQUIVALENCE (C(4211),MZE)		EQUIVALENCE (C(4221),MZE)		EQUIVALENCE (C(4231),MZE)		EQUIVALENCE (C(4241),MZE)		EQUIVALENCE (C(4251),MZE)		EQUIVALENCE (C(4261),MZE)		EQUIVALENCE (C(4271),MZE)		EQUIVALENCE (C(4281),MZE)		EQUIVALENCE (C(4291),MZE)		EQUIVALENCE (C(4301),MZE)		EQUIVALENCE (C(4311),MZE)		EQUIVALENCE (C(4321),MZE)		EQUIVALENCE (C(4331),MZE)		EQUIVALENCE (C(4341),MZE)		EQUIVALENCE (C(4351),MZE)		EQUIVALENCE (C(4361),MZE)		EQUIVALENCE (C(4371),MZE)		EQUIVALENCE (C(4381),MZE)		EQUIVALENCE (C(4391),MZE)		EQUIVALENCE (C(4401),MZE)		EQUIVALENCE (C(4411),MZE)		EQUIVALENCE (C(4421),MZE)		EQUIVALENCE (C(4431),MZE)		EQUIVALENCE (C(4441),MZE)		EQUIVALENCE (C(4451),MZE)		EQUIVALENCE (C(4461),MZE)		EQUIVALENCE (C(4471),MZE)		EQUIVALENCE (C(4481),MZE)		EQUIVALENCE (C(4491),MZE)		EQUIVALENCE (C(4501),MZE)		EQUIVALENCE (C(4511),MZE)		EQUIVALENCE (C(4521),MZE)		EQUIVALENCE (C(4531),MZE)		EQUIVALENCE (C(4541),MZE)		EQUIVALENCE (C(4551),MZE)		EQUIVALENCE (C(4561),MZE)		EQUIVALENCE (C(4571),MZE)		EQUIVALENCE (C(4581),MZE)		EQUIVALENCE (C(4591),MZE)		EQUIVALENCE (C(4601),MZE)		EQUIVALENCE (C(4611),MZE)		EQUIVALENCE (C(4621),MZE)		EQUIVALENCE (C(4631),MZE)		EQUIVALENCE (C(4641),MZE)		EQUIVALENCE (C(4651),MZE)		EQUIVALENCE (C(4661),MZE)		EQUIVALENCE (C(4671),MZE)		EQUIVALENCE (C(4681),MZE)		EQUIVALENCE (C(4691),MZE)		EQUIVALENCE (C(4701),MZE)		EQUIVALENCE (C(4711),MZE)		EQUIVALENCE (C(4721),MZE)		EQUIVALENCE (C(4731),MZE)		EQUIVALENCE (C(4741),MZE)		EQUIVALENCE (C(4751),MZE)		EQUIVALENCE (C(4761),MZE)		EQUIVALENCE (C(4771),MZE)		EQUIVALENCE (C(4781),MZE)		EQUIVALENCE (C(4791),MZE)		EQUIVALENCE (C(4801),MZE)		EQUIVALENCE (C(4811),MZE)		EQUIVALENCE (C(4821),MZE)		EQUIVALENCE (C(4831),MZE)		EQUIVALENCE (C(4841),MZE)		EQUIVALENCE (C(4851),MZE)		EQUIVALENCE (C(4861),MZE)		EQUIVALENCE (C(4871),MZE)		EQUIVALENCE (C(4881),MZE)		EQUIVALENCE (C(4891),MZE)		EQUIVALENCE (C(4901),MZE)		EQUIVALENCE (C(4911),MZE)		EQUIVALENCE (C(4921),MZE)		EQUIVALENCE (C(4931),MZE)		EQUIVALENCE (C(4941),MZE)		EQUIVALENCE (C(4951),MZE)		EQUIVALENCE (C(4961),MZE)		EQUIVALENCE (C(4971),MZE)		EQUIVALENCE (C(4981),MZE)		EQUIVALENCE (C(4991),MZE)		EQUIVALENCE (C(5001),MZE)		EQUIVALENCE (C(5011),MZE)		EQUIVALENCE (C(5021),MZE)		EQUIVALENCE (C(5031),MZE)		EQUIVALENCE (C(5041),MZE)		EQUIVALENCE (C(5051),MZE)		EQUIVALENCE (C(5061),MZE)		EQUIVALENCE (C(5071),MZE)		EQUIVALENCE (C(5081),MZE)		EQUIVALENCE (C(5091),MZE)		EQUIVALENCE (C(5101),MZE)		EQUIVALENCE (C(5111),MZE)		EQUIVALENCE (C(5121),MZE)		EQUIVALENCE (C(5131),MZE)		EQUIVALENCE (C(5141),MZE)		EQUIVALENCE (C(5151),MZE)		EQUIVALENCE (C(5161),MZE)		EQUIVALENCE (C(5171),MZE)		EQUIVALENCE (C(5181),MZE)		EQUIVALENCE (C(5191),MZE)		EQUIVALENCE (C(5201),MZE)		EQUIVALENCE (C(5211),MZE)		EQUIVALENCE (C(5221),MZE)		EQUIVALENCE (C(5231),MZE)		EQUIVALENCE (C(5241),MZE)		EQUIVALENCE (C(5251),MZE)		EQUIVALENCE (C(5261),MZE)		EQUIVALENCE (C(5271),MZE)		EQUIVALENCE (C(5281),MZE)		EQUIVALENCE (C(5291),MZE)		EQUIVALENCE (C(5301),MZE)		EQUIVALENCE (C(5311),MZE)		EQUIVALENCE (C(5321),MZE)		EQUIVALENCE (C(5331),MZE)		EQUIVALENCE (C(5341),MZE)		EQUIVALENCE (C(5351),MZE)		EQUIVALENCE (C(5361),MZE)		EQUIVALENCE (C(5371),MZE)		EQUIVALENCE (C(5381),MZE)		EQUIVALENCE (C(5391),MZE)		EQUIVALENCE (C(5401),MZE)		EQUIVALENCE (C(5411),MZE)		EQUIVALENCE (C(5421),MZE)		EQUIVALENCE (C(5431),MZE)		EQUIVALENCE (C(5441),MZE)		EQUIVALENCE (C(5451),MZE)		EQUIVALENCE (C(5461),MZE)		EQUIVALENCE (C(5471),MZE)		EQUIVALENCE (C(5481),MZE)		EQUIVALENCE (C(5491),MZE)		EQUIVALENCE (C(5501),MZE)		EQUIVALENCE (C(5511),MZE)		EQUIVALENCE (C(5521),MZE)		EQUIVALENCE (C(5531),MZE)		EQUIVALENCE (C(5541),MZE)		EQUIVALENCE (C(5551),MZE)		EQUIVALENCE (C(5561),MZE)		EQUIVALENCE (C(5571),MZE)		EQUIVALENCE (C(5581),MZE)		EQUIVALENCE (C(5591),MZE)		EQUIVALENCE (C(5601),MZE)		EQUIVALENCE (C(5611),MZE)		EQUIVALENCE (C(5621),MZE)		EQUIVALENCE (C(5631),MZE)		EQUIVALENCE (C(5641),MZE)		EQUIVALENCE (C(5651),MZE)		EQUIVALENCE (C(5661),MZE)		EQUIVALENCE (C(5671),MZE)		EQUIVALENCE (C(5681),MZE)		EQUIVALENCE (C(5691),MZE)		EQUIVALENCE (C(5701),MZE)		EQUIVALENCE (C(5711),MZE)		EQUIVALENCE (C(5721),MZE)		EQUIVALENCE (C(5731),MZE)		EQUIVALENCE (C(5741),MZE)		EQUIVALENCE (C(5751),MZE)		EQUIVALENCE (C(5761),MZE)		EQUIVALENCE (C(5771),MZE)		EQUIVALENCE (C(5781),MZE)		EQUIVALENCE (C(5791),MZE)		EQUIVALENCE (C(5801),MZE)		EQUIVALENCE (C(5811),MZE)		EQUIVALENCE (C(5821),MZE)		EQUIVALENCE (C(5831),MZE)		EQUIVALENCE (C(5841),MZE)		EQUIVALENCE (C(5851),MZE)		EQUIVALENCE (C(5861),MZE)		EQUIVALENCE (C(5871),MZE)		EQUIVALENCE (C(5881),MZE)		EQUIVALENCE (C(5891),MZE)		EQUIVALENCE (C(5901),MZE)		EQUIVALENCE (C(5911),MZE)		EQUIVALENCE (C(5921),MZE)		EQUIVALENCE (C(5931),MZE)		EQUIVALENCE (C(5941),MZE)		EQUIVALENCE (C(5951),MZE)		EQUIVALENCE (C(5961),MZE)		EQUIVALENCE (C(5971),MZE)		EQUIVALENCE (C(5981),MZE)		EQUIVALENCE (C(5991),MZE)		EQUIVALENCE (C(6001),MZE)		EQUIVALENCE (C(6011),MZE)		EQUIVALENCE (C(6021),MZE)		EQUIVALENCE (C(6031),MZE)		EQUIVALENCE (C(6041),MZE)		EQUIVALENCE (C(6051),MZE)		EQUIVALENCE (C(6061),MZE)		EQUIVALENCE (C(6071),MZE)	
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SUBROUTINE 011		74/74	OPT=1	FTN 6.2+7A.355	07/07/75	11.06.08.	PAGE	5
230	YEO = YZE				01	241		
	ROELX = RTXE - RKE				01	242		
	ROELY = RTYE - RYE				01	243		
	ROELZ = RTZE - RZE				01	244		
	RETURN				01	245		
	END				01	246		

SUBROUTINE D11		7474	OPT=1	FTN ++27.335	07/07/75	11.06.09.	PAGE
CARD NR. SEVERITY DETAILS		DIAGNOSIS OF PROBLEM					6
96	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				
97	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				
103	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				
104	I	ITCI	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				

SYMBOLIC REFERENCE MAP (N=3)

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1 011 127

VARIABLES SN TYPE RELOCATION

3340 A011	REAL	C	53	DEFINED	160	
3341 A012	REAL	C	54	DEFINED	169	
3342 A013	REAL	C	55	DEFINED	170	
3332 A021	REAL	C	56	DEFINED	171	
3333 A022	REAL	C	57	DEFINED	172	
3334 A023	REAL	C	58	DEFINED	173	
3335 A031	REAL	C	59	DEFINED	174	
3336 A032	REAL	C	60	DEFINED	175	
3337 A033	REAL	C	61	DEFINED	176	
550 BALPHA	REAL	C	14	213	222	
557 BALPHY	REAL	C	15	220	221	
4201 BLOSV	REAL	C	19	193	130	
3327 BP410	REAL	C	83	182	193	207
547 BP412R	REAL	C	70	162	163	DEFINED 152
656 BPSIG	REAL	C	17	186	DEFINED 213	
3331 BPSIO	REAL	C	45	166	167	204
			221	DEFINED	186	
551 BPSIER	REAL	C	72	169	167	DEFINED 159
652 BT4TG	REAL	C	16	2+136	DEFINED 212	
3330 BTMTO	REAL	C	44	184	165	203
			DEFINED	189		222
550 BTMZER	REAL	C	71	REFS	71	
0 C	ARRAY	C	3	4	5	2+7
			13	15	16	18
			21	22	23	19
			31	32	33	25
			39	40	41	28
			47	48	49	30
			55	56	57	44
			63	64	65	51
			71	72	73	2+52
			106	DEFINED	107	61
			REFS	2+199	DEFINED	62
			REFS	22	186	69
			REFS	145	156	70
			REFS	73	DEFINED	71
			REFS	74	DEFINED	72
			REFS	144	145	73
			REFS	183	185	74
			REFS	145	146	155
			DEFINED	144	155	143
			REFS	94	95	156
			REFS	5	5	157
			REFS	111	112	DEFINED 98
			REFS	119	120	96
			REFS	121	121	97
			REFS	6	7	115
			REFS	184	185	114
			REFS	52	53	145
			REFS	6	6	152
			REFS	101	108	DEFINED 94
513 CPSIO	REAL	C				
3326 CX4D	REAL	C				
503 D04	REAL	C				
3031 GSPOTY	REAL	C				
3043 GSPOTZ	REAL	C				
501 I	INTEGER	C				
502 I03	INTEGER	C				
476 I0L	INTEGER	C				
3004 IPL	INTEGER	C				
7061 ISNDX	INTEGER	C				
7210 I73T	INTEGER	C				
7250 ITNDX	INTEGER	C				
477 ITSN0X	INTEGER	C				

SUBROUTINE D11			74/74	OPT=1	FTN 4.2+74.355			07/07/75	11.06.08.	PAGE	8
VARIABLES	SN	TYPE	RELOCATION								
3007 13912	INT-GER		C								
3000 N											
1146 UPTARG	REAL		C		193	194	195	101	103	104	105
3055 OPTNE	REAL		C		111	112	113	98	115	116	117
3057 OPTN4	REAL		C		119	120	121	122	128	129	130
3061 OPTN6	REAL		C		122	123	124	125	131	132	133
3143 P1	REAL		C		125	126	127	128	134	135	136
3142 RDELX	REAL		C		128	129	130	131	137	138	139
3143 RDELY	REAL		C		131	132	133	134	141	142	143
3144 RDELZ	REAL		C		134	135	136	137	147	148	149
312 RM	REAL		C		137	138	139	140	153	154	155
3208 KMPRO	REAL		C		140	141	142	143	161	162	163
3209 RNSRT	REAL		C		143	144	145	146	169	170	171
3217 R3JMC	REAL		C		146	147	148	149	172	173	174
3220 R3JMC	REAL		C		149	150	151	152	175	176	177
3162 K1RE	REAL		C		151	152	153	154	181	182	183
3166 K1YE	REAL		C		153	154	155	156	184	185	186
3172 K1ZE	REAL		C		156	157	158	159	187	188	189
323 K13A	REAL		C		159	160	161	162	191	192	193
3116 K1E	REAL		C		162	163	164	165	194	195	196
3203 K1J	REAL		C		165	166	167	168	197	198	199
324 K13A	REAL		C		168	169	170	171	201	202	203
3122 K1E	REAL		C		171	172	173	174	204	205	206
3204 K1D	REAL		C		174	175	176	177	207	208	209
325 K13A	REAL		C		177	178	179	180	210	211	212
3126 K1E	REAL		C		180	181	182	183	212	213	214
3205 K1J	REAL		C		183	184	185	186	214	215	216
314 K1	REAL		C		186	187	188	189	216	217	218
3054 S13POT	REAL		C		189	190	191	192	218	219	220
314 T1ATG	REAL		C		192	193	194	195	220	221	222
317 UC9	REAL		C		195	196	197	198	222	223	224
321 UC9H	REAL		C		198	199	200	201	224	225	226
305 UC9H11	REAL		C		201	202	203	204	226	227	228
311 UC9S11	REAL		C		204	205	206	207	228	229	230
320 UGT	REAL		C		207	208	209	210	230	231	232
307 UGT12	REAL		C		210	211	212	213	232	233	234
316 USP	REAL		C		213	214	215	216	234	235	236
322 USP4	REAL		C		216	217	218	219	236	237	238
304 USP11	REAL		C		219	220	221	222	238	239	240
310 US9S11	REAL		C		222	223	224	225	240	241	242
315 U3T	REAL		C		225	226	227	228	242	243	244
306 U3T12	REAL		C		228	229	230	231	244	245	246
313 VM1CM	REAL		C		231	232	233	234	246	247	248
321 VM1F1	REAL		C		234	235	236	237	248	249	250
327 VM1XY	REAL		C		237	238	239	240	250	251	252
326 V5OUND	REAL		C		240	241	242	243	252	253	254

VARIABLES	SN	TYPE	RELOCATION	REFS	10	220
143 VMXE	REAL	C		REFS	11	221
144 VMZE	REAL	C		REFS	12	222
145 VMZE	REAL	C		REFS	31	227
146 VMZE	REAL	C		REFS	40	DEFINED 228
147 VMZE	REAL	C		REFS	32	DEFINED 227
148 VMZE	REAL	C		REFS	32	DEFINED 221
149 VMZE	REAL	C		REFS	31	DEFINED 220
150 VMZE	REAL	C		REFS	31	DEFINED 222
151 VMZE	REAL	C		REFS	42	DEFINED 229
152 VMZE	REAL	C		REFS	77	DEFINED 106
153 VMZE	REAL	C		REFS	64	DEFINED 136
154 VMZE	REAL	C		REFS	67	DEFINED 137
155 VMZE	REAL	C		REFS	65	DEFINED 138
156 VMZE	REAL	C		REFS	66	DEFINED 139
157 VMZE	REAL	C		REFS	69	DEFINED 140
158 VMZE	REAL	C		REFS	76	DEFINED 141

EXTENSIVE	TYPE	REFS	REFERENCES
ASIN	REAL	1	LIBRARY 196
ATANU	REAL	2	LIBRARY 199
COSD	REAL	1	LIBRARY 163
MCARLO	REAL	3	LIBRARY 213
SILO	REAL	1	LIBRARY 101
SORT	REAL	1	LIBRARY 213

STATEMENT LABELS	DEF LINE	REFERENCES
0 5	136	191
243 10	137	190
0 11	138	154
247 20	139	191
0 24	216	
270 30	201	195
351 40	214	200
51 200	189	93
31 202	102	95
0 503	147	143

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
11 500	* IOL	93 109	438	EXT REFS
114 503	* I	143 147	148	EXT REFS
132 11	* I	154 158	148	EXT REFS
213 5	* I	181 186	208	EXT REFS

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)

ELIUV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)
131 VMZE	(1)	131 VMZE (1)
350 BTMZE	(1)	350 BTMZE (1)
357 BALPMA	(1)	357 BALPMA (1)
151 GSPOTV	(1)	151 GSPOTV (1)
1579 M0	(1)	1579 M0 (1)
1575 VYE	(1)	1575 VYE (1)
1618 RYE	(1)	1618 RYE (1)

SUBROUTINE D11			74/74	OPT=1	FTN ++2+74355		07/07/73	11.06.08.	PAGE	10
EQUIV CLASSES		LENGTH	MEMBERS - BIAS NAME(LENGTH)							
			1622 R2E (11)	1634 R0ELX (11)	1635 R0ELT (11)					
			1636 R0ELZ (11)	1638 OPTARG (11)	1639 RTXE (11)					
			1639 RTVE (11)	1650 RTZE (11)	1654 R0ZRO (11)					
			1665 RLOSV (11)	1666 RSLANT (11)	1657 RXO (11)					
			1668 RVO (11)	1669 RZQ (11)	1670 RYO (11)					
			1671 RVO (11)	1672 RYO (11)	1673 RYIE (11)					
			1679 R5JYHC (11)	1680 R5JYHC (11)	1670 R0R0 (11)					
			1721 R0R10 (11)	1732 R0R10 (11)	1733 R0S10 (11)					
			1734 R0Z1 (11)	1735 R0Z2 (11)	1736 R0Z3 (11)					
			1757 R0J1 (11)	1758 R0J2 (11)	1759 R0J3 (11)					
			1760 R0J1 (11)	1761 R0J2 (11)	1762 R0J3 (11)					
			1763 R1 (11)	1764 R1 (11)	1757 R0J1 (11)					
			1768 R0J1 (11)	1769 R0J1 (11)	1770 R0J2 (11)					
			1771 R0J2 (11)	1772 R0J2 (11)	2550 N (11)					
			2561 IPL (1100)	3501 OPTNE (11)	3503 OPTM4 (11)					
			3205 OPTNG (11)	3511 R3512 (11)	3633 ISNDR (148)					
			3720 RYCT (11)	3752 RYNDK (110)						
STATISTICS										
PROGRAM LENGTH			5302	34.						
CM LABELED COMMON LENGTH			73668	3030						

SUBROUTINE 01	74/74	OPT=1	FIN +.247.355	07/0775	11.05.14.	PAGE	1
SUBROUTINE 01							247
C**TRANSLATIONAL DYNAMICS MODULE							248
COMMON /C/ C13838)							15
C							250
C**INPUT DATA							251
5	EQUIVALENCE (C(1627),ACRAV)						252
	EQUIVALENCE (C(1628),ACRAV)						253
	EQUIVALENCE (C(1629),ACRAV)						254
	EQUIVALENCE (C(1630),ACRAV)						255
10	EQUIVALENCE (C(1631),ACRAV)						256
	EQUIVALENCE (C(1632),ACRAV)						257
	EQUIVALENCE (C(1633),ACRAV)						258
	EQUIVALENCE (C(1634),ACRAV)						259
15	C**INPUTS FROM OTHER MODULES						260
	EQUIVALENCE (C(1300),FABA)						261
	EQUIVALENCE (C(1301),FABA)						262
	EQUIVALENCE (C(1302),FABA)						263
	EQUIVALENCE (C(1303),FABA)						264
20	EQUIVALENCE (C(1707),CFA12)						265
	EQUIVALENCE (C(1711),CFA12)						266
	EQUIVALENCE (C(1713),CFA12)						267
	EQUIVALENCE (C(1715),CFA21)						268
	EQUIVALENCE (C(1719),CFA21)						269
	EQUIVALENCE (C(1723),CFA21)						270
25	EQUIVALENCE (C(1727),CFA31)						271
	EQUIVALENCE (C(1731),CFA32)						272
	EQUIVALENCE (C(1735),CFA33)						273
	EQUIVALENCE (C(2000),T)						274
30	C**STATE VARIABLE OUTPUTS						275
	EQUIVALENCE (C(1500),VXED)						276
	EQUIVALENCE (C(1503),VXED)						277
	EQUIVALENCE (C(1504),VYED)						278
	EQUIVALENCE (C(1507),VYED)						279
35	EQUIVALENCE (C(1508),VZED)						280
	EQUIVALENCE (C(1511),VZED)						281
	EQUIVALENCE (C(1512),VZED)						282
	EQUIVALENCE (C(1515),VXE)						283
	EQUIVALENCE (C(1516),VYE)						284
40	EQUIVALENCE (C(1519),VYE)						285
	EQUIVALENCE (C(1520),VZE)						286
	EQUIVALENCE (C(1523),VZE)						287
	EQUIVALENCE (C(1524),VZE)						288
	EQUIVALENCE (C(1525),VZE)						289
45	EQUIVALENCE (C(1526),VZE)						290
	EQUIVALENCE (C(1527),VZE)						291
	EQUIVALENCE (C(1528),VZE)						292
	EQUIVALENCE (C(1529),VZE)						293
	EQUIVALENCE (C(1530),VZE)						294
50	EQUIVALENCE (C(1531),VZE)						295
	EQUIVALENCE (C(1532),VZE)						296
	EQUIVALENCE (C(1533),VZE)						297
	EQUIVALENCE (C(1534),VZE)						298
	EQUIVALENCE (C(1535),VZE)						299
55	C**OTHER OUTPUTS						300
	EQUIVALENCE (C(1624),ACRAV)						301
	EQUIVALENCE (C(1625),ACRAV)						302
	EQUIVALENCE (C(1626),ACRAV)						303

SUBROUTINE U1	P4/74	OPT=1	FTN 4.2474355	07/07/75	11.06.14.	PAGE
115				01	361	3
		RTYD = VTYE		01	362	
		RIZEL = VTZE		01	363	
	C			01	364	
		VDLX = VTXE-VXE		01	365	
		VDLY = VTYE-VYE		01	366	
120		VDLZ = VTZE-VZE		01	367	
	C			01	368	
		VCLSG = (VDLX*VDLX+VDLY*VDLY+VDLZ*VDLZ)/RANGE		01	369	
		RETURN		01	370	
		END		01		

VARIABLES	SN	TYPE	RELOCATION	REFS	37	DEFINED	100
3113 RXD	REAL	C		REFS	40	DEFINED	101
3112 RYE	REAL	C		REFS	39	DEFINED	101
3117 RYD	REAL	C		REFS	42	DEFINED	102
3126 RZE	REAL	C		REFS	28	DEFINED	122
3123 RZD	REAL	C		REFS	58	DEFINED	118
3117 T	REAL	C		REFS	59	DEFINED	119
3149 VCLNG	REAL	C		REFS	60	DEFINED	120
3137 VDELX	REAL	C		REFS	69	DEFINED	92
3140 VDELY	REAL	C		REFS	69	DEFINED	93
3141 VDELZ	REAL	C		REFS	70	DEFINED	94
3176 VDXB	REAL	C		REFS	44	DEFINED	110
3177 VDYB	REAL	C		REFS	43	DEFINED	106
3200 VDFB	REAL	C		REFS	65	DEFINED	113
3152 VTARG	REAL	C		REFS	66	DEFINED	113
3147 VTARGD	REAL	C		REFS	67	DEFINED	112
3173 VTXE	REAL	C		REFS	32	DEFINED	110
3174 VTYE	REAL	C		REFS	31	DEFINED	87
3175 VTZE	REAL	C		REFS	34	DEFINED	88
3102 VXE	REAL	C		REFS	33	DEFINED	89
3077 VXD	REAL	C		REFS	36	DEFINED	89
3106 VYE	REAL	C		REFS	35	DEFINED	89
3103 VYD	REAL	C		REFS	92	DEFINED	89
3112 VZE	REAL	C		REFS	92	DEFINED	89
3107 VZD	REAL	C		REFS	92	DEFINED	89

EXTERNALS	TYPE	ARGS	REFERENCES
COSD	REAL	1	2*110 111
SIND	REAL	1	111 112
STATEMENT LABELS			
0 10	INACTIV:	100	DEF LINE REFERENCES

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)
EUJIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	370 RANGE (1)
		1301 FZ3A (1)
		1603 VYED (1)
		1610 VZE (1)
		1615 RYED (1)
		1622 RZE (1)
		1625 RZBA (1)
		1628 ATURST (1)
		1631 VDELX (1)
		1634 RDELX (1)
		1637 VLSNG (1)
		1642 VTARG (1)
		1643 BPSIT (1)
		1647 RYED (1)
		1654 RYED (1)
		1659 VYED (1)
		1662 VDXB (1)
		1675 ANGA (1)
		1680 ADIVE (1)
		1710 G-413 (1)
		1722 CFA31 (1)
		1734 CFA33 (1)
		1699 RYED (1)
		1606 VYED (1)
		1611 RYED (1)
		1616 RYED (1)
		1623 RYED (1)
		1627 RYED (1)
		1629 ATURST (1)
		1632 VDELX (1)
		1635 RDELX (1)
		1636 VTARG (1)
		1646 BPSIT (1)
		1651 RYED (1)
		1654 RYED (1)
		1659 VYED (1)
		1662 VDXB (1)
		1675 ANGA (1)
		1680 ADIVE (1)
		1710 G-413 (1)
		1722 CFA31 (1)
		1734 CFA33 (1)
		1699 RYED (1)
		1606 VYED (1)
		1611 RYED (1)
		1616 RYED (1)
		1623 RYED (1)
		1627 RYED (1)
		1629 ATURST (1)
		1632 VDELX (1)
		1635 RDELX (1)
		1636 VTARG (1)
		1646 BPSIT (1)
		1651 RYED (1)
		1654 RYED (1)
		1659 VYED (1)
		1662 VDXB (1)
		1675 ANGA (1)
		1680 ADIVE (1)
		1710 G-413 (1)
		1722 CFA31 (1)
		1734 CFA33 (1)

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FTM 4.2+7.355

74/74 OPT=1

SUBROUTINE G1

STATISTICS

PROGRAM LENGTH

CH LABELED COMMON LENGTH

1334

73668

94

3030

LINE	CODE	TEXT	COL
5	C**ROUTINE 021		02
	C**AUTONUMAL DYNAMICS INITIALIZATION MODULE 02IEUL		02
	COMMON /C/ C13839)		02
	DIMENSION IPL (100)		02
	C**INPUT DATA		02
	EQUIVALENCE (C(1752),BP10)		02
	EQUIVALENCE (C(1753),STMT0)		02
	EQUIVALENCE (C(1754),BP51C)		02
	C**INPUTS FROM MAIN PROGRAM		02
	EQUIVALENCE (C(2561),N)		02
	EQUIVALENCE (C(2562),IPL)		02
	C**STATE VARIABLE OUTPUTS		02
	EQUIVALENCE (C(1703),CFA11)		02
	EQUIVALENCE (C(1707),CFA12)		02
	EQUIVALENCE (C(1711),CFA13)		02
	EQUIVALENCE (C(1715),CFA21)		02
	EQUIVALENCE (C(1719),CFA22)		02
	EQUIVALENCE (C(1723),CFA23)		02
	EQUIVALENCE (C(1727),CFA31)		02
	EQUIVALENCE (C(1731),CFA32)		02
	EQUIVALENCE (C(1735),CFA33)		02
	C**OTHER INPUTS		02
	EQUIVALENCE (C(1755),A02A)		02
	EQUIVALENCE (C(1756),A02B)		02
	EQUIVALENCE (C(1757),A02C)		02
	EQUIVALENCE (C(1758),A031)		02
	EQUIVALENCE (C(1759),A032)		02
	EQUIVALENCE (C(1760),A033)		02
	C**INITIAL CALCULATION OF EULER ANGLE MATRIX OF DIRECTION COSINES (CFA)		02
	USF-1 = SIND(BP10)		02
	UCPH1 = COS(BP10)		02
	US141 = SIND(3TMT0)		02
	UC141 = COS(3TMT0)		02
	USF51 = SIND(BP510)		02
	UCP51 = COS(BP510)		02
	CFA11 = UCP51*UCTMT		02
	CFA12 = USF51*UCFMT		02
	CFA13 = -USTMT		02
	CFA21 = -USP51*UCPH1+UCP51*USTMT*USPMT		02
	CFA22 = UCP51*UCPH1+USP51*USTMT*USPMT		02
	CFA23 = UCTMT*USPMT		02
	CFA31 = UCP51*USTMT*UCPH1+USP51*USPMT		02
	CFA32 = USF51*USTMT*UCPH1+USP51*USPMT		02
	CFA33 = UCTMT*UCPH1		02
	C		02
	C**INITIALIZE MATRIX COEF F3R FREE GYRO MODEL(S)		02
	C		02
	C**INTEGRATED PARAMETER LIST (IPL) FOR MPD,MQD,MRD,AND CFAD		02
	IPLTMT = 1700		02
	IPLIN-1 = 1704		02
	IPLIN-2 = 1708		02
	IPLIN-3 = 1712		02
	IPLIN-4 = 1716		02
	IPLIN-5 = 1720		02
	IPLIN-6 = 1724		02
	IPLIN-7 = 1728		02
	IPLIN-8 = 1732		02

SUBROUTINE 021	74/74	OPT=1	FTN 4.2+74355	07/07/75	11.06.21.	PAGE 2
60	IPL(NM1) = 1736 IPL(NM10) = 1740 IPL(NM11) = 1744 N = NM12 RETURN END					
				02	59	
				02	60	
				02	61	
				02	62	
				02	63	
				02	64	

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	
1 021	1	02	
VARIABLES	SN	TYPE	RELOCATION
3332 A021	REAL	C	REFS 23
3333 A022	REAL	C	REFS 24
3334 A023	REAL	C	REFS 25
3335 A031	REAL	C	REFS 26
3336 A032	REAL	C	REFS 27
3337 A033	REAL	C	REFS 28
3337 B0410	REAL	C	REFS 31
3331 B0510	REAL	C	REFS 35
3330 B0410	REAL	C	REFS 33
0 C	ARRAY	C	REFS 7
			REFS 14
			REFS 15
			REFS 16
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			REFS 449

SUBROUTINE D2L		7/4/74	GPT=1	FTN 4.2+74355	07/07/75	11.06.21.	PAGE
EJUV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)					
		1797	4031	11	1799	4033	(11)
		2560	N	(11)	2561	IPL	(100)
STATISTICS							
PROGRAM LENGTH		1009					
CM LABELED COMMON LENGTH		73668					
			64				
			3830				

SYMBOLIC REFERENCE MAP (R-37)

ENTRY POINTS DEF LINE REFERENCES
1 D2 1 59

VARIABLES SN TYPE RELOCATION

0	C	REAL	DEF LINE	REFERENCES	0	C	REAL	DEF LINE	REFERENCES
3240	CF411	REAL			19	19	28	21	22
3243	CF412	REAL			20	20	29	30	31
3247	CF412D	REAL			33	34	36	37	38
3256	CF413	REAL			41	53			
3253	CF413D	REAL			19	DEFINED			
3262	CF421	REAL			21	54			
3267	CF421D	REAL			20	DEFINED			
3266	CF422	REAL			23	55			
3263	CF422D	REAL			22	DEFINED			
3272	CF423	REAL			25	56			
3277	CF423D	REAL			24	DEFINED			
3276	CF431	REAL			27	54			
3273	CF431D	REAL			26	DEFINED			
3282	CF432	REAL			28	52			
3277	CF432D	REAL			31	50			
3286	CF433	REAL			30	DEFINED			
3283	CF433D	REAL			33	51			
3290	CF430	REAL			32	DEFINED			
3290	CF430D	REAL			35	52			
3290	CF430D	REAL			34	DEFINED			
3290	CF430D	REAL			36	50			
3290	CF430D	REAL			38	51			
3290	CF430D	REAL			39	50			
3290	CF430D	REAL			45	50			
3290	CF430D	REAL			46	50			
3290	CF430D	REAL			47	50			
3290	CF430D	REAL			48	50			
3290	CF430D	REAL			49	50			
3290	CF430D	REAL			50	50			
3290	CF430D	REAL			51	50			
3290	CF430D	REAL			52	50			
3290	CF430D	REAL			53	50			
3290	CF430D	REAL			54	50			
3290	CF430D	REAL			55	50			
3290	CF430D	REAL			56	50			
3290	CF430D	REAL			57	50			
3290	CF430D	REAL			58	50			
3290	CF430D	REAL			59	50			
3290	CF430D	REAL			60	50			
3290	CF430D	REAL			61	50			
3290	CF430D	REAL			62	50			
3290	CF430D	REAL			63	50			
3290	CF430D	REAL			64	50			
3290	CF430D	REAL			65	50			
3290	CF430D	REAL			66	50			
3290	CF430D	REAL			67	50			
3290	CF430D	REAL			68	50			
3290	CF430D	REAL			69	50			
3290	CF430D	REAL			70	50			
3290	CF430D	REAL			71	50			
3290	CF430D	REAL			72	50			
3290	CF430D	REAL			73	50			
3290	CF430D	REAL			74	50			
3290	CF430D	REAL			75	50			
3290	CF430D	REAL			76	50			
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3290	CF430D	REAL			79	50			
3290	CF430D	REAL			80	50			
3290	CF430D	REAL			81	50			
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3290	CF430D	REAL			112	50			
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3290	CF430D	REAL			124	50			
3290	CF430D	REAL			125	50			
3290	CF430D	REAL			126	50			
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3290	CF430D	REAL			165	50			
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3290	CF430D	REAL			167	50			
3290	CF430D	REAL			168	50			
3290	CF430D	REAL			169	50			
3290	CF430D	REAL			170	50			
3290	CF430D	REAL			171	50			
3290	CF430D	REAL			172	50			
3290	CF430D	REAL			173	50			
3290	CF430D	REAL			174	50			
3290	CF430D	REAL			175	50			
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3290	CF430D	REAL			179	50			
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3290	CF430D	REAL			187	50			
3290	CF430D	REAL			188	50			
3290	CF430D	REAL			189	50			
3290	CF430D	REAL			190	50			
3290	CF430D	REAL			191	50			
3290	CF430D	REAL			192	50			
3290	CF430D	REAL			193	50			
3290	CF430D	REAL			194	50			
3290	CF430D	REAL			195	50			
3290	CF430D	REAL			196	50			
3290	CF430D	REAL			197	50			
3290	CF430D	REAL			198	50			
3290	CF430D	REAL			199	50			
3290	CF430D	REAL			200	50			

STATEMENT LABELS DEF LINE REFERENCES

0 49 INACTIVE 50
0 52 INACTIVE 49
0 05 INACTIVE 47

SUBROUTINE 02 7/4/74 OPT=1 FTN 4.2*7.355 07/07/73 11.06.25. PAGE 4

ENVI CLASS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3838	
		1302 PMXDR (1)
		1699 CFALD (1)
		1702 CFALC (1)
		1706 CFALD (1)
		1711 CFALD (1)
		1714 CFALD (1)
		1719 CFALD (1)
		1721 CFALD (1)
		1723 CFALD (1)
		1730 CFALD (1)
		1735 WPD (1)
		1742 W2 (1)
		1747 FMIX (1)
		1750 CRAD (1)
		1303 PMXDR (1)
		1703 CFALD (1)
		1710 CFALD (1)
		1715 CFALD (1)
		1722 CFALD (1)
		1727 CFALD (1)
		1734 CFALD (1)
		1739 WPD (1)
		1746 W2 (1)
		1749 FMIX (1)
		3582 OPTAB (1)

STATISTICS

PROGRAM LENGTH	648	52
CM LABELED COMMON LENGTH	73668	3838

SUBROUTINE S11	74/7	OPT=1	FT4 .2+74355	07/07/75	11.06.29.	PAGE	1
SUBROUTINE S11							
C**SEEKER JANIT.MODULE							
COMMON /C/ C138301							
5	DIMENSION IZ(150), IV(150), ISNOX(40)						2
	EQUIVALENCE IC(136347), ISNOX(1), C135127, I3512						3
	EQUIVALENCE IC(14701), BIGERR						4
	EQUIVALENCE IC(14711), EPGER						5
	EQUIVALENCE IC(14651), S0Y						6
10	1 FORMAT(5X,2H3Z,5X,4(I13,111)/(13X,4(I13,111)))						7
	2 FORMAT(5X,2H3Z,5X,4(I13,111)/(13X,4(I13,111)))						8
	EQUIVALENCE IC(111),BY						9
	EQUIVALENCE IC(112),BZ						10
	EQUIVALENCE IC(2011),XSTEP						11
15	EQUIVALENCE IC(1600),IZ						12
	EQUIVALENCE IC(1630),IV						13
	DIMENSION IPL(100)						14
	EQUIVALENCE IC(1452),SMP						15
20	EQUIVALENCE IC(10415),HLR						16
	EQUIVALENCE IC(18419),HLQS						17
	EQUIVALENCE IC(14231),HLRS						18
	EQUIVALENCE IC(10427),STRIG						19
	EQUIVALENCE IC(10311),SPSLG						20
25	EQUIVALENCE IC(2562),IPL						21
	EQUIVALENCE IC(15504),OPTN4						22
	EQUIVALENCE IC(2662),DERSV						23
30	IPL(N1)=424						24
	IPL(N2)=409						25
	IPL(N3)=412						26
	IPL(N4)=415						27
	IPL(N5)=420						28
35	N=N*6						29
	C(411)=0.						30
	C(412)=0.						31
	C(413)=0.						32
	C(423)=0.						33
40	BY=0.						34
	S0Y=0.						35
	S0Z=0.						36
	100=1						37
45	C MONTE CARLO SEEKER OUTPUT STARTING VALUES						38
	C						39
50	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						40
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						41
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						42
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						43
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						44
55	C MONTE CARLO SEEKER POINTING ERROR						45
	C						46
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						47
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						48
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						49
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						50
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						51
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						52
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						53
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						54
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						55
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						56
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						57
	IF(15NOX(1),EQ.12) CALL MCARLO (0UM, 1, 100)						58

Line	Code	Statement	Address
59		IF(15NXX11.EQ.77) CALL MCARLC (DUM, 1, 100)	51
60	C	MCNTECARLO SEEKER DRIET	51
61	C	IF(15NXX11.EQ.55) CALL MCARLC (DUM, 1, 100)	51
62	C	IF(15NXX11.EQ.466) CALL MCARLC (DUM, 1, 100)	51
63	C	10 CONTINUE	51
64		BPTSIG = 3*HTG + BTGER	51
65		BPTSIG = BPTSIG + BPGERR	51
66			51
67			51
68			51
69			51
70		MLQ5=SMP*(3*HTG-BPTSIG)	51
71		MLQ=SMP*(BPTSIG-BPTSIG)	51
72		MLQ=SMP*(BPTSIG-BPTSIG)	51
73		C(13) = -1.	51
74		DENSIV=.002	51
75		C(451)=0.	51
76		C(452)=0.	51
77		C(453)=0.	51
78		C(454)=0.	51
79		IF(JUPIN,GT,1.) 50 TO 30	51
80		C(451)=1.	51
81		C(452)=1.	51
82		C(453)=1.	51
83		C(454)=1.	51
84		30 CONTINUE	51
85		NI=1	51
86		NI=1	51
87		SET=0.	51
88		DO 200 I=1,50	51
89		IZ(1)=0	51
90		200 IY(1)=0	51
91		RETURN	51
92		ENTRY 30	51
93		IF(SET,GT,0.) RETURN	51
94		IF(NI,GT,50) RETURN	51
95		IF(MI,GT,10) GO TO 100	51
96		NI=NI+1	51
97		MI=1	51
98		100 IZ(NI)=IZ(NI)+INT (52*2.*10**((10-MI)	51
99		IY(NI)=IY(NI)+INT (48*2.*10**((10-MI)	51
100		MI=MI+1	51
101		RETURN	51
102		ENTRY 50	51
103		IF(SET,GT,0. OR KSTEP,NE,2) RETURN	51
104		SET=1.	51
105		WRITE(6,1) (IZ(I),I=1,NI)	51
106		WRITE(6,2) (IY(I),I=1,NI)	51
107		RETURN	51
108		END	51

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	93	100
120 QJ	91			
1 S1I	1		90	
100 Sd	101	102	106	

VARIABLES	SN	TYPE	RELOCATION	7	63	69	70	71
720 BPSKR		REAL	C	REFS				
050 BPSIG		REAL	C	REFS	24	65	58	
				DEFINED	66			
720 BPSKR		REAL	C	REFS	6	63		
050 BPSIG		REAL	C	REFS	24	65	58	
				DEFINED	66			
12 BY		REAL	C	REFS	12	2*62	48	52
13 BZ		REAL	C	REFS	13	2*63	41	53
0 C		REAL	C	REFS	14	2*5	7	9
			ARRAY	REFS	15	16	19	20
				REFS	16	17	21	
				REFS	17	18	22	
				REFS	18	19	23	
				REFS	19	20	24	
				REFS	20	21	25	
				REFS	21	22	26	
				REFS	22	23	27	
				REFS	23	24	28	
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				REFS	143	144	148	
				REFS	144	145	149	
				REFS	145	146	150	
				REFS	146	147	151	
				REFS	147	148	152	
				REFS	148	149	153	
				REFS	149	150	154	
				REFS	150	151	155	
				REFS	151	152	156	
				REFS	152	153	157	
				REFS	153	154	158	
				REFS	154	155	159	
				REFS	155	156	160	
				REFS	156	157	161	
				REFS	157	158	162	
				REFS	158	159	163	
				REFS	159	160	164	
				REFS	160	161	165	
				REFS	161	162	166	
				REFS	162	163	167	
				REFS	163	164	168	
				REFS	164	165	169	
				REFS	165	166	170	
				REFS	166	167	171	
				REFS	167	168	172	
				REFS	168	169	173	
				REFS	169	170	174	
				REFS	170	171	175	
				REFS	171	172	176	
				REFS	172	173	177	
				REFS	173	174	178	
				REFS	174	175	179	
				REFS	175	176	180	
				REFS	176	177	181	
				REFS	177	178	182	
				REFS	178	179	183	
				REFS	179	180	184	
				REFS	180	181	185	
				REFS	181	182	186	
				REFS	182	183	187	
				REFS	183	184	188	
				REFS	184	185	189	
				REFS	185	186	190	
				REFS	186	187	191	
				REFS	187	188	192	
				REFS	188	189	193	
				REFS	189	190	194	
				REFS	190	191	195	
				REFS	191	192	196	
				REFS	192	193	197	
				REFS	193	194	198	
				REFS	194	195	199	
				REFS	195	196	200	
				REFS	196	197	201	
				REFS	197	198	202	
				REFS	198	199	203	
				REFS	199	200	204	
				REFS	200	201	205	
				REFS	201	202	206	
				REFS	202	203	207	
				REFS	203	204	208	
				REFS	204	205	209	
				REFS	205	206	210	
				REFS	206	207	211	
				REFS	207	208	212	
				REFS	208	209	213	
				REFS	209	210	214	
				REFS	210			

EXTERNALS	TYPE	ARGS	REFERENCES	59	50	51	52	53	54	55
PCRCLO		3								
INLINE FUNCTIONS										
A35	REAL	1	INTRIN	52						
INT	INTEGER	1	INTRIN	97						
SIGN	REAL	2	INTRIN	52						
STATEMENT LABELS										
213 1	FMT	10	104							
220 2	FMT	11	105							
0 18		64	44							
116 30		83	78							
140 100		87	87							
0 200		89	87							
LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES EXT REFS										
22 10	I	44 64	528							
123 200	I	67 89	23							
COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)										
C			0 C							
EQUIV CLASSES LENGTH MEMBERS - BIAS NAME(LENGTH)										
C			10 3V							
410 4LO			11 8Z							
422 4LOS			418 4LOS							
431 SMP			430 4LOS							
459 4TGERD			455 4TGERD							
649 IY			599 IZ							
2551 IPL			2560 M							
3511 13512			3503 OPT144							
3633 13512			3633 13512							
STATISTICS										
PROGRAM LENGTH			2503							
COMMON LABELLED COMMON LENGTH			73663							

SUBROUTINE S1	74/74	OPT=1	FIN +.2+7.355	07/07/75	11.06.31.	PAGE
175	C	30 CONTINUE				280
	C**MISSILE BODY RATES IN GIMBAL AXES					281
	MZ = U*31*NP*UB32*WD*UB33*MR					282
	MY = U*31*NP*UB22*WD*UB23*MR					283
						284
						285
						286
180	C	L**GIMBAL COUPLING				287
	UZK = SMP*(-BTHG + .1*3PSIG)					288
	UYK = SMP*(-BPSIG + .1*8THG)					289
	UZK = UZK + SOZ					290
	UYK = UYK + SOY					291
						292
185	C	C**GIMBAL ANGLE DERIVATIVES				293
	BTHG = MOP + UYK - MY					294
	BPSIG = MRP + UYK - MZ/UB33					295
						296
						297
190	C	IF (CAGE .GT. 0.) RETURN				298
	MLMR = 0.					299
	MLGD = 0.					300
	MLKD = 0.					301
	MLSD = 0.					302
	MLASD = 0.					303
	BTHG = 0.					304
	BPSIG = 0.					305
	RETJRN					306
	END					307
200	C**HELPER: AUTOPILOT INITIATION MODULE					308
	C**HIGH FREQ. MODEL					309
						310

[illegible]

SUBROUTINE S1				74/74	OPT=1	FTN **2+74355	07/0776	11.06.31.	PAGE	6
VARIABLES	SN	TYPE	RELOCATION							
373 US13	REAL			REFS	90	DEFINED	78			
374 US21	REAL			REFS	91	177	79			
375 US22	REAL			REFS	91	177	80			
376 US23	REAL			REFS	91	177	81			
377 US31	REAL			REFS	92	175	82			
400 US32	REAL			REFS	92	175	83			
401 US33	REAL			REFS	92	176	84			
367 US2	REAL			REFS	75	90	92	DEFINED	74	
365 UCT	REAL			REFS	76	77	94	DEFINED	72	
370 US2	REAL			REFS	77	74	93	DEFINED	75	
366 UST	REAL			REFS	78	82	93	DEFINED	73	
411 UY	REAL			REFS	163	DEFINED	122	172		
413 UYS	REAL			REFS	183	189	181	183		
410 UZ	REAL			REFS	151	DEFINED	121	168		
414 UZK	REAL			REFS	182	185	188	182		
022 MLAM1	REAL		C	REFS	59	131	134	157	DEFINED	140
				REFS	198					
026 MLAMR	REAL		C	REFS	60	132	135	169	DEFINED	141
				REFS	191					
032 ML2	REAL		C	REFS	41	133				
027 ML2D	REAL		C	REFS	43	135	138	DEFINED	184	158
				REFS	192					
042 ML2S	REAL		C	REFS	40	143	145			
037 ML2SU	REAL		C	REFS	47	145	DEFINED	143	159	194
038 ML2	REAL		C	REFS	46	184				
033 ML2D	REAL		C	REFS	45	137	139	DEFINED	135	170
				REFS	193					
046 ML2S	REAL		C	REFS	50	144	146			
043 ML2SU	REAL		C	REFS	49	145	DEFINED	144	173	195
712 ML2	REAL		C	REFS	25	145	146			
3312 MP	REAL		C	REFS	30	175	177			
3316 M1	REAL		C	REFS	39	173	177			
412 14P	REAL			REFS	140	143	186	DEFINED	181	145
				REFS	157					
3322 MR	REAL		C	REFS	48	175	177	DEFINED	182	146
413 MRP	REAL			REFS	141	144	177	DEFINED		
				REFS	169					
710 MSL	REAL		C	REFS	23	133	138	139		
711 MSN	REAL		C	REFS	24	142	143	144		
005 MT	REAL		C	REFS	64	185	DEFINED	177		
004 M2	REAL		C	REFS	63	186	DEFINED	176		
FILE NAMES										
EXTERNALS	TYPE	ARGS	REFERENCES							
ATAND	REAL	2	95							
OSD	REAL	1	72							
			149							
SIND	REAL	1	73							
SQT	REAL	1	LIBRARY	07						
INLINE FUNCTIONS										
ABS	REAL	1	DEF LINE	REFERENCES						
INT	REAL	1	INTRIN	117	118					
		2	INTRIN	107						
SIGN	REAL	2	INTRIN	114	115					

STATEMENT LABELS	DEF LINE	REFERENCES
0 10	INACTIVE	150
177 12		151
204 20		152
217 22		153
224 30		154
0 80	INACTIVE	101
127 31		110
131 82		129
163 83		148
274 101	FMT	6
306 102	FMT	8
320 103	FMT	10
66 823		104

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)
C 3830 0 3 (3830)

EQUIV CLASSES	LENGTH	MEMBERS	- BIAS NAME(LENGTH)
C	3830	10 84	(1)
		371 RYBA	(1)
		402 MLAMQ	(1)
		410 MLQ	(1)
		415 MLOSD	(1)
		422 M-RS	(1)
		427 8P9160	(1)
		435 BEPSY	(1)
		438 BGOEFL	(1)
		449 BJB	(1)
		449 CSA	(1)
		453 JS	(1)
		458 M2	(1)
		461 TKRZ	(1)
		464 SY	(1)
		1742 M2	(1)
		11 82	(1)
		372 RYBA	(1)
		405 MLAMR	(1)
		411 MLQ	(1)
		419 MLPSB	(1)
		423 BTHIC	(1)
		430 8P916	(1)
		436 M2	(1)
		437 WY	(1)
		445 DT	(1)
		447 CFOVZ	(1)
		450 SEPS	(1)
		456 MSL	(1)
		459 SZ	(1)
		462 TKRZ	(1)
		465 SDZ	(1)
		1746 WR	(1)
		378 RANGE	(1)
		373 RYBA	(1)
		407 MLQD	(1)
		414 MLR	(1)
		419 MLPSB	(1)
		426 BTHIC	(1)
		434 8P916	(1)
		437 WY	(1)
		445 DT	(1)
		447 CFOVZ	(1)
		451 SMP	(1)
		457 MSN	(1)
		458 GAGE	(1)
		463 TRKZY	(1)
		478 MP	(1)
		1939 T	(1)

STATISTICS

PROGRAM LENGTH 4108 279
CM LABELED COMMON LENGTH 73663 3830

60		EQUIVALENCE (C(433),MLZ)	34	60
		EQUIVALENCE (C(437),MLY)	34	61
		EQUIVALENCE (C(494),MLZS)	34	62
		EQUIVALENCE (C(501),MLYS)	34	63
		EQUIVALENCE (C(1657),RSLANT)	34	64
		EQUIVALENCE (C(1504),OPTN4)	34	65
65		EQUIVALENCE (C(2261),TME)	34	66
		EQUIVALENCE (C(2562),IPL)	34	67
		EQUIVALENCE (C(2662),JERSY)	34	68
		EQUIVALENCE (C(3634), ISNDX), (C(3512), I3512)	34	69
		EQUIVALENCE (C(3753), ITMOR)	34	70
70		EQUIVALENCE (C(3721), ITCT)	34	71
		EQUIVALENCE (C(3517), SIGM4)	34	72
		EQUIVALENCE (C(3524), SIGL3)	34	73
		EQUIVALENCE (C(3594), SIGO3)	34	74
		EQUIVALENCE (C(2011), KSTEP)	34	75
75		EQUIVALENCE (C(371),RANGE), (C(1615),PARKE), (C(1623),RZE)	34	76
		EQUIVALENCE (C(371),RANGE)	34	77
		C**NOMINAL SLEWER INPUT VALUES	34	78
		C DATA MSL, MSN, ML2, SMP, GS, MCZ, MF, OF, CROSS	34	79
80		.	34	80
		C DATA CZEIA,CKSWP,SGBIAS, MCN, MCL,SGSTOT, BLUP,CKNULL	34	81
		.	34	82
		C DATA STOTSM, STOTMX, RDES, MDES, RVIS, CPT, ETMR	34	83
85		.	34	84
		C DATA EDES,GSLIM/	34	85
		.	34	86
90		C DATA UVIS /1.,3.,5.,10.,15./	34	87
		UO 3 J=1,5	34	88
		IF (ABS(RVIS(J) - RVIS) .LT. .00001) GO TO 6	34	89
95		6 CONTINUE	34	90
		6 JVIS = J	34	91
		KUTJ = 1	34	92
		C(17) = 0.	34	93
		C(18) = 0.	34	94
		IPLIN = 424	34	95
100		IPLIN = 27420	34	96
		IPLIN = 21408	34	97
		IPLIN = 31412	34	98
		IPLIN = 41416	34	99
		IPLIN = 51420	34	100
105		NEN6	34	101
		C(411) = 0.	34	102
		C(415) = 0.	34	103
		C(419) = 0.	34	104
		C(423) = 0.	34	105
110		C(450) = 0.	34	106
		BY = 0.	34	107
		BY = 0.	34	108
		SOY = 0.	34	109
		SOZ = 0.	34	110
		SOY = 0.	34	111
		SOZ = 0.	34	112
		SOY = 0.	34	113
		SOZ = 0.	34	114
		SOY = 0.	34	115
		SOZ = 0.	34	116

	CI 401H = 1.	174
	CI 402I = 1.	175
	CI 403I = 1.	176
	CI 404I = 1.	177
175	30 CONTINUE	178
	C** SEEKER INIT.	179
	MLQ = VMITE/RSIANT+BTMG + SMP+BTMG + BPSIG + 550145	180
	MLR = VMITE/RSIANT+BPSIG + SMP+BTMG + BPSIG	181
180	MLQS = MLQ	182
	MLRS = MLR	183
	IPLIN 1 = 488	184
	IPLIN 11 = 484	185
	N = N + 2	186
185	CI 403I = 0.	187
	CI 407I = 0.	188
	IPLIN 1 = 488	189
	IPLIN 11 = 491	190
190	IPLIN 21 = 495	191
	IPLIN 31 = 499	192
	N = N + 4	193
	CI 491I = 0.	194
	CI 494I = 0.	195
	CI 498I = 0.	196
195	CI 501I = 0.	197
	MLZ = MLQ	198
	MLZS = MLQ	199
	MLYS = MLR	200
200	MLY = MLR	201
	RETURN	202
	END	203

437

VARIABLES	SN	TYPE	RELOCATION	REFS	34	DEFINED	96	101	102	103	104
1057 KOTO	INTEGER	C		REFS	64	94	100	101	102	103	104
5000 N	INTEGER	C		REFS	189	189	184	187	188	189	190
				REFS	191	184	184	191			
3027 OPTN4	REAL	C		REFS	63	171					
302 RANGE	REAL	C		REFS	74	DEFINED	135				
1015 ROTS	REAL	C		REFS	13	DEFINED	94				
20 RUSTOT	REAL	C		REFS	44	DEFINED	115				
207 KINSTRT	REAL	C		REFS	160	161					
3202 RLANT	REAL	C		REFS	62	179					
1020 RVIS	REAL	C		REFS	15	35	93	DEFINED	94		
5110 RVS	REAL	C		REFS	74	2*135					
3120 MTS	REAL	C		REFS	74	115	2*135				
720 SOT	REAL	C		REFS	47	150	132	DEFINED	113		
721 SOT	REAL	C		REFS	46	145	147	DEFINED	114		
702 SOPS	REAL	C		REFS	24						
774 SOSIAS	REAL	C		REFS	20	32	178	DEFINED	94		
776 SOSTOT	REAL	C		REFS	21	DEFINED	31				
3741 S1L3	REAL	C	ARRAY	REFS	4	78	DEFINED	139			
3071 SIGMA	REAL	C	ARRAY	REFS	4	70	DEFINED	146	147	151	152
7011 SISUB	REAL	C	ARRAY	REFS	4	70	DEFINED	146			
264 SHR	REAL	C		REFS	141	DEFINED	117	138			
1007 STOT	REAL	C		REFS	39	139					
1014 STOTX	REAL	C		REFS	12	33	137	DEFINED	94		
1013 STOTSM	REAL	C		REFS	41	41	130	DEFINED	94		
703 SPS	REAL	C		REFS	25	57	178	179	DEFINED	78	
1010 TK38	REAL	C		REFS	36	146	2*147	151	2*152		
1110 UVIS	REAL	C		REFS	4	93	DEFINED	98			
316 VDATE	REAL	C	ARRAY	REFS	50	178	179				
775 V2	REAL	C		REFS	21	DEFINED	91				
1009 VCV	REAL	C		REFS	21	DEFINED	91				
723 VZ	REAL	C		REFS	19	DEFINED	78				
705 VZ	REAL	C		REFS	19	DEFINED	78				
632 V2	REAL	C		REFS	51	180	196	197	DEFINED	178	
642 WLS	REAL	C		REFS	53	DEFINED	198	199	DEFINED	179	
636 WLS	REAL	C		REFS	52	181	198	199	DEFINED		
680 WLS	REAL	C		REFS	54	DEFINED	191				
746 WLY	REAL	C		REFS	59	DEFINED	199				
764 WLYS	REAL	C		REFS	61	DEFINED	198				
742 WLS	REAL	C		REFS	58	DEFINED	196				
755 WLS	REAL	C		REFS	60	DEFINED	197				
712 WLS	REAL	C		REFS	29	DEFINED	78				
710 WLS	REAL	C		REFS	27	DEFINED	78				
711 WSN	REAL	C		REFS	28	DEFINED	78				
265 X	REAL	C		REFS	145	146	147	150	154	152	
				DEFINED	141	145	150				
EXTERNALS	TYPE	ARGS	REFERENCES								
60400	REAL	1	134	125	129	153	150	161			
SORT	REAL	1	LIBRARY								
SST	REAL	0	135								
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE REFERENCES								
ABS	REAL	1	INTRIN	93	145	147	150	152			

STATEMENT LABELS		DEF LINE REFERENCES	
0 5	94	92	
13 6	95	93	
0 10	156	120	
14 20	153	148	
111 21	144	142	
125 22	144	143	
182 23	154	134	
201 30	176	171	
0 500	162	158	

LIPS LABEL		INDEX		FROM-TO		LENGTH		PROPERTIES		EXITS	
0 5	J	12	44	53				INSTACK			
147 500	I	120	156	1030				EXT REFS			

COMMON BLOCKS		LENGTH		MEMBERS - BIAS NAME(LENGTH)	
C		3830		0 C	(3830)

CIVIL CLASSES		LENGTH		MEMBERS - BIAS NAME(LENGTH)	
C		3830		10 3V	(1)
				206 VMTE	(1)
				414 MLR	(1)
				426 RMTG	(1)
				435 BEPSV	(1)
				451 S4P	(1)
				457 ASN	(1)
				465 SZZ	(1)
				493 MLZS	(1)
				501 WFL	(1)
				506 CETA	(1)
				509 MSL	(1)
				518 BLUR	(1)
				522 GKNUL	(1)
				525 RDES	(1)
				529 OPT	(1)
				534 JVIS	(1)
				538 S3LIM	(1)
				1666 RSLANT	(1)
				2661 IPL	(100)
				3511 I3512	(1)
				3593 SIGUR	(40)
				3752 IINDX	(10)

STATISTICS		PROGRAM LENGTH		CM LABELED COMMON LENGTH	
		11153	589		
		73668	3830		

SUBROUTINE S4 7/4/74 OPT=1 FTN 4.274355 07/0775 11.06.39. PAGE 3

```

119 C
C  ATMOSPHERIC COEFFICIENTS AS A FUNCTION OF ALTITUDE (UM)
C
C  DATA UM / 0..300..500..1000..2000..5000..6560..10000..
C  * 20000..33000./
C
120 C  DATA UGRM /
C  1 0...04210...06735...1254...2180...3697...4049...4465...4773...4762,
C  3 0...03636...05987...1101...1916...3255...3588...3921...4134...4222,
C  5 0...03179...05079...09472...1649...2613...3086...3399...3594...3.42,
C  * 0...01878...03010...05631...09863...1709...1883...2086...2245...2133,
C  * 0...00378...00340...0179...03235...06056...06737...07733...04962,
C  * 0.00000/
C
125 C
C  IF (SGSTOT.GT.0.)CALL NORM(ROSTOT,-3..3..0.,SGSTOT,RANSTT)
C  UCT = COSD(THETA)
C  UST = JND(THETA)
C  UCP = CSD(THETA)
C  USP = SLD(THETA)
C  UUT = UCT*UCP
C  UB12 = UCT*USP
C  UB13 = -UST
C  UB21 = -USP
C  UB22 = UCP
C  UB23 = 0.
C  UB31 = -UST*UCP
C  UB32 = UST*USP
C  UB33 = UCT
C
130 C
C  TRANSFORM LOS FROM BODY TO GIMBAL AXES
C  RXG = UBL1*RXA+UBL2*RYBA+UBL3*RZBA
C  RYG = UBL1*RYA+UBL2*RYB+UBL3*RZB
C  RZG = UBL1*RXA+UBL2*RYB+UBL3*RZBA
C
135 C  LOS ERRORS IN PLATFORM COORDINATES
C  BEPS2 = ATAND(RYG/RXG)
C  BEPSY = ATAND(RYG/RXG)
C  BEPSZ = BEPS2 - SEPS + THETA + 90 + SINT(MFAT)
C  BEPSY = BEPSY - SEPS + UPSI + 90 + COS(MFAT)
C  BEPSZ = BEPSZ - SEPS + UPSI + 90 + COS(MFAT)
C  GO CONTINUE
C  IF (C(17).LE.0.) GO TO 82
C  IF (C(17).GT.-.00001) GO TO 82
C  IF (C(13).LE.0.) GO TO 820
C  C(13) = 1.
C  ST = T
C  C(266) = OT / AINT(OT / C(276))
C  820 CONTINUE
C  ST = ST + OT
C
140 C  SIGNATURE TO FREQUENCY RATIO FOR LASER DETECTOR
C  ENTRY JNST
C  J = JNIS
C  UCOSA = -RXZ/RANGE
C  DESIGNATOR TRANSMISSION
C  IF (CUTU.EQ. 0) GO TO 16
C  160 GO TO 0
C  IF (C(13).GT. 0.) GO TO 14
C  UTU = EXP (-UGANZ(JN)* RDES/3201.)

```

Line	Code	Text	Address
175	C**	SEKER TRANSMISSION 1b IF(ICH.GT. 0.1) GO TO 18	375 376 377 378 379 380 381
180	C**	UTS = DAP (-UGAM1/2) + RANGE/32811 GO TO 20	382 383 384 385 386 387
185	C**	18 F = 0. UGAMS = FINTPI(185,UM,UGAM1,1,10,F,XL) UTS = EXP(-UGAMS + RANGE/RH)	388 389 390 391 392 393
190	C**	20 STOT = (DES + CRT + JGOSK + UTO + UTS) / (PI * ETAR * (RANGE/3281.1**2))	394 395 396 397 398 399
195	C**	STOT = STOT + 10.0**400STOT/10.1 BLUR2 = BLUR/2.0 IF(1STOT.LE. 0.1) GO TO 22	400 401 402 403 404 405
200	C**	TKO3 = BLUR/12. * STOT BNUL = BLUR/100BNUL * STOT GO TO 24	406 407 408 409 410 411
205	C**	22 TKO3 = BLUR BNUL = BLUR 24 BNUL12 = BNUL/2. IF(1N12.EQ.0) RETURN	412 413 414 415 416 417
210	C**	BNZ = SIGN(1.,BEP5Z) IF(ABS(BEP5Z).GT. FK08) GO TO 100 BZ = 0. GO TO 200	418 419 420 421 422 423
215	C**	100 IF(1BNUL.GT. BLUR) GO TO 200 IF(ABS(BEP5Z).GT. BLUR2) GO TO 200 IF(ABS(BEP5Z).GT. BNUL2) GO TO 110	424 425 426 427 428 429
220	C**	110 SMALL SIGNAL BANG-BANG BZ = SIGN(1BNUL/BLUR,BEP5Z) GO TO 200	430 431 432 433 434 435
225	C**	200 3Y = SIGN(1.,BEP5Y) IF(ABS(BEP5Y).GT. FK08) GO TO 210 BY = 0. GO TO 32	436 437 438 439 440 441
230	C**	32 IF(1BNUL.GT. BLUR) GO TO 32 IF(ABS(BEP5Y).GT. BLUR2) GO TO 12 IF(ABS(BEP5Y).GT. BNUL2) GO TO 220	442 443 444 445 446 447
235	C**	12 SMALL SIGNAL BANG-BANG BY = SIGN(1BNUL/BLUR,BEP5Y)	448 449 450 451 452 453

```

230 C** LINEAR
231 220 BY = B2PSY/BLR2
232 32 CONTINUE
233 C SIGNAL PROCESSING GAIN VARIATIONS
234 C
235 DO 13 I=1,ITOT
236 C***RANDOMIZE SEEKER OUTPUT GAIN GS=C(1450)+-- AND/OR SEEKER OUTPUT
237 C**LIMIT GS LIN=C(1539)--
238 I00=1
239 IF (ITNOX(I).EQ.456)CALL MCARLO(DUM,2,I00)
240 IF (ITNOX(I).EQ.456)CALL MCARLO(DUM,2,I00)
241 13 CONTINUE
242 B2=55*B2
243 BY=65*BY
244 IF (ABS(B2).GT.GSLIN)B2=SIGN(GSLIN,B2)
245 IF (ABS(BY).GT.GSLIN)BY=SIGN(GSLIN,BY)
246 C
247 C** LIMIT SWITCH ON S/T RATIO
248 /O IF (STOT.GT.STOTSM) GO TO 40
249 IF (ABS(B2).GT.STOTMX) B2 = SIGN(STOTMX,B2)
250 IF (ABS(BY).GT.STOTMX) BY = SIGN(STOTMX,BY)
251 40 CONTINUE
252 C
253 MLAQ = B2
254 MQF = MLAQ
255 MLAR = BY
256 MRF = MLAR
257 82 CONTINUE
258 C** LEAD INTEGRAL COMPENSATION
259 C
260 MSL = 0.3*AIM GS ONLY
261 MSL = NE. 0. GS * (S/MSL + 1)/S
262 C
263 IF (MSL.EQ.0) GO TO 83
264 MLQD = B2
265 MLRQ = BY
266 IF (STOT.GT.STOTSM) MLRQ = 0.
267 IF (STOT.GT.STOTSM) MLQD = 0.
268 MQPPP = MLQD/MSL + MLQ
269 MRPPP = MLRQ/MSL + MLR
270 MLAMQ = MQPPP
271 MLARQ = MRPPP
272 C** PLATFORM COMPENSATION (S/ML2 + 1) / (S/MSN + 1)
273 C
274 IF (MSN.EQ.0) GO TO 83
275 MLQSD = MSN * (MQPPP - MLQD)
276 MLRSD = MSN * (MRPPP - MLRQ)
277 MQFFF = MLQSD / ML2 + MLQD
278 MRFFF = MLRSD / ML2 + MLRQ
279 IF (STOT.GT.STOTSM) GO TO 83
280 MLAMQ = MLAMQ
281 MLARQ = MLARQ
282 MQP = MQPPP
283

```



```

      WRP = WRP + WRP
      93 CONTINUE
      C** SPRING TERM COMPENSATION
      C
      290      MLAMP = MLAMP
      MLAMP = MLAMP
      295
      C** GUIDANCE FILTER 1. (S/MCN+1) ((S/MCZ)**2 * CZETA * S/MCZ+1)
      C
      299      MLAYZ = MLAMP
      MLAYZ = MLAMP
      C NO GUIDANCE FILTER DURING LINEAR OPERATION
      C
      300      IF (MCN .LE. 0.) GO TO 90
      IF (STOT .GT. STOTSM) MLAMP = 0.
      IF (STOT .GT. STOTSM) MLAMP = 0.
      MLZ = MCN * (MLAMP - MLZ)
      MLZ = MCN * (MLAMP - MLZ)
      MLZ = MCN * (MLAMP - MLZ)
      305      MLAYZ = MLZ/MCZ + MLZ
      MLAYZ = MLZ/MCZ + MLZ
      IF (MCZ .LE. 0.) GO TO 90
      MLZSD = MCZ * (MCZ*(MLAYZ - MLZS) - 2. * MLZSD * CZETA)
      MLZSD = MCZ * (MCZ*(MLAYZ - MLZS) - 2. * MLZSD * CZETA)
      IF (STOT .GT. STOTSM) GO TO 90
      310      MLAYZ = MLZS
      MLAYZ = MLZS
      90 CONTINUE
      C** MISSILE RATES IN GIMBAL AXES
      C
      315      WZ = WZ + WZ + WZ + WZ + WZ + WZ
      WY = WY + WY + WY + WY + WY + WY
      C** SPRING TERM (IN-AXIS AND CROSS AXIS) AND CROSS COUPLING
      C
      320      UZK = SHP * (-BHTG - BPSIG) - CROSS * WRP
      UZK = UZK + S2
      UYK = UYK + S2
      C** GIMBAL ANGLE DERIVATIVES
      C
      325      BHTG = WRP + UZK - WY - S2
      BPSIG = WRP + UYK - WZ/U33
      RETURN
      END
  
```

SYMBOLIC REFERENCE MAP (1-3)									
ENTRY POINTS	DEF LINE	REFERENCES							
1 5*	164	199	330						
103 S4ST									
* VARIABLES									
003 B2SV	REAL	C							
002 B2SZ	REAL	C							
770 3F	REAL	C							
1005 BLJR	REAL	C							
504 9LJR2	REAL								
505 BNJLL	REAL								
1011 BNJLL2	REAL	C							
020 B2SIG	REAL	C							
053 B2S1G0	REAL	C							
022 B1T1G	REAL	C							
047 B1T1G0	REAL	C							
12 EF	REAL	C							
13 JZ	REAL	C							
0 C	REAL	C							
1012 UKNUL	REAL	C							
773 UK3M*	REAL	C							
1021 GPT	REAL	C							
771 G2S*	REAL	C							
772 G2T*	REAL	C							
070 UT	REAL	C							
570 UY4	REAL	C							
1023 G2S	REAL	C							
1022 E1R	REAL	C							
557 F	REAL	C							
707 JS	REAL	C							
1016 GSL14	REAL	C							
1010 M2S	REAL	C							
560 I	INTEGER	C							
507 IJ0	INTEGER	C							
1031 INIT	INTEGER	C							
7210 I20T	INTEGER	C							
7250 ITN0X	INTEGER	C							
554 J	INTEGER	C							

SUBROUTINE S4				74/74 OPT=1				FTN 4.2+74355				07/07/76 11.06.39.				PAGE 10			
INLINE FUNCTIONS		TYPE		AKOS		DEF LINE		REFERENCES											
ABS		REAL		1		INTRIN		204		209		210		220		225		246	
AIYT		REAL		1		INTRIN		251		252									
SIGN		REAL		2		INTRIN		203		212		213		228		245		251	
STATEMENT LABELS						DEF LINE		REFERENCES											
0 13						242		236											
122 14						173		170											
133 16						177		158		172									
141 18						180		177											
152 20						184		179											
174 22						196		182											
177 24						198		195											
244 32						232		223		224		225		223					
305 40						253		250											
0 70						250													
0 80						153													
311 82						259		154		155									
325 83						207		265		277		202							
421 90						312		293		306		309							
210 100						208		204											
221 110						215		210											
223 200						219		207		208		209		243					
231 410						224		220											
242 220						231		226											
100 820						160		156											
LOOPS LABEL		INDEX		FROM-TO		LENGTH		PROPERTIES		EXT REFS									
245 13		1		236 242		148													
COMMON BLOCKS		LENGTH		MEMBERS - BIAS NAME(LENGTH)															
C		3830		0 C		(3830)													
C		LENGTH		MEMBERS - BIAS NAME(LENGTH)															
C		3830		10 BY		(1)						11 RZ		(1)		16 RDS101		(1)	
				208 R4		(1)						370 RANG		(1)		371 RY8A		(1)	
				372 R78A		(1)						373 R28A		(1)		412 W44Z		(1)	
				406 W44Y		(1)						407 W400		(1)		418 WLO		(1)	
				411 W400		(1)						414 WLR		(1)		415 W4250		(1)	
				418 W425		(1)						419 W4250		(1)		422 W4250		(1)	
				423 BTH160		(1)						426 BTH160		(1)		427 BTH160		(1)	
				430 BPS16		(1)						432 W440		(1)		433 W440		(1)	
				434 BPS16		(1)						435 BPS16		(1)		436 W42		(1)	
				437 W42		(1)						438 DT		(1)		439 SEPS		(1)	
				451 W40		(1)						455 G5		(1)		456 W42		(1)	
				457 W40		(1)						458 W42		(1)		459 ST		(1)	
				464 S3T		(1)						465 S02		(1)		479 W420		(1)	
				482 W42		(1)						483 W420		(1)		486 W42		(1)	
				487 W42500		(1)						490 W42500		(1)		493 W425		(1)	
				494 W42500		(1)						497 W4250		(1)		499 W42		(1)	
				500 W425		(1)						501 W42		(1)		502 W4250		(1)	
				503 W425		(1)						504 W42		(1)		505 W4250		(1)	
				506 W4250		(1)						507 W4250		(1)		508 W4250		(1)	
				509 W42		(1)						510 W4250		(1)		511 W4250		(1)	
				519 B40R		(1)						520 W4250		(1)		521 W4250		(1)	
				521 BNULL2		(1)						522 BNULL2		(1)		523 W4250		(1)	
				524 STOTMX		(1)						525 W4250		(1)		526 W4250		(1)	

SUBROUTINE S= 7474 OPT=1 FTN 3.2*74355 07/0775 11.06.39. PAGE 11

QUIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
500 RYIS	(1)	500 OPT (1)
531 EDES	(1)	531 JVIS (1)
537 IMIT	(1)	538 GSLEM (1)
1618 RYE	(1)	1614 RYE (1)
1782 M2	(1)	1622 RZE (1)
3510 RANSTT	(1)	1786 MR (1)
		3720 ITCT (1)
		530 CTR2 (1)
		535 KUT2 (1)
		1614 RYE (1)
		1710 WP (1)
		1939 Y (1)
		3722 ITNDX (10)

STATISTICS
PROGRAM LENGTH 7048 452
CH LABELED COMMON LENGTH 73668 3830

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
I CII 1 67

VARIABLES	SN	TYPE	RELOCATION	REFS	DEF LINE	REFERENCES
0 C		REAL	ARRAY C			
137 UMIG		REAL		30	31	32
134 UM4		REAL		37	38	39
132 I		INTEGER		45	46	47
133 I00		INTEGER		51	52	53
5001 IPL		INTEGER	ARRAY C	58	59	60
7001 ISNDX		INTEGER	ARRAY C	61	62	63
5007 I3312		INTEGER	C	64	65	66
5000 N		INTEGER	C	67	68	69
1317 NUSUM		INTEGER	C	70	71	72
136 RN		REAL		73	74	75
135 KMSRT		REAL		76	77	78
1310 USC6		REAL		79	80	81
1311 USC5		REAL		82	83	84
EXTERNALS		TYPE	ARG	REFS	DEF LINE	REFERENCES
CJSD		REAL	1	51	52	53
MCARLO		REAL	3	54	55	56
KANNUM		REAL	3	57	58	59
SIND		REAL	1	60	61	62
STATEMENT LABELS		DEF LINE	REFERENCES			
0 30		59	50			
LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS	
47 30	1	30 59	403			
COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)			
C	3030	0 C	(3030)			
ENTRY CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)			
C	3810	843 USC6 (1)	841 USC5 (1)			
		2500 N (1)	2501 IPL (1004)			
		3033 ISNDX (40)	3514 NUSUM (1)			
STATISTICS						
PROGRAM LENGTH		1408	95			
CM LABELLED COMMON LENGTH		73003	3630			


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115 1* (ABS(WRS) - GT, 30.) WRS = SIGN(30., WRS)
    LNS=(WRS-400) - (WRS-WRC)
    WPR=(WRS-WRC) * (WRS-WRC)
    C**SUMMATION OF RATE DAMPING AND GUIDANCE SIGNALS AND THEIR DERIVATIVES
    EZMSD = ZMRSP
    EZMSD = EZMRSP
    EZMSD = WPI*(WPI*(EZMSD - EZMSD) - 2.*001*EZMSD)
    EZMSD = 401*(WPI*(EZMSD - EZMSD) - 2.*001*EZMSD)
    EODCR = 2.*0*(EZMSD + (40.*15.) * EZMSD + (40.*15.) * EZMSD / (40.*15.))
    EVNCR = 2.*0*(EZMSD + (40.*15.) * EZMSD + (40.*15.) * EZMSD / (40.*15.))
    IF (ABS(EODCR) .LT. HLIMP) GO TO 30
    EODCR = SIGN (HLIMP, EODCR)
    EVNCR = SIGN (HLIMP, EVNCR)
    30 IF (ABS(EVNCR) .LT. HLIMP) GO TO 40
    EVNCR = SIGN (HLIMP, EVNCR)
    40 CONTINUE
    C**FULL SIGNAL SHAPING
    BPISD = ZMRSP
    BPISD = WPI*(WPI*(BPISD - BPISD) - 2.*001*BPISD)
    BPISD = 401*(WPI*(BPISD - BPISD) - 2.*001*BPISD)
    IF (ABS(BPISD) .GT. HLIMP) BPISD = SIGN(HLIMP, BPISD)
    135 BDELPC = .1*(BPISD/.1 + BPISD)
    C**COMMANDS TO ACTUATORS
    BDELTC(1) = EODCR + BDELPC
    BDELTC(2) = EVNCR + BDELPC
    BDELTC(3) = EODCR - BDELPC
    BDELTC(4) = EVNCR - BDELPC
    RETURN
    END

```


SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS DEF LINE REFERENCES
1 C1 141

VARIABLES SN TYPE RELOCATION

1474 AK33	REAL			29	105	
1475 AK3R	REAL			30	2*106	
1504 AK3A	REAL			33	105	
1505 AK3AK	REAL			34	105	
1500 AK3Q	REAL			31	105	
1501 AK3R	REAL			32		
217 AN3	REAL			105	DEFINED 104	
214 AN3Y	REAL			27	104	
215 AN3Z	REAL			28	104	
1552 B0ELPC	REAL			82	137	139 140
1327 B0ELTC	REAL			135	138	139 140
222 B04	REAL			132	DEFINED 137	138 139 140
1442 B041S	REAL			49	135	DEFINED 133 134
1437 B041SD	REAL			25	133	133
540 B041	REAL			74	132	133
1576 B01S	REAL			73	132	133
1573 B01SU	REAL			71	133	DEFINED 131
1567 B01SDO	REAL			72	131	DEFINED 132
1572 B01SP	REAL			4	7	9 10 11 12
0 C				13	15	16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81
1535 B01	REAL			15	132	
1547 B01	REAL			21	121	122
1406 B01CK	REAL			48	125	126 137 139
1463 B01CKO	REAL			126		
1472 B01CKR	REAL			47	DEFINED 123	123 128 140
1407 B01CKO	REAL			49	DEFINED 124	124
026 B01	REAL			38	94	DEFINED 88
1543 B01R	REAL			81	122	DEFINED 117
1402 B01S	REAL			70	124	124
1427 B01SD	REAL			69	122	124
1423 B01SDO	REAL			67	124	DEFINED 120
1456 B01SP	REAL			68	120	DEFINED 122
1512 B01	REAL			58	94	96
1507 B01SD	REAL			57	36	DEFINED 92
1503 B01SDO	REAL			55	DEFINED 94	
1500 B01SP	REAL			56	92	
1500 B01SD	REAL			62	92	
1503 B01SDO	REAL			37	DEFINED 87	

SUBROUTINE C1	7474	GPI=1	MEMBERS - BIAS NAME(LENGTH)		FTN	*274355	07/07/75	11:06:46.	PAGE	6
EQUIV CLASSES	LENGTH									
910 EVRS	(1)	911 EVRSDD	(1)	914 EVRSP	(1)					
915 EVRS	(1)	918 EVRS	(1)	919 EDCRD	(1)					
922 EDCRD	(1)	923 EVNCRD	(1)	926 EVNCR	(1)					
927 E2SDO	(1)	928 AK91	(1)	929 AK91	(1)					
930 E2SP	(1)	931 E2S1	(1)	932 AKPD	(1)					
933 AKPR	(1)	934 E2S	(1)	935 EYSDO	(1)					
936 AKORR	(1)	937 AKORR	(1)	938 EVSP	(1)					
939 E2SD	(1)	940 UCC1	(1)	941 USC1	(1)					
942 E2S1	(1)	943 HLMQ	(1)	944 HLMQ	(1)					
951 Q2IAS	(1)	952 GRIAS	(1)	953 GRIAS	(1)					
954 GR	(1)	955 BDELTC	(1)	956 MPI	(1)					
961 DPI	(1)	962 TAUZ	(1)	963 TAUJ	(1)					
964 TLMF	(1)	965 TOR	(1)	966 QZ	(1)					
967 EVRR	(1)	968 MQC	(1)	969 MRC	(1)					
970 M21	(1)	971 DOL	(1)	972 SDELPC	(1)					
975 EVRR	(1)	976 TAUJ	(1)	979 E2SDO	(1)					
982 EVSS	(1)	983 EYSDO	(1)	985 EYSS	(1)					
987 SPISDO	(1)	988 BPISB	(1)	991 SPISD	(1)					
994 SPIS	(1)	995 AKST	(1)	997 AKST	(1)					
1735 MPD	(1)	1742 HQ	(1)	1743 AKST	(1)					
1999 F	(1)	3583 OPTN4	(1)	1746 WR	(1)					

STATISTICS

PROGRAM LENGTH 2238 147

CM LARS-23 COMMON-LENGTH 23665 3936

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SUBROUTINE C31
COMMON /C/ C(1839)
1  IF (C(2664)-0.01 .LT. 1.E-6) GO TO 10
   WRITE(6,20)
   C(2664)=0.01
20  FORMAT(* INTEGRATION STEP SIZE LARGER THAN SAMPLE RATE,SET EQUAL
    TO SAMPLE RATE*)
10  IF (ABS(C(446)-0.01*AINT(C(446)/0.01*1.E-6)).LT.1.E-6) GO TO 30
   WRITE(6,30)
40  FORMAT(* PRF IS NOT A MULTIPLE OF THE SAMPLE RATE*)
   STOP
30  IF (ABS(0.01-C(2634)*AINT(0.01/C(2664)+1.E-6)).LT.1.E-6) GO TO 50
   C(2634)=0.01*AINT(0.01/C(2664)+1.E-6)
   WRITE(6,45)C(2634)
15  FORMAT(* INTEGRATION STEP SIZE NOT A MULTIPLE OF SAMPLE RATE*
    C* ADJUSTED STEP SIZE IS*,15.5)
50  CONTINUE
   C(3+62)=0.0
   DO 1 I=1,21
20  1  C(337+I)=0.0
   C(877)=0.
   C(831)=0.
   RETURN
   END

```


SYMBOLIC REFERENCE MAP (3=3)

ENTRY POINTS		DEF LINE		REFERENCES	
1 G31		1		23	
VARIABLES		SN TYPE		RELOCATION	
0 C		REAL		ARRAY C	
114 A		INTEGEN		REFS	
				DEFINED	
				REFS	
				2	
				5	
				20	
				DEFINED	
				19	
				20	
				21	
				22	
FILE NAMES		MODE		WRITES	
TAPED		FMT		4	
				9	
				14	
INLINE FUNCTIONS		TYPE		DEF LINE	
ABS		REAL		REFERENCES	
MINI		REAL		12	
				12	
				13	
STATEMENT LABELS		DEF LINE		REFERENCES	
0 1		20		19	
11 10		0		3	
20 20		0		4	
22 30		12		8	
64 40		10		9	
70 45		15		14	
33 50		17		12	
LOOPS		INDEX		FROM-TO	
40 1		1		LENGTH	
				PROPERTIES	
				INSTACK	
				33	
COMMON BLOCKS		LENGTH		MEMB-RS - BIAS NAME(LENGTH)	
0 C		3330		0 C	
				13330	
STATISTICS		PROGRAM LENGTH		1153	
		COMMON LENGTH		77	
		COMMON LABELS		73008	
				3330	

SUBROUTINE C3	74/74	UPI=1	FTN ++2+7+355	07/07/76	11.06.53.	PAGE	2
60	BPSIS=BPSI BXA=BPHL CALL ATD(BXX,3) CALL ATD(3THS,*) CALL ATD(BPSIS,*) CALL MODCON(2,3,M2C,BLQSS) CALL MODCON(2,4,M2C,BLQSS) BJJ=9LQSS-3THS BKK=2LRSS-BPSIS CALL QUAN(BJJ,4,*) CALL QUAN(BKK,4,*) CALL MODCON(4,7,BXX,BKKSS) CALL MODCON(3,5,BJJ,BKKSS) CALL MODCON(3,6,BKK,BKKSS) IF(ABS(BJJSS).GT.HJK)BJJSS=SIGN(HJK,BJJSS) IF(ABS(BKKSS).GT.HJK)BKKSS=SIGN(HJK,BKKSS) IF(ABS(BXXSS).GT.HXX)BXXSS=SIGN(HXX,BXXSS) HX=3XKSS-BJJSS GX=BKXSS-BJJSS CALL QUAN(HX,4,5) CALL QUAN(GX,4,5) BOLLTC(1)=HX+BKXSS BOLLTC(2)=HX-BKXSS BOLLTC(3)=GX+BKXSS BOLLTC(4)=GX-BKXSS DO 16 II=1,4 CALL OTA(BOLLTC(II),II) REIJRN ENG						72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105
65							
70							
75							
80							
85	16						

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS 1 C3	DEF LINE 1	REFERENCES 42	85	2	31	84	89	80	81
VARIABLES	IN TYPE	RELOCATION	REFS						
1327 DUTLC	REAL	ARRAY	REFS						
1300 BJJ	REAL	C	REFS	24	67	70	DEFINED	65	
1503 BJJS	REAL	C	REFS	27	70	2*72	75	76	
			DEFINED	72					
1501 JKC	REAL	C	REFS	25	68	71	DEFINED	66	
1504 BKCS	REAL	C	REFS	29	74	2*73	79	88	81
			DEFINED	73					
1472 BLSS	REAL	C	REFS	21	64	65			
1476 BLSS	REAL	C	REFS	22	64	66			
540 BP41	REAL	C	REFS	14	54				
1506 BPSIS	REAL	C	REFS	30	62	66	DEFINED	59	
1482 BT41	REAL	C	REFS	16	59				
1505 BT4S	REAL	C	REFS	29	61	65	DEFINED	57	
141 BT42	REAL	C	REFS	15	57				
1507 JAK	REAL	C	REFS	23	60	59	DEFINED	59	
1502 BKXS	REAL	C	REFS	26	63	2*74	75	76	
			DEFINED	74					
0 C	REAL	ARRAY	REFS	3	*	5	6	7	9
			10	11	12	13	14	15	16
			18	19	20	21	22	23	24
			26	27	28	29	30	31	40
			REFS	17	52	55			
714 CASE	REAL	C	REFS	46	43	48	49		
1147 DER	REAL	C	REFS	47	47	51	52		
1334 GDIAS	REAL	C	REFS	73	84	82	DEFINED	76	
201 GA	REAL	C	REFS	8	2*72	2*73			
1545 HJK	REAL	C	REFS	5	41	42	DEFINED	41	43
1005 MO-D	REAL	C	REFS	77	74	30	DEFINED	75	
200 MK	REAL	C	REFS	11	2*74				
1371 MAX	REAL	C	REFS	14	2*74				
202 LI	INT-GER	C	REFS	2*84	DEFINED	33			
1355 UBIAS	REAL	C	REFS	9	54				
1326 UBIAS	REAL	C	REFS	10	44	34			
1717 T	REAL	C	REFS	20	59	52			
1533 TUV	REAL	C	REFS	6	50	52			
715 TARY	REAL	C	REFS	49	54				
715 TARZ	REAL	C	REFS	13	50	46	52		
822 MAMU	REAL	C	REFS	12	45	48	55		
826 MAMK	REAL	C	REFS	13	45	48	55		
250 M3	REAL	C	REFS	63	DEFINED	47	51	52	
257 M3	REAL	C	REFS	64	DEFINED	49	54	55	
EXTERNALS	TYPE	BACK	REFERENCES						
ATJ	2	2	44	68	61	62			
LTA	2	2	34	63	59	78	71		
MODJUN	3	3	46	77	73				
QUAN	3	3	57						

SUBROUTINE G3			74/74	OPT=1	FTN 4.2+7.355	07/07/75	11.06.53.	PAGE 4
INLINE FUNCTIONS			TYPE	ARGS	DEF LINE	REFERENCES		
ABS	REAL	1	INTRIN		72	73	74	
SIGN	REAL	2	INTRIN		72	73	74	
STATEMENT LABELS			DEF LINE	REFERENCES				
35			53	50				
43			56	23				
0			84	93				
LJOPS LABEL			INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS	
131	16		11	83	84	63		
COMMON BLOCKS			LENGTH	MEMBERS	- BIAS NAME(LENGTH)			
C			3830		0 C	133307		
EQUIV CLASSES			LENGTH	MEMBERS	- BIAS NAME(LENGTH)			
C			3830					
				352 BPH1	(1)	353 BT42	(1)	354 APS1
				402 MAMQ	(1)	405 MAMR	(1)	450 GAGE
				461 TKR2	(1)	462 TKR3	(1)	926 BLOSS
				930 BRSS	(1)	933 BBELG	(1)	939 T04
				860 G31AS	(1)	869 HJK	(1)	877 DBIAS
				978 R31AS	(1)	979 BKR	(1)	930 RJJ
				881 BKK	(1)	882 BKKSS	(1)	933 RJJSS
				884 BKKSS	(1)	885 BHTS	(1)	936 APSIS
				889 HXX	(1)	1999 T	(1)	2553 DER
				3461 MOLD	(1)			

STATISTICS
PROGRAM LENGTH 2633 179
CM Labeled COMMON LENGTH 75668 3830

467

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	20
3 QUAN	1	11	
VARIABLES	SN	TYPE	RELOCATION
3270 BIT	REAL	ARRAY C	REFS 18
0 C	REAL	ARRAY C	REFS 2
0 I	INTEGER	F.P.	REFS 16
0 J	INTEGER	F.P.	REFS 15
3472 REF	REAL	ARRAY C	REFS 3
40 SIS	REAL		REFS 4
0 XIN	REAL	F.P.	REFS 13
			REFS 12
			REFS 14
			REFS 15
			REFS 16
			REFS 17
			REFS 18
			REFS 19

FILE NAMES	MODE	WRITES	16
TAPED	FMT		

LINE FUNCTIONS	TYPE	WRDS	DEF LINE	REFERENCES
ASJ	REAL	1	INTRIN	14
AMJO	REAL	2	INTRIN	18

STATEMENT LABELS	DEF LINE	REFERENCES
21 10	18	15
40 14	17	15
0 100	INACTIVE	19

COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3830	0 C	(3830)

ENTRY CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3830	3386 REF	(28)

STATISTICS	PROGRAM LENGTH	478	39
COMMON LENGTH	73668		3830

3414 BIT (28)

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SUBROUTINE ATD(XIN,J)
COMMON /C/ C(3838)
DIMENSION REF(5),BIT(5)
EQUIVALENCE (C(3443),REF)
EQUIVALENCE (C(3448),BIT)
REF(1) IS WLMQ
REF(2) IS WLMR
REF(3) IS BXX
REF(4) IS BTMS
REF(5) IS BPSIS
SIG = 1.
IF (XIN.LT.0.) SIG = -1.
XIN = ABS(XIN)
IF (XIN.LT.REF(1)) GO TO 10
WRITE(6,14) C(2000),XIN,J
FORMAT(* ATD *,2E20.10,15)
10 XIN=XIN-AMOD(XIN,BIT(J))
XIN=SIG*XIN
RETURN
END

```

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES				
3 ATD	1	19				
VARIABLES	SN	TYPE	RELOCATION	REFS	DEF LINE	REFERENCES
3587 DIT	0	REAL	0	REFS	3	17
0 C	0	REAL	0	REFS	2	5
0 J	0	INTEGER	0	REFS	14	17
3502 REF	0	REAL	0	REFS	14	15
41 SIS	0	REAL	0	REFS	10	17
0 AIN	0	REAL	0	REFS	12	15
	0	F.P.	0	REFS	13	17
	0	F.P.	0	REFS	13	17
	0	DEFINED	0	REFS	1	17

FILE NAMES	MODE	WRITES	15
TAB00	FMT		
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE REFERENCES
355	REAL	1 INTRIN	13
ADD	REAL	2 INTRIN	17
STATEMENT LABELS		DEF LINE	REFERENCES
17 10		17	14
33 17		16	15
0 100	FMT		
	INACTIVE		10

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)
COMMON CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	3842 REF (5)

STATISTICS	PROGRAM LENGTH	CM LABEL-ED COMMON LENGTH
	428	34
	74663	3830

SUBROUTINE DTA	74/74	OPT=1	FTN **2+7+355	07/07/76	11.06.59.	PAGE	1
SUBROUTINE DTAXIN,J)							
		COMMON /Z/ C(1830)		C3	LABCOM	196	
		DIMENSION REF(4),BIT(1)		C3		197	
		EQUIVALENCE (C(1830),REF)		C3		198	
		EQUIVALENCE (C(1830),BIT)		C3		199	
5	C	REF(1 THRU 4) IS SUELC(1 THRU 4)		C3		200	
		SIG=1.		C3		201	
		IF(XIN.LT.0.)SIG=-1.		C3		202	
		XIN=ABS(XIN)		C3		203	
10		IF(XIN.LT.REF(J))GO TO 10		C3		204	
		WRITE(6,1410)(2000),XIN,J		C3		205	
	14	FORMAT(' D10A *2E20.10,15)		C3		206	
		XIN=XIN/J		C3		207	
		GO TO 100		C3		208	
15	10	XIN=XIN-AMOD(XIN,BIT(J))		C3		209	
	100	XIN=SIG*XIN		C3		210	
		RETURN		C3		211	
		END		C3		212	
				C3		213	

SYMBOLIC REFERENCE MAP (R-S)

ENTRY POINTS	DEF LINE	REFERENCES				
3 JTA	1	17				
VARIABLES	SN	TYPE	RELOCATION	REFS	DEF	DEFINED
3000 BIT		REAL	ARRAY C	2	15	
0 C		REAL	ARRAY C	11	15	
0 C		INTEGER	F.P.	10	13	
3574 REF		REAL	ARRAY C	3	10	
40 S15		REAL		16	7	
0 XIV		REAL	F.P.	8	10	2*15
				DEFIN	13	15

FILE NAMES	MODE	4RITES	11
TAPED	FMT		
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE REFERENCES
333	REAL	1 INTRIN	9
AMDO	REAL	2 INTRIN	15
STATEMENT LABELS		DEF LINE REFERENCES	
22 10		15	10
20 14		12	11
27 103	FMT		

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)
EQUIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	3452 817 (14)

STATISTICS
PROGRAM LENGTH 73 39
COMMON LENGTH 73063 3830

LINE	CODE	STATEMENT	OPERANDS	OPERATION	REGISTER	VALUE
5	C	COMMON C(1630)			C4	
	C	DIMENSION IPL(100), ISNOX(40)			C4	
	C	C**INFUT DATA			C4	
	C	EQUIVALENCE (C(1143),DOELTL)			C4	
	C	EQUIVALENCE (C(11407),DOELT)			C4	
10	C	EQUIVALENCE (C(13634), ISNOX), (C(13512), I3512)			C4	
	C	DIMENSION BOELT(4)			C4	
	C	EQUIVALENCE (C(11103),BOELT1)			C4	
	C	EQUIVALENCE (C(11107),BOELT2)			C4	
	C	EQUIVALENCE (C(11111),BOELT3)			C4	
	C	EQUIVALENCE (C(11151),BOELT4)			C4	
	C	EQUIVALENCE (C(11101),FELECB)			C4	
	C	EQUIVALENCE (C(11102),FELECC3)			C4	
	C	EQUIVALENCE (C(11105),FELECR3)			C4	
	C	EQUIVALENCE (C(11106),FMECH3)			C4	
	C	EQUIVALENCE (C(11109),FMECHQ3)			C4	
	C	EQUIVALENCE (C(11101),FMECHR3)			C4	
	C	EQUIVALENCE (C(11254), DELT8)			C4	
	C	EQUIVALENCE (C(11255), DELT8)			C4	
	C	EQUIVALENCE (C(11256), DELT8)			C4	
	C	EQUIVALENCE (C(11257), DELT8)			C4	
	C	EQUIVALENCE (C(11258), DELT8)			C4	
	C	EQUIVALENCE (C(11259), DELT8)			C4	
	C	EQUIVALENCE (C(11260), DELT8)			C4	
	C	EQUIVALENCE (C(11261), DELT8)			C4	
	C	EQUIVALENCE (C(11262), DELT8)			C4	
	C	EQUIVALENCE (C(11263), DELT8)			C4	
	C	EQUIVALENCE (C(11264), DELT8)			C4	
	C	EQUIVALENCE (C(11265), DELT8)			C4	
	C	EQUIVALENCE (C(11266), DELT8)			C4	
	C	EQUIVALENCE (C(11267), DELT8)			C4	
	C	EQUIVALENCE (C(11268), DELT8)			C4	
	C	EQUIVALENCE (C(11269), DELT8)			C4	
	C	EQUIVALENCE (C(11270), DELT8)			C4	
	C	EQUIVALENCE (C(11271), DELT8)			C4	
	C	EQUIVALENCE (C(11272), DELT8)			C4	
	C	EQUIVALENCE (C(11273), DELT8)			C4	
	C	EQUIVALENCE (C(11274), DELT8)			C4	
	C	EQUIVALENCE (C(11275), DELT8)			C4	
	C	EQUIVALENCE (C(11276), DELT8)			C4	
	C	EQUIVALENCE (C(11277), DELT8)			C4	
	C	EQUIVALENCE (C(11278), DELT8)			C4	
	C	EQUIVALENCE (C(11279), DELT8)			C4	
	C	EQUIVALENCE (C(11280), DELT8)			C4	
	C	EQUIVALENCE (C(11281), DELT8)			C4	
	C	EQUIVALENCE (C(11282), DELT8)			C4	
	C	EQUIVALENCE (C(11283), DELT8)			C4	
	C	EQUIVALENCE (C(11284), DELT8)			C4	
	C	EQUIVALENCE (C(11285), DELT8)			C4	
	C	EQUIVALENCE (C(11286), DELT8)			C4	
	C	EQUIVALENCE (C(11287), DELT8)			C4	
	C	EQUIVALENCE (C(11288), DELT8)			C4	
	C	EQUIVALENCE (C(11289), DELT8)			C4	
	C	EQUIVALENCE (C(11290), DELT8)			C4	
	C	EQUIVALENCE (C(11291), DELT8)			C4	
	C	EQUIVALENCE (C(11292), DELT8)			C4	
	C	EQUIVALENCE (C(11293), DELT8)			C4	
	C	EQUIVALENCE (C(11294), DELT8)			C4	
	C	EQUIVALENCE (C(11295), DELT8)			C4	
	C	EQUIVALENCE (C(11296), DELT8)			C4	
	C	EQUIVALENCE (C(11297), DELT8)			C4	
	C	EQUIVALENCE (C(11298), DELT8)			C4	
	C	EQUIVALENCE (C(11299), DELT8)			C4	
	C	EQUIVALENCE (C(11300), DELT8)			C4	
	C	EQUIVALENCE (C(11301), DELT8)			C4	

SUBROUTINE C41	7/4/74	OPT=1	FTN ++2+7+353	07/07/75	11-06-59.	PAGE	2
10	CONTINUE						
60	ENTRY A11						59
	DEL18 = FELECB + FMECHB						58
	DEL19 = FELECB + FMECHB						51
	DEL18 = FELECB + FMECHB						52
	DEL11 = -80P + 30Q - 80R						58
	DEL12 = -80P + 80Q - 80R						54
65	DEL13 = 80P + 80Q - 80R						55
	DEL14 = 80P + 80Q - 80R						56
	DEL11 = 80EL11 - DEL18 + DEL19 - DEL18						57
	DEL12 = 80EL12 - DEL18 + DEL19 - DEL18						58
	DEL13 = 80EL13 + DEL18 + DEL19 - DEL18						59
70	DEL14 = 80EL14 + DEL18 + DEL19 - DEL18						70
	RETURN						71
	END						72
	C** HELFIRE SIMPLIFIED ACTUATOR MODEL						73
	C+++++ NON - LINEAR MODEL +++++						74
75	C						75
							76

SYMBOLIC REFERENCE MAP (R=3)

SUBROUTINE CMI				74774	OPT=1	FTN **2474355	07/07/75	11.06.59.	PAGE	4
EQUIV CLASSES		LENGTH	MEMBERS - BIAS NAME(LENGTH)							
C	C	3830	1100 FELECR (11)							
			1104 FELECR (11)							
			1108 FECHOR (11)							
			1114 BDELT (11)							
			1143 BDELT (11)							
			1232 BDR (11)							
			1255 BDELT (11)							
			3511 B3512 (11)							
			1101 FELECR (11)							
			1105 FECHOR (11)							
			1109 FECHOR (11)							
			1113 OPTACT (11)							
			1230 BDR (11)							
			1254 BDELT (11)							
			2500 N (11)							
			3533 ISNOR (100)							
STATISTICS										
PROGRAM LENGTH		1158	77							
CM LABELED COMMON LENGTH		73668	3830							

AD-A032 048

ARMY MISSILE RESEARCH DEVELOPMENT AND ENGINEERING LAB--ETC F/G 16/4
THAD T-7 MISSILE MONTE-CARLO TERMINAL HOMING SIMULATION UTILIZI--ETC(U)
JUL 76 C L LEWIS, W R HOOKER, A W LEE

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RG-7T-2

NL

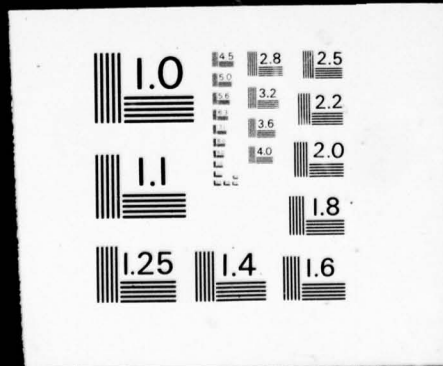
6 OF 7
ADA032048



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7

ADA032048



		SUBROUTINE C*	C*	77
		COMMON /C/ C(J839)	C*	78
		DIMENSION BDELTD(4),BDELT(4),BDELTG(4)	C*	79
		C**INPUT DATA	C*	80
		EQUIVALENCE (C(1143),BDELT)	C*	81
		EQUIVALENCE (C(1144),BDELT)	C*	82
		C	C*	83
		C**INPUTS FROM OTHER MODULES	C*	84
		EQUIVALENCE (C(1261),BDELT)	C*	85
		EQUIVALENCE (C(1254), DELTB)	C*	86
		EQUIVALENCE (C(1255),DELTQB)	C*	87
		EQUIVALENCE (C(1256),DELTQB)	C*	88
		C**STATE VARIABLE OUTPUTS	C*	89
		BDELTG(1) = BDELTG(1) - DELTA + DELTQB - DELTRB	C*	90
		BDELTG(2) = BDELTG(2) - DELTA + DELTQB - DELTRB	C*	91
		BDELTG(3) = BDELTG(3) - DELTA + DELTQB - DELTRB	C*	92
		BDELTG(4) = BDELTG(4) - DELTA + DELTQB - DELTRB	C*	93
		BDELTG(1)=C(1143)	C*	94
		BDELTG(2)=C(1147)	C*	95
		BDELTG(3)=C(1111)	C*	96
		BDELTG(4)=C(1115)	C*	97
		C	C*	98
		C**ACTUATOR DYNAMICS	C*	99
		DO 30 I=1,4	C*	100
		IFABS(BDELT(I)) .GT. 20.)BDELT(I)=SIGN(20.,BDELT(I))	C*	101
		31 BDELTG(I)=BDELT(I)-BDELT(I)*H	C*	102
		IFABS(BDELTG(I)).GT.WDELT)BDELTG(I)=SIGN(WDELT,BDELTG(I))	C*	103
		32 CONTINUE	C*	104
		30 CONTINUE	C*	105
		C	C*	106
		C(1103) = BDELT(1)	C*	107
		C(1107) = BDELT(2)	C*	108
		C(1111) = BDELT(3)	C*	109
		C(1115) = BDELT(4)	C*	110
		C	C*	111
		C**OUTPUT DERIVATIVES OF STATE VARIABLES TO INTEGRATION	C*	112
		C(1109) = BDELTG(1)	C*	113
		C(1104) = BDELTG(2)	C*	114
		C(1108) = BDELTG(3)	C*	115
		C(1112) = BDELTG(4)	C*	116
		C	C*	117
		RETURN	C*	118
		END	C*	119
			C*	120
			C*	121

Line	Code	Text	Address
5	C	***INPUT DATA	
10		EQUIVALENCE (C(1120),Z1)	05
		EQUIVALENCE (C(1124),Z2)	05
		EQUIVALENCE (C(1128),Z3)	05
		EQUIVALENCE (C(1132),Z4)	05
		EQUIVALENCE (C(1136),Z5)	05
		EQUIVALENCE (C(1140),Z6)	05
15		EQUIVALENCE (C(1103),ZDEL1)	05
		EQUIVALENCE (C(1107),ZDEL2)	05
		EQUIVALENCE (C(1111),ZDEL3)	05
		EQUIVALENCE (C(1115),ZDEL4)	05
		EQUIVALENCE (C(1119),ZDEL5)	05
		EQUIVALENCE (C(1123),ZDEL6)	05
20		EQUIVALENCE (C(1127),ZDEL7)	05
		EQUIVALENCE (C(1131),ZDEL8)	05
		EQUIVALENCE (C(1135),ZDEL9)	05
		EQUIVALENCE (C(1139),ZDEL10)	05
25		DATA Z1/Z2,Z3,Z4,Z5,Z6,Z7,Z8,Z9,Z10,Z11,Z12,Z13,Z14,Z15,Z16,Z17,Z18,Z19,Z20,Z21,Z22,Z23,Z24,Z25,Z26,Z27,Z28,Z29,Z30,Z31,Z32,Z33,Z34,Z35,Z36,Z37,Z38,Z39,Z40,Z41,Z42,Z43,Z44,Z45,Z46,Z47,Z48,Z49,Z50,Z51,Z52,Z53,Z54,Z55,Z56,Z57,Z58,Z59,Z60	05
30		EQUIVALENCE (C(1103),ZDEL1)	05
		EQUIVALENCE (C(1107),ZDEL2)	05
		EQUIVALENCE (C(1111),ZDEL3)	05
		EQUIVALENCE (C(1115),ZDEL4)	05
		EQUIVALENCE (C(1119),ZDEL5)	05
		EQUIVALENCE (C(1123),ZDEL6)	05
		EQUIVALENCE (C(1127),ZDEL7)	05
		EQUIVALENCE (C(1131),ZDEL8)	05
		EQUIVALENCE (C(1135),ZDEL9)	05
		EQUIVALENCE (C(1139),ZDEL10)	05
		EQUIVALENCE (C(1143),ZDEL11)	05
		EQUIVALENCE (C(1147),ZDEL12)	05
		EQUIVALENCE (C(1151),ZDEL13)	05
		EQUIVALENCE (C(1155),ZDEL14)	05
		EQUIVALENCE (C(1159),ZDEL15)	05
		EQUIVALENCE (C(1163),ZDEL16)	05
		EQUIVALENCE (C(1167),ZDEL17)	05
		EQUIVALENCE (C(1171),ZDEL18)	05
		EQUIVALENCE (C(1175),ZDEL19)	05
		EQUIVALENCE (C(1179),ZDEL20)	05
		EQUIVALENCE (C(1183),ZDEL21)	05
		EQUIVALENCE (C(1187),ZDEL22)	05
		EQUIVALENCE (C(1191),ZDEL23)	05
		EQUIVALENCE (C(1195),ZDEL24)	05
		EQUIVALENCE (C(1199),ZDEL25)	05
		EQUIVALENCE (C(1203),ZDEL26)	05
		EQUIVALENCE (C(1207),ZDEL27)	05
		EQUIVALENCE (C(1211),ZDEL28)	05
		EQUIVALENCE (C(1215),ZDEL29)	05
		EQUIVALENCE (C(1219),ZDEL30)	05
		EQUIVALENCE (C(1223),ZDEL31)	05
		EQUIVALENCE (C(1227),ZDEL32)	05
		EQUIVALENCE (C(1231),ZDEL33)	05
		EQUIVALENCE (C(1235),ZDEL34)	05
		EQUIVALENCE (C(1239),ZDEL35)	05
		EQUIVALENCE (C(1243),ZDEL36)	05
		EQUIVALENCE (C(1247),ZDEL37)	05
		EQUIVALENCE (C(1251),ZDEL38)	05
		EQUIVALENCE (C(1255),ZDEL39)	05
		EQUIVALENCE (C(1259),ZDEL40)	05
		EQUIVALENCE (C(1263),ZDEL41)	05
		EQUIVALENCE (C(1267),ZDEL42)	05
		EQUIVALENCE (C(1271),ZDEL43)	05
		EQUIVALENCE (C(1275),ZDEL44)	05
		EQUIVALENCE (C(1279),ZDEL45)	05
		EQUIVALENCE (C(1283),ZDEL46)	05
		EQUIVALENCE (C(1287),ZDEL47)	05
		EQUIVALENCE (C(1291),ZDEL48)	05
		EQUIVALENCE (C(1295),ZDEL49)	05
		EQUIVALENCE (C(1299),ZDEL50)	05
		EQUIVALENCE (C(1303),ZDEL51)	05
		EQUIVALENCE (C(1307),ZDEL52)	05
		EQUIVALENCE (C(1311),ZDEL53)	05
		EQUIVALENCE (C(1315),ZDEL54)	05
		EQUIVALENCE (C(1319),ZDEL55)	05
		EQUIVALENCE (C(1323),ZDEL56)	05
		EQUIVALENCE (C(1327),ZDEL57)	05
		EQUIVALENCE (C(1331),ZDEL58)	05
		EQUIVALENCE (C(1335),ZDEL59)	05
		EQUIVALENCE (C(1339),ZDEL60)	05
		EQUIVALENCE (C(1343),ZDEL61)	05
		EQUIVALENCE (C(1347),ZDEL62)	05
		EQUIVALENCE (C(1351),ZDEL63)	05
		EQUIVALENCE (C(1355),ZDEL64)	05
		EQUIVALENCE (C(1359),ZDEL65)	05
		EQUI	

SYMBOLIC REFERENCE MAP (4=3)

ENTRY POINTS	DEF LINE	REFERENCES		
1 C51	1	56		
VARIABLES	SN	TYPE	RELOCATION	REFS
2110 BDELTA	REAL	C	3	14
2112 BDELTA	REAL	C	15	15
2114 BDELTA	REAL	C	16	16
2116 BDELTA	REAL	C	17	17
2118 BDELTA	REAL	C	18	18
2120 BDELTA	REAL	C	19	19
2122 BDELTA	REAL	C	20	20
2124 BDELTA	REAL	C	21	21
2126 BDELTA	REAL	C	22	22
2128 BDELTA	REAL	C	23	23
2130 BDELTA	REAL	C	24	24
2132 BDELTA	REAL	C	25	25
2134 BDELTA	REAL	C	26	26
2136 BDELTA	REAL	C	27	27
2138 BDELTA	REAL	C	28	28
2140 BDELTA	REAL	C	29	29
2142 BDELTA	REAL	C	30	30
2144 BDELTA	REAL	C	31	31
2146 BDELTA	REAL	C	32	32
2148 BDELTA	REAL	C	33	33
2150 BDELTA	REAL	C	34	34
2152 BDELTA	REAL	C	35	35
2154 BDELTA	REAL	C	36	36
2156 BDELTA	REAL	C	37	37
2158 BDELTA	REAL	C	38	38
2160 BDELTA	REAL	C	39	39
2162 BDELTA	REAL	C	40	40
2164 BDELTA	REAL	C	41	41
2166 BDELTA	REAL	C	42	42
2168 BDELTA	REAL	C	43	43
2170 BDELTA	REAL	C	44	44
2172 BDELTA	REAL	C	45	45
2174 BDELTA	REAL	C	46	46
2176 BDELTA	REAL	C	47	47
2178 BDELTA	REAL	C	48	48
2180 BDELTA	REAL	C	49	49
2182 BDELTA	REAL	C	50	50
2184 BDELTA	REAL	C	51	51
2186 BDELTA	REAL	C	52	52
2188 BDELTA	REAL	C	53	53
2190 BDELTA	REAL	C	54	54
2192 BDELTA	REAL	C	55	55
2194 BDELTA	REAL	C	56	56
2196 BDELTA	REAL	C	57	57
2198 BDELTA	REAL	C	58	58
2200 BDELTA	REAL	C	59	59
2202 BDELTA	REAL	C	60	60
2204 BDELTA	REAL	C	61	61
2206 BDELTA	REAL	C	62	62
2208 BDELTA	REAL	C	63	63
2210 BDELTA	REAL	C	64	64
2212 BDELTA	REAL	C	65	65
2214 BDELTA	REAL	C	66	66
2216 BDELTA	REAL	C	67	67
2218 BDELTA	REAL	C	68	68
2220 BDELTA	REAL	C	69	69
2222 BDELTA	REAL	C	70	70
2224 BDELTA	REAL	C	71	71
2226 BDELTA	REAL	C	72	72
2228 BDELTA	REAL	C	73	73
2230 BDELTA	REAL	C	74	74
2232 BDELTA	REAL	C	75	75
2234 BDELTA	REAL	C	76	76
2236 BDELTA	REAL	C	77	77
2238 BDELTA	REAL	C	78	78
2240 BDELTA	REAL	C	79	79
2242 BDELTA	REAL	C	80	80
2244 BDELTA	REAL	C	81	81
2246 BDELTA	REAL	C	82	82
2248 BDELTA	REAL	C	83	83
2250 BDELTA	REAL	C	84	84
2252 BDELTA	REAL	C	85	85
2254 BDELTA	REAL	C	86	86
2256 BDELTA	REAL	C	87	87
2258 BDELTA	REAL	C	88	88
2260 BDELTA	REAL	C	89	89
2262 BDELTA	REAL	C	90	90
2264 BDELTA	REAL	C	91	91
2266 BDELTA	REAL	C	92	92
2268 BDELTA	REAL	C	93	93
2270 BDELTA	REAL	C	94	94
2272 BDELTA	REAL	C	95	95
2274 BDELTA	REAL	C	96	96
2276 BDELTA	REAL	C	97	97
2278 BDELTA	REAL	C	98	98
2280 BDELTA	REAL	C	99	99
2282 BDELTA	REAL	C	100	100
2284 BDELTA	REAL	C	101	101
2286 BDELTA	REAL	C	102	102
2288 BDELTA	REAL	C	103	103
2290 BDELTA	REAL	C	104	104
2292 BDELTA	REAL	C	105	105
2294 BDELTA	REAL	C	106	106
2296 BDELTA	REAL	C	107	107
2298 BDELTA	REAL	C	108	108
2300 BDELTA	REAL	C	109	109
2302 BDELTA	REAL	C	110	110
2304 BDELTA	REAL	C	111	111
2306 BDELTA	REAL	C	112	112
2308 BDELTA	REAL	C	113	113
2310 BDELTA	REAL	C	114	114
2312 BDELTA	REAL	C	115	115
2314 BDELTA	REAL	C	116	116
2316 BDELTA	REAL	C	117	117
2318 BDELTA	REAL	C	118	118
2320 BDELTA	REAL	C	119	119
2322 BDELTA	REAL	C	120	120
2324 BDELTA	REAL	C	121	121
2326 BDELTA	REAL	C	122	122
2328 BDELTA	REAL	C	123	123
2330 BDELTA	REAL	C	124	124
2332 BDELTA	REAL	C	125	125
2334 BDELTA	REAL	C	126	126
2336 BDELTA	REAL	C	127	127
2338 BDELTA	REAL	C	128	128
2340 BDELTA	REAL	C	129	129
2342 BDELTA	REAL	C	130	130
2344 BDELTA	REAL	C	131	131
2346 BDELTA	REAL	C	132	132
2348 BDELTA	REAL	C	133	133
2350 BDELTA	REAL	C	134	134
2352 BDELTA	REAL	C	135	135
2354 BDELTA	REAL	C	136	136
2356 BDELTA	REAL	C	137	137
2358 BDELTA	REAL	C	138	138
2360 BDELTA	REAL	C	139	139
2362 BDELTA	REAL	C	140	140
2364 BDELTA	REAL	C	141	141
2366 BDELTA	REAL	C	142	142
2368 BDELTA	REAL	C	143	143
2370 BDELTA	REAL	C	144	144
2372 BDELTA	REAL	C	145	145
2374 BDELTA	REAL	C	146	146
2376 BDELTA	REAL	C	147	147
2378 BDELTA	REAL	C	148	148
2380 BDELTA	REAL	C	149	149
2382 BDELTA	REAL	C	150	150
2384 BDELTA	REAL	C	151	151
2386 BDELTA	REAL	C	152	152
2388 BDELTA	REAL	C	153	153
2390 BDELTA	REAL	C	154	154
2392 BDELTA	REAL	C	155	155
2394 BDELTA	REAL	C	156	156
2396 BDELTA	REAL	C	157	157
2398 BDELTA	REAL	C	158	158
2400 BDELTA	REAL	C	159	159
2402 BDELTA	REAL	C	160	160
2404 BDELTA	REAL	C	161	161
2406 BDELTA	REAL	C	162	162
2408 BDELTA	REAL	C	163	163
2410 BDELTA	REAL	C	164	164
2412 BDELTA	REAL	C	165	165
2414 BDELTA	REAL	C	166	166
2416 BDELTA	REAL	C	167	167
2418 BDELTA	REAL	C	168	168
2420 BDELTA	REAL	C	169	169
2422 BDELTA	REAL	C	170	170
2424 BDELTA	REAL	C	171	171
2426 BDELTA	REAL	C	172	172
2428 BDELTA	REAL	C	173	173
2430 BDELTA	REAL	C	174	174
2432 BDELTA	REAL	C	175	175
2434 BDELTA	REAL	C	176	176
2436 BDELTA	REAL	C	177	177
2438 BDELTA	REAL	C	178	178
2440 BDELTA	REAL	C	179	179
2442 BDELTA	REAL	C	180	180
2444 BDELTA	REAL	C	181	181
2446 BDELTA	REAL	C	182	182
2448 BDELTA	REAL	C	183	183
2450 BDELTA	REAL	C	184	184
2452 BDELTA	REAL	C	185	185
2454 BDELTA	REAL	C	186	186
2456 BDELTA	REAL	C	187	187
2458 BDELTA	REAL	C	188	188
2460 BDELTA	REAL	C	189	189
2462 BDELTA	REAL	C	190	190
2464 BDELTA	REAL	C	191	191
2466 BDELTA	REAL	C	192	192
2468 BDELTA	REAL	C	193	193
2470 BDELTA	REAL	C	194	194
2472 BDELTA	REAL	C	195	195
2474 BDELTA	REAL	C	196	196
2476 BDELTA	REAL	C	197	197
2478 BDELTA	REAL	C	198	198
2480 BDELTA	REAL	C	199	199
2482 BDELTA	REAL	C	200	200
2484 BDELTA	REAL	C	201	201
2486 BDELTA	REAL	C	202	202
2488 BDELTA	REAL	C	203	203
2490 BDELTA	REAL	C	204	204
2492 BDELTA	REAL	C	205	205
2494 BDELTA	REAL	C	206	206
2496 BDELTA	REAL	C	207	207
2498 BDELTA	REAL	C	208	208
2500 BDELTA	REAL	C	209	209
2502 BDELTA	REAL	C	210	210
2504 BDELTA	REAL	C	211	211
2506 BDELTA	REAL	C	212	212
2508 BDELTA	REAL	C	213	213
2510 BDELTA	REAL	C	214	214
2512 BDELTA	REAL	C	215	215
2514 BDELTA	REAL	C	216	216
2516 BDELTA	REAL	C	217	217
2518 BDELTA	REAL	C	218	218
2520 BDELTA	REAL	C	219	219
2522 BDELTA	REAL	C	220	220
2524 BDELTA	REAL	C	221	221
2526 BDELTA	REAL	C	222	222
2528 BDELTA	REAL	C	223	223
2530 BDELTA	REAL	C	224	224
2532 BDELTA	REAL	C	225	225
2534 BDELTA	REAL	C	226	226
2536 BDELTA	REAL	C	227	227
2538 BDELTA	REAL	C	228	228
2540 BDELTA	REAL	C	229	229
2542 BDELTA	REAL	C	230	230
2544 BDELTA	REAL	C	231	231
2546 BDELTA	REAL	C	232	232
2548 BDELTA	REAL	C	233	233
2550 BDELTA	REAL	C	234	234
2552 BDELTA	REAL	C	235	235
2554 BDELTA	REAL	C	236	236
2556 BDELTA	REAL	C	237	237
2558 BDELTA	REAL	C	238	238
2560 BDELTA	REAL	C	239	239
2562 BDELTA	REAL	C	240	240
2564 BDELTA	REAL	C	241	241
2566 BDELTA	REAL	C	242	242
2568 BDELTA	REAL	C	243	243
2570 BDELTA	REAL	C	244	244
2572 BDELTA	REAL	C	245	245
2574 BDELTA	REAL	C	246	246
2576 BDELTA	REAL	C	247	247
2578 BDELTA	REAL	C	248	248
2580 BDELTA	REAL	C	249	249
2582 BDELTA	REAL	C	250	250
2584 BDELTA	REAL	C	251	251
2586 BDELTA	REAL	C	252	252
2588 BDELTA	REAL	C	253	253
2590 BDELTA	REAL	C	254	254
2592 BDELTA	REAL	C	255	255
2594 BDELTA	REAL	C	256	256
2596 BDELTA	REAL	C	257	257
2598 BDELTA	REAL	C	258	258
2600 BDELTA	REAL	C	259	259
2602 BDELTA	REAL	C	260	260
2604 BDELTA	REAL	C	261	261
2606 BDELTA	REAL	C	262	262
2608 BDELTA	REAL	C	263	263
2610 BDELTA	REAL	C	264	264
2612 BDELTA	REAL	C	265	265
2614 BDELTA	REAL	C	266	266
2616 BDELTA	REAL	C	267	267
2618 BDELTA	REAL	C	268	268
2620 BDELTA	REAL	C	269	269
2622 BDELTA	REAL	C	270	270
2624 BDELTA	REAL	C	271	271
2626 BDELTA	REAL	C	272	272
2628 BDELTA	REAL	C	273	273
2630 BDELTA	REAL	C	274	274
2632 BDELTA	REAL	C	275	275
2634 BDELTA	REAL	C	276	276
2636 BDELTA	REAL	C	277	277
2638 BDELTA	REAL	C	278	278
2640 BDELTA	REAL	C	279	279
2642 BDELTA	REAL	C	280	280
2644 BDELTA	REAL	C	281	281
2646 BDELTA	REAL	C	282	282
2648 BDELTA	REAL	C	283	283
2650 BDELTA	REAL	C	284	284
2652 BDELTA	REAL	C	285	285
2654 BDELTA	REAL	C	286	286
2656 BDELTA				

SYMBOLIC REFERENCE MAP (R=J)

ENTRY POINTS	DEF LINE	REFERENCES
I C5	I	C8
VARIABLES	SN TYPE	RELOCATION
197 A1	REAL	REFS 62 63 66 DEFINED 64
174 B0ELT	REAL	REFS 51 56 71 72 73
1927 B0ELTC	REAL	REFS 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000

SUBROUTINE C5 74/74 OPT=1 FTN **2+7+355 07/07/76 11.07.05. PAGE 4

STATEMENT LABELS	DEF LINE	REFERENCES
50 3	57	58
62 4	58	56
64 5	60	59
0 50	INACTIVE	57
0 50	70	51

LOOPS LABEL	INDEX	PROMPT	LENGTH	PROPERTIES
47 30	51 70	473	OPT	

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)

CTIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	203 VMACH (1) 1123 ZN (4) 1135 MN (4) 1141 BDR (1)
		855 BDELTC (4) 1127 M1 (4) 1139 OPTACT (1) 1142 BDR (1)
		1119 G1 (4) 1131 G2 (4) 1140 3DP (1) 1146 HDEL (1)

STATISTICS	PROGRAM LENGTH	CM LABELED COMMON LENGTH	2408	160
		73668	3830	

SUBROUTINE G4	74/74	OPT=1	FTV 1.2074355	07/07/76	11.07.07.	PAGE	1
5	SUBROUTINE G4						
10	C*** THIS IS A SUBROUTINE (NOT A MODULE) CALLED BY STAGE 1 **						
15	C*** STOPS PROGRAM AND COMPUTES MISS DISTANCE						
20	C***						
25	COMMON /C/ C(3830)						
30	100 FORMAT(10,17N MISS DISTANCE = ,1PE15.7)						
35	200 FORMAT(10, 8X,0HROELX = ,1PE15.7, 8X,0HROELZ = ,1PE15.7,						
40	300 FORMAT(10,40X,0HRYFP = ,1PE15.7, 8X,0HRRZF = ,1PE15.7)						
45	EQUIVALENCE (C(1357),BGAMH)						
50	EQUIVALENCE (C(1358),BGAMH)						
55	EQUIVALENCE (C(1359),BGAMH)						
60	EQUIVALENCE (C(1360),BGAMH)						
65	EQUIVALENCE (C(1361),BGAMH)						
70	EQUIVALENCE (C(1362),BGAMH)						
75	EQUIVALENCE (C(1363),BGAMH)						
80	EQUIVALENCE (C(1364),BGAMH)						
85	EQUIVALENCE (C(1365),BGAMH)						
90	EQUIVALENCE (C(1366),BGAMH)						
95	EQUIVALENCE (C(1367),BGAMH)						
100	EQUIVALENCE (C(1368),BGAMH)						
105	EQUIVALENCE (C(1369),BGAMH)						
110	EQUIVALENCE (C(1370),BGAMH)						
115	EQUIVALENCE (C(1371),BGAMH)						
120	EQUIVALENCE (C(1372),BGAMH)						
125	EQUIVALENCE (C(1373),BGAMH)						
130	EQUIVALENCE (C(1374),BGAMH)						
135	EQUIVALENCE (C(1375),BGAMH)						
140	EQUIVALENCE (C(1376),BGAMH)						
145	EQUIVALENCE (C(1377),BGAMH)						
150	EQUIVALENCE (C(1378),BGAMH)						
155	EQUIVALENCE (C(1379),BGAMH)						
160	EQUIVALENCE (C(1380),BGAMH)						
165	EQUIVALENCE (C(1381),BGAMH)						
170	EQUIVALENCE (C(1382),BGAMH)						
175	EQUIVALENCE (C(1383),BGAMH)						
180	EQUIVALENCE (C(1384),BGAMH)						
185	EQUIVALENCE (C(1385),BGAMH)						
190	EQUIVALENCE (C(1386),BGAMH)						
195	EQUIVALENCE (C(1387),BGAMH)						
200	EQUIVALENCE (C(1388),BGAMH)						
205	EQUIVALENCE (C(1389),BGAMH)						
210	EQUIVALENCE (C(1390),BGAMH)						
215	EQUIVALENCE (C(1391),BGAMH)						
220	EQUIVALENCE (C(1392),BGAMH)						
225	EQUIVALENCE (C(1393),BGAMH)						
230	EQUIVALENCE (C(1394),BGAMH)						
235	EQUIVALENCE (C(1395),BGAMH)						
240	EQUIVALENCE (C(1396),BGAMH)						
245	EQUIVALENCE (C(1397),BGAMH)						
250	EQUIVALENCE (C(1398),BGAMH)						
255	EQUIVALENCE (C(1399),BGAMH)						
260	EQUIVALENCE (C(1400),BGAMH)						
265	EQUIVALENCE (C(1401),BGAMH)						
270	EQUIVALENCE (C(1402),BGAMH)						
275	EQUIVALENCE (C(1403),BGAMH)						
280	EQUIVALENCE (C(1404),BGAMH)						
285	EQUIVALENCE (C(1405),BGAMH)						
290	EQUIVALENCE (C(1406),BGAMH)						
295	EQUIVALENCE (C(1407),BGAMH)						
300	EQUIVALENCE (C(1408),BGAMH)						
305	EQUIVALENCE (C(1409),BGAMH)						
310	EQUIVALENCE (C(1410),BGAMH)						
315	EQUIVALENCE (C(1411),BGAMH)						
320	EQUIVALENCE (C(1412),BGAMH)						
325	EQUIVALENCE (C(1413),BGAMH)						
330	EQUIVALENCE (C(1414),BGAMH)						
335	EQUIVALENCE (C(1415),BGAMH)						
340	EQUIVALENCE (C(1416),BGAMH)						
345	EQUIVALENCE (C(1417),BGAMH)						
350	EQUIVALENCE (C(1418),BGAMH)						
355	EQUIVALENCE (C(1419),BGAMH)						
360	EQUIVALENCE (C(1420),BGAMH)						
365	EQUIVALENCE (C(1421),BGAMH)						
370	EQUIVALENCE (C(1422),BGAMH)						
375	EQUIVALENCE (C(1423),BGAMH)						
380	EQUIVALENCE (C(1424),BGAMH)						
385	EQUIVALENCE (C(1425),BGAMH)						
390	EQUIVALENCE (C(1426),BGAMH)						
395	EQUIVALENCE (C(1427),BGAMH)						
400	EQUIVALENCE (C(1428),BGAMH)						
405	EQUIVALENCE (C(1429),BGAMH)						
410	EQUIVALENCE (C(1430),BGAMH)						
415	EQUIVALENCE (C(1431),BGAMH)						
420	EQUIVALENCE (C(1432),BGAMH)						
425	EQUIVALENCE (C(1433),BGAMH)						
430	EQUIVALENCE (C(1434),BGAMH)						
435	EQUIVALENCE (C(1435),BGAMH)						
440	EQUIVALENCE (C(1436),BGAMH)						
445	EQUIVALENCE (C(1437),BGAMH)						
450	EQUIVALENCE (C(1438),BGAMH)						
455	EQUIVALENCE (C(1439),BGAMH)						
460	EQUIVALENCE (C(1440),BGAMH)						
465	EQUIVALENCE (C(1441),BGAMH)						
470	EQUIVALENCE (C(1442),BGAMH)						
475	EQUIVALENCE (C(1443),BGAMH)						
480	EQUIVALENCE (C(1444),BGAMH)						
485	EQUIVALENCE (C(1445),BGAMH)						
490	EQUIVALENCE (C(1446),BGAMH)						
495	EQUIVALENCE (C(1447),BGAMH)						
500	EQUIVALENCE (C(1448),BGAMH)						
505	EQUIVALENCE (C(1449),BGAMH)						
510	EQUIVALENCE (C(1450),BGAMH)						
515	EQUIVALENCE (C(1451),BGAMH)						
520	EQUIVALENCE (C(1452),BGAMH)						
525	EQUIVALENCE (C(1453),BGAMH)						
530	EQUIVALENCE (C(1454),BGAMH)						
535	EQUIVALENCE (C(1455),BGAMH)						
540	EQUIVALENCE (C(1456),BGAMH)						
545	EQUIVALENCE (C(1457),BGAMH)						
550	EQUIVALENCE (C(1458),BGAMH)						
555	EQUIVALENCE (C(1459),BGAMH)						
560	EQUIVALENCE (C(1460),BGAMH)						
565	EQUIVALENCE (C(1461),BGAMH)						
570	EQUIVALENCE (C(1462),BGAMH)						
575	EQUIVALENCE (C(1463),BGAMH)						
580	EQUIVALENCE (C(1464),BGAMH)						
585	EQUIVALENCE (C(1465),BGAMH)						
590	EQUIVALENCE (C(1466),BGAMH)						
595	EQUIVALENCE (C(1467),BGAMH)						
600	EQUIVALENCE (C(1468),BGAMH)						
605	EQUIVALENCE (C(1469),BGAMH)						
610	EQUIVALENCE (C(1470),BGAMH)						
615	EQUIVALENCE (C(1471),BGAMH)						
620	EQUIVALENCE (C(1472),BGAMH)						
625	EQUIVALENCE (C(1473),BGAMH)						
630	EQUIVALENCE (C(1474),BGAMH)						
635	EQUIVALENCE (C(1475),BGAMH)						
640	EQUIVALENCE (C(1476),BGAMH)						
645	EQUIVALENCE (C(1477),BGAMH)						
650	EQUIVALENCE (C(1478),BGAMH)						
655	EQUIVALENCE (C(1479),BGAMH)						
660	EQUIVALENCE (C(1480),BGAMH)						
665	EQUIVALENCE (C(1481),BGAMH)						
670	EQUIVALENCE (C(1482),BGAMH)						
675	EQUIVALENCE (C(1483),BGAMH)						
680	EQUIVALENCE (C(1484),BGAMH)						
685	EQUIVALENCE (C(1485),BGAMH)						
690	EQUIVALENCE (C(1486),BGAMH)						
695	EQUIVALENCE (C(1487),BGAMH)						
700	EQUIVALENCE (C(1488),BGAMH)						
705	EQUIVALENCE (C(1489),BGAMH)						
710	EQUIVALENCE (C(1490),BGAMH)						
715	EQUIVALENCE (C(1491),BGAMH)						
720	EQUIVALENCE (C(1492),BGAMH)						
725	EQUIVALENCE (C(1493),BGAMH)						
730	EQUIVALENCE (C(1494),BGAMH)						
735	EQUIVALENCE (C(1495),BGAMH)						
740	EQUIVALENCE (C(1496),BGAMH)						
745	EQUIVALENCE (C(1497),BGAMH)						
750	EQUIVALENCE (C(1498),BGAMH)						
755	EQUIVALENCE (C(1499),BGAMH)						
760	EQUIVALENCE (C(1500),BGAMH)						
765	EQUIVALENCE (C(1501),BGAMH)						
770	EQUIVALENCE (C(1502),BGAMH)						
775	EQUIVALENCE (C(1503),BGAMH)						
780	EQUIVALENCE (C(1504),BGAMH)						
785	EQUIVALENCE (C(1505),BGAMH)						
790	EQUIVALENCE (C(1506),BGAMH)						
795	EQUIVALENCE (C(1507),BGAMH)						
800	EQUIVALENCE (C(1508),BGAMH)						
805	EQUIVALENCE (C(1509),BGAMH)						
810	EQUIVALENCE (C(1510),BGAMH)						
815	EQUIVALENCE (C(1511),BGAMH)						
820	EQUIVALENCE (C(1512),BGAMH)						
825	EQUIVALENCE (C(1513),BGAMH)						
830	EQUIVALENCE (C(1514),BGAMH)						
835	EQUIVALENCE (C(1515),BGAMH)						
840	EQUIVALENCE (C(1516),BGAMH)						
845	EQUIVALENCE (C(1517),BGAMH)						
850	EQUIVALENCE (C(1518),BGAMH)						
855	EQUIVALENCE (C(1519),BGAMH)						
860	EQUIVALENCE (C(1520),BGAMH)						
865	EQUIVALENCE (C(1521),BGAMH)						
870	EQUIVALENCE (C(1522),BGAMH)						
875	EQUIVALENCE (C(1523),BGAMH)						
880	EQUIVALENCE (C(1524),BGAMH)						
885	EQUIVALENCE (C(1525),BGAMH)						
890	EQUIVALENCE (C(1526),BGAMH)						
895	EQUIVALENCE (C(1527),BGAMH)						
900	EQUIVALENCE (C(1528),BGAMH)						
905	EQUIVALENCE (C(1529),BGAMH)						
910	EQUIVALENCE (C(1530),BGAMH)						
915	EQUIVALENCE (C(1531),BGAMH)						
920	EQUIVALENCE (C(1532),BGAMH)						
925	EQUIVALENCE (C(1533),BGAMH)						
930	EQUIVALENCE (C(1534),BGAMH)						
935	EQUIVALENCE (C(1535),BGAMH)						
940	EQUIVALENCE (C(1536),BGAMH)						
945	EQUIVALENCE (C(1537),BGAMH)						
950	EQUIVALENCE (C(1538),BGAMH)						
955	EQUIVALENCE (C(1539),BGAMH)						
960	EQUIVALENCE (C(1540),BGAMH)						
965	EQUIVALENCE (C(1541),BGAMH)						
970	EQUIVALENCE (C(1542),BGAMH)						
975	EQUIVALENCE (C(1543),BGAMH)						
980	EQUIVALENCE (C(1544),BGAMH)						
985	EQUIVALENCE (C(1545),BGAMH)						
990	EQUIVALENCE (C(1546),BGAMH)						
995	EQUIVALENCE (C(1547),BGAMH)						
1000	EQUIVALENCE (C(1548),BGAMH)						

SUBROUTINE G4		7/4/74	OPT=1	FTN 4.2*74.355	07/07/76	11.07.07.	PAGE
CARD NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM				
58	I	INVT	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				
63	I	INVT	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.				

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	100	108	110
I G	I				
VARIABLES	SN TYPE	RELOCATION			
544 3GARM	REAL	C			REFS 12
545 3GANV	REAL	C			REFS 12
546 3G	REAL	C			REFS 12
547 3G	REAL	C			REFS 12
548 3G	REAL	C			REFS 12
549 3G	REAL	C			REFS 12
550 3G	REAL	C			REFS 12
551 3G	REAL	C			REFS 12
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746 3G	REAL	C			REFS 12
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749 3G	REAL	C			REFS 12
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784 3G	REAL	C			REFS 12
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815 3G	REAL	C			REFS 12
816 3G	REAL	C			REFS 12
817 3G	REAL	C			REFS 12
818 3G	REAL	C			REFS 12
819 3G	REAL	C			REFS 12
820 3G	REAL	C			REFS 12
821 3G	REAL	C			REFS 12
822 3G	REAL	C			

VARIABLES	SN	TYPE	RELOCATION	REFS	2*P1	DEFINED	197
*26 UZP	REAL			REFS	54	55	DEFINED
*11 VALUE	REAL			REFS	31	32	DEFINED
*301 VMEAN	REAL		ARRAY C	REFS	30	31	DEFINED
*307 V3J	REAL		ARRAY C	REFS	35	36	DEFINED
*36 V3JM	REAL		ARRAY	DEFINED	54		
*50 V52	REAL		ARRAY	REFS	35	36	DEFINED
*35 XN3SPOT	REAL			REFS	85	86	DEFINED
*32 Y44	REAL			REFS	77	78	DEFINED
*33 YM2	REAL		C	REFS	19	20	DEFINED
*34 YM2	REAL		C	REFS	20	21	DEFINED
*45 ZM2	REAL		C	REFS	21	22	DEFINED
*346 ZM2	REAL		C	REFS	22	23	DEFINED
FILE NAMES	MODE						
1220	FMT						
			*RTIES	76	77	78	83
							85
							95
							96

EXTERNALS	TYPE	REFS	REFERENCES
CUSS	REAL	1	39
MCARLX	REAL	3	82
SAND	REAL	1	38
SURT	REAL	1	LIBRARY
			53
			73
			84

STATEMENT LABELS

STATEMENT LABELS	DEF LINE	REFERENCES
00 2	59	
73 3	51	
0 5	51	
104 10	101	
175 20	37	
182 30	87	
100 20	65	
211 101	7	
221 201	9	
231 300	11	
204 401	60	
312 500	80	
251 600	78	
325 2255	91	
335 2556	93	
		77

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
			51 04	330	EXT REFS

COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)
	3630	0 C	(3630)

ENVY CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
	3630		
		301 RYF	(1)
		357 B5AMV	(1)
		1504 YMC2	(1)
		1634 RDELX	(1)
		1499 T	(1)
		3009 VMEAN	(10)
		3720 ITOT	(1)
		299 RM55	(1)
		302 RZF	(1)
		370 RANGE	(1)
		1573 YMC	(1)
		1574 YMC2	(1)
		1636 RDELZ	(1)
		2019 VSD	(10)
		3019 INVDET	(1)

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STATISTICS

PROGRAM LENGTH	4528	306
CM LABELED COMMON LENGTH	74668	3830

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SUBROUTINE AMRK(AUXSUB)
COMMON /X/ C(183)
DIMENSION CSAV(100), IPL(100)
REAL K1(100), K2(100), K3(100), K4(100)
EQUIVALENCE (C(2000), T)
EQUIVALENCE (C(2664), DELT)
EQUIVALENCE (C(1174), NJ)
EQUIVALENCE (C(2562), IPL)
EQUIVALENCE (C(1375), XNRK)
XNRK = -1.
DO 1 I = 1, NJ
  J = IPL(I)
C *****STORE INITIAL VALUES
C CSAV(I) = C(J*3)
C *** COMPUTE K1
K1(I) = DELT*C(J)
1 C(J*3) = CSAV(I) + .5*K1(I)
  T = T + .5*DELT
  CALL AUXSUB
C *** COMPUTE K2
DO 2 I = 1, NJ
  J = IPL(I)
  K2(I) = DELT*C(J)
  2 C(J*3) = CSAV(I) + .5*K2(I)
  CALL AUXSUB
C *** COMPUTE K3
DO 3 I = 1, NJ
  J = IPL(I)
  K3(I) = DELT*C(J)
  3 C(J*3) = CSAV(I) + K3(I)
  T = T + .5*DELT
  CALL AUXSUB
C *** COMPUTE K4
DO 4 I = 1, NJ
  J = IPL(I)
  K4(I) = DELT*C(J)
  4 C(J*3) = CSAV(I) + (K1(I) + 2.*K2(I) + K3(I) + C4(I))/5.
  XNRK = K4
  CALL AUXSUB
  RETURN
END

```

SUBROUTINE AMK		7474	OPI=1	FTN **27435	07/0773	11.07.10.	PAGE	2
CARD NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM					
19	I	NJ	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.					
27	I	NJ	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.					
34	I	NJ	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.					
42	I	NJ	THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.					

SYMBOLIC REFERENCE MAP (K=3)

ENTRY POINTS DEF LINE REFERENCES
3 AMRK 1 45

VARIABLES SN TYPE RELOCATION

0 C	REAL	ARRAY	C	REFS	2	3	5	6	7	8	9	15
114	USAV	REAL	ARRAY	REFS	10	26	33	41	DEFINED	19	27	34
117	DEL-T	REAL	C	REFS	42	3	19	27	34	42		
112	I	INTEGER	C	DEFINED	15	6	14	20	26	33	35	41
5001	IPL	INTEGER	C	REFS	12	12	13	18	24	25	26	27
113	J	INTEGER	C	REFS	32	33	24	31	39	54	42	
200	K1	REAL	ARRAY	REFS	11	11	24	31	35	32	40	
424	K2	REAL	ARRAY	REFS	3	3	3	12	25	27	33	34
570	K3	REAL	ARRAY	REFS	15	15	18	19	26	27	33	
734	K4	REAL	ARRAY	REFS	42	42	DEFINED	12	25	32	40	
5005	NJ	INTEGER	C	REFS	4	4	27	42	DEFINED	26		
5717	T	REAL	C	REFS	4	4	34	42	DEFINED	41		
5007	XNDK	REAL	C	REFS	5	5	11	24	31	39		
				REFS	9	9	DEFINED	18	43	20	35	

EXTERNALS TYPE AMKS REFERENCES

AUXSUB	0	F.P.	21	28	36	44
STATEMENT LABELS	DEF LINE	REFERENCES				
0	1	41				
2	27	24				
3	34	31				
4	42	39				

LAOPS LABEL INDEX FROM-TO LENGTH PROPERTIES

23	1	11	19	54	INSTACK
41	2	24	27	54	INSTACK
54	3	34	34	54	INSTACK
70	4	34	42	113	OPT

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

0	3430	0	4340
ENTR CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)	
0	3430	1973 NJ (1)	1975 XNDK (1)
		2501 IPL (100)	2663 DELT (1)

STATISTICS

PROGRAM LENGTH 11058 581
COMMON LENGTH 74009 3636

SUBROUTINE AUX1	74/74	OPT=1	FTN +.2474355	07/07/75	11.07.11.	PAGE	1
SUBROUTINE AUX1							
COMMON /C/ C(1830)							
EQUIVALENCE (C(12361),NOMOD), (C(2362),XMODNO), (C(2561),N)							
DIMENSION XMODNO(99)							
N = 1							
DO 1 I=1,NOMOD							
L=XMODNO(I)							
1 GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23							
2 CALL ALL							
3 CALL A2I							
4 CALL A3I							
5 CALL A4I							
6 CALL A5I							
7 CALL C1I							
8 CALL C2I							
9 CALL C3I							
10 CALL C4I							
11 CALL C5I							
12 CALL C6I							
13 CALL C7I							
14 CALL C8I							
15 CALL C9I							
16 CALL C10I							
17 CALL C11I							
18 CALL C2I							
19 CALL C3I							
20 CALL C4I							
21 CALL C5I							
22 CALL C11I							
23 CALL C2I							
24 CALL C3I							
25 CALL C4I							
GO TO L							

SUBROUTINE	AUX1	74/74	OPT=1	FIN 4.2*74.355	07/07/76 11.07.11.	PAGE	2
60	26 CALL G91	GO TO 1			AMRK 105		
	27 CALL G61	GO TO 1			AMRK 106		
	28 CALL S21	GO TO 1			AMRK 107		
	29 CALL S21	GO TO 1			AMRK 108		
	30 CALL S31	GO TO 1			AMRK 109		
	31 CALL S41	GO TO 1			AMRK 110		
	32 CALL S51	GO TO 1			AMRK 111		
	33 CALL S61	GO TO 1			AMRK 112		
	34 CALL S71	GO TO 1			AMRK 113		
	35 CALL S81	GO TO 1			AMRK 114		
	36 CALL S91	GO TO 1			AMRK 115		
	37 CALL S101	GO TO 1			AMRK 116		
	38 CALL S111	GO TO 1			AMRK 117		
	39 CALL S121	GO TO 1			AMRK 118		
	40 CALL S131	GO TO 1			AMRK 119		
	41 CALL S141	GO TO 1			AMRK 120		
	42 CALL S151	GO TO 1			AMRK 121		
	43 CALL S161	GO TO 1			AMRK 122		
	44 CALL S171	GO TO 1			AMRK 123		
	45 CALL S181	GO TO 1			AMRK 124		
	46 CALL S191	GO TO 1			AMRK 125		
	47 CALL S201	GO TO 1			AMRK 126		
	48 CALL S211	GO TO 1			AMRK 127		
	49 CALL S221	GO TO 1			AMRK 128		
	50 CALL S231	GO TO 1			AMRK 129		
	51 CALL S241	GO TO 1			AMRK 130		
	52 CALL S251	GO TO 1			AMRK 131		
	53 CALL S261	GO TO 1			AMRK 132		
	54 CALL S271	GO TO 1					
	55 CALL S281	GO TO 1					
	56 CALL S291	GO TO 1					
	57 CALL S301	GO TO 1					
	58 CALL S311	GO TO 1					
	59 CALL S321	GO TO 1					
	60 CALL S331	GO TO 1					
	61 CALL S341	GO TO 1					
	62 CALL S351	GO TO 1					
	63 CALL S361	GO TO 1					
	64 CALL S371	GO TO 1					
	65 CALL S381	GO TO 1					
	66 CALL S391	GO TO 1					
	67 CALL S401	GO TO 1					
	68 CALL S411	GO TO 1					
	69 CALL S421	GO TO 1					
	70 CALL S431	GO TO 1					
	71 CALL S441	GO TO 1					
	72 CALL S451	GO TO 1					
	73 CALL S461	GO TO 1					
	74 CALL S471	GO TO 1					
	75 CALL S481	GO TO 1					
	76 CALL S491	GO TO 1					
	77 CALL S501	GO TO 1					
	78 CALL S511	GO TO 1					
	79 CALL S521	GO TO 1					
	80 CALL S531	GO TO 1					
	81 CALL S541	GO TO 1					
	82 CALL S551	GO TO 1					
	83 CALL S561	GO TO 1					
	84 CALL S571	GO TO 1					
	85 CALL S581	GO TO 1					
	86 CALL S591	GO TO 1					
	87 CALL S601	GO TO 1					
	88 CALL S611	GO TO 1					
	89 CALL S621	GO TO 1					
	90 CALL S631	GO TO 1					
	91 CALL S641	GO TO 1					
	92 CALL S651	GO TO 1					
	93 CALL S661	GO TO 1					
	94 CALL S671	GO TO 1					
	95 CALL S681	GO TO 1					
	96 CALL S691	GO TO 1					
	97 CALL S701	GO TO 1					
	98 CALL S711	GO TO 1					
	99 CALL S721	GO TO 1					
	100 CALL S731	GO TO 1					
	101 CALL S741	GO TO 1					
	102 CALL S751	GO TO 1					
	103 CALL S761	GO TO 1					
	104 CALL S771	GO TO 1					
	105 CALL S781	GO TO 1					
	106 CALL S791	GO TO 1					
	107 CALL S801	GO TO 1					
	108 CALL S811	GO TO 1					
	109 CALL S821	GO TO 1					
	110 CALL S831	GO TO 1					
	111 CALL S841	GO TO 1					
	112 CALL S851	GO TO 1					
	113 CALL S861	GO TO 1					
	114 CALL S871	GO TO 1					
	115 CALL S881	GO TO 1					
	116 CALL S891	GO TO 1					
	117 CALL S901	GO TO 1					
	118 CALL S911	GO TO 1					
	119 CALL S921	GO TO 1					
	120 CALL S931	GO TO 1					
	121 CALL S941	GO TO 1					
	122 CALL S951	GO TO 1					
	123 CALL S961	GO TO 1					
	124 CALL S971	GO TO 1					
	125 CALL S981	GO TO 1					
	126 CALL S991	GO TO 1					
	127 CALL S1001	GO TO 1					
	128 CALL S1011	GO TO 1					
	129 CALL S1021	GO TO 1					
	130 CALL S1031	GO TO 1					
	131 CALL S1041	GO TO 1					
	132 CALL S1051	GO TO 1					
	133 CALL S1061	GO TO 1					
	134 CALL S1071	GO TO 1					
	135 CALL S1081	GO TO 1					
	136 CALL S1091	GO TO 1					
	137 CALL S1101	GO TO 1					
	138 CALL S1111	GO TO 1					
	139 CALL S1121	GO TO 1					
	140 CALL S1131	GO TO 1					
	141 CALL S1141	GO TO 1					
	142 CALL S1151	GO TO 1					
	143 CALL S1161	GO TO 1					
	144 CALL S1171	GO TO 1					
	145 CALL S1181	GO TO 1					
	146 CALL S1191	GO TO 1					
	147 CALL S1201	GO TO 1					
	148 CALL S1211	GO TO 1					
	149 CALL S1221	GO TO 1					
	150 CALL S1231	GO TO 1					
	151 CALL S1241	GO TO 1					
	152 CALL S1251	GO TO 1					
	153 CALL S1261	GO TO 1					
	154 CALL S1271	GO TO 1					
	155 CALL S1281	GO TO 1					
	156 CALL S1291	GO TO 1					
	157 CALL S1301	GO TO 1					
	158 CALL S1311	GO TO 1					
	159 CALL S1321	GO TO 1					
	160 CALL S1331	GO TO 1					
	161 CALL S1341	GO TO 1					
	162 CALL S1351	GO TO 1					
	163 CALL S1361	GO TO 1					
	164 CALL S1371	GO TO 1					
	165 CALL S1381	GO TO 1					
	166 CALL S1391	GO TO 1					
	167 CALL S1401	GO TO 1					
	168 CALL S1411	GO TO 1					
	169 CALL S1421	GO TO 1					
	170 CALL S1431	GO TO 1					
	171 CALL S1441	GO TO 1					
	172 CALL S1451	GO TO 1					
	173 CALL S1461	GO TO 1					
	174 CALL S1471	GO TO 1					
	175 CALL S1481	GO TO 1					
	176 CALL S1491	GO TO 1					
	177 CALL S1501	GO TO 1					
	178 CALL S1511	GO TO 1					
	179 CALL S1521	GO TO 1					
	180 CALL S1531	GO TO 1					
	181 CALL S1541	GO TO 1					
	182 CALL S1551	GO TO 1					
	183 CALL S1561	GO TO 1					
	184 CALL S1571	GO TO 1					
	185 CALL S1581	GO TO 1					
	186 CALL S1591	GO TO 1					
	187 CALL S1601	GO TO 1					
	188 CALL S1611	GO TO 1					
	189 CALL S1621	GO TO 1					
	190 CALL S1631	GO TO 1					
	191 CALL S1641	GO TO 1					
	192 CALL S1651	GO TO 1					
	193 CALL S1661	GO TO 1					
	194 CALL S1671	GO TO 1					
	195 CALL S1681	GO TO 1					
	196 CALL S1691	GO TO 1					
	197 CALL S1701	GO TO 1					
	198 CALL S1711	GO TO 1					
	199 CALL S1721	GO TO 1					
	200 CALL S1731	GO TO 1					
	201 CALL S1741	GO TO 1					
	202 CALL S1751	GO TO 1					
	203 CALL S1761	GO TO 1					
	204 CALL S1771	GO TO 1					
	205 CALL S1781	GO TO 1					
	206 CALL S1791	GO TO 1					
	207 CALL S1801	GO TO 1					
	208 CALL S1811	GO TO 1					
	209 CALL S1821	GO TO 1					
	210 CALL S1831	GO TO 1					
	211 CALL S1841	GO TO 1					
	212 CALL S1851	GO TO 1					
	213 CALL S1861	GO TO 1					
	214 CALL S1871	GO TO 1					
	215 CALL S1881	GO TO 1					
	216 CALL S1891	GO TO 1					
	217 CALL S1901	GO TO 1					
	218 CALL S1911	GO TO 1					
	219 CALL S1921	GO TO 1					
	220 CALL S1931	GO TO 1					
	221 CALL S1941	GO TO 1					
	222 CALL S1951	GO TO 1					
	223 CALL S						

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES					
1	1	84					
VARIABLES	SN	TYPE	RELOCATION	REFS	2	3-3	6
0 C	ARRAY	C					
174 I	INTEGER			REFS	7	DEFINED	6
175 L	INTEGER			REFS	0	DEFINED	7
200 N	INTEGER		C	REFS	3	DEFINED	5
**70 NUM00	INTEGER		C	REFS	3		5
**71 NUM000	REAL		C	REFS	3		7
EXTERNALS	TYPE	REFS	REFERENCES				
A11	0	10					
A21	0	12					
A31	0	14					
A41	0	16					
A51	0	18					
G11	0	20					
G101	0	30					
G21	0	22					
G31	0	24					
G41	0	26					
G51	0	28					
G61	0	30					
G71	0	32					
G81	0	34					
G91	0	36					
D11	0	40					
D21	0	42					
D31	0	44					
D41	0	46					
D51	0	48					
G11	0	50					
G21	0	52					
G31	0	54					
G41	0	56					
G51	0	58					
G61	0	60					
SP311	0	62					
S11	0	62					
S101	0	60					
S21	0	64					
S31	0	66					
S41	0	68					
S51	0	70					
S61	0	72					
S71	0	74					
S81	0	76					
S91	0	78					
STATEMENT LABELS	DEF LINE	REFERENCES					
171 1	83	8					
		25					
		43					
		63					
		11					
		15					
		17					
		19					
		21					
		23					
		29					
		33					
		35					
		37					
		41					
		45					
		47					
		51					
		53					
		55					
		57					
		59					
		61					
		65					
		67					
		71					
		73					
		75					
		77					

STATEMENT LABELS		DEF LINE		REFERENCES	
00 2	10	0	0	0	0
02 3	12	0	0	0	0
04 4	14	0	0	0	0
06 5	16	0	0	0	0
08 6	18	0	0	0	0
10 7	20	0	0	0	0
12 8	22	0	0	0	0
14 9	24	0	0	0	0
16 10	26	0	0	0	0
18 11	28	0	0	0	0
20 12	30	0	0	0	0
22 13	32	0	0	0	0
24 14	34	0	0	0	0
26 15	36	0	0	0	0
28 16	38	0	0	0	0
30 17	40	0	0	0	0
32 18	42	0	0	0	0
34 19	44	0	0	0	0
36 20	46	0	0	0	0
38 21	48	0	0	0	0
40 22	50	0	0	0	0
42 23	52	0	0	0	0
44 24	54	0	0	0	0
46 25	56	0	0	0	0
48 26	58	0	0	0	0
50 27	60	0	0	0	0
52 28	62	0	0	0	0
54 29	64	0	0	0	0
56 30	66	0	0	0	0
58 31	68	0	0	0	0
60 32	70	0	0	0	0
62 33	72	0	0	0	0
64 34	74	0	0	0	0
66 35	76	0	0	0	0
68 36	78	0	0	0	0
70 37	80	0	0	0	0
72 38	82	0	0	0	0
LJUP LABEL INDEX FROM-TO LENGTH PROPERTIES EXT REFS					
* 1	0 83	1703			
COMMON BLOCKS					
C	LENGTH	MEMBERS	BIAS NAME(LENGTH)		
	3830	0 C	(3830)		
EQUIV CLASSES					
C	LENGTH	MEMBERS	BIAS NAME(LENGTH)		
	3830	2360 NO-MOD (1)	2361 XMODMOD (93)	2550 N	(1)
STATISTICS					
PROGRAM LENGTH		1768	126		
CM LABELED COMMON LENGTH		73603	3830		

60	23 CALL G2	AMRK	190
	GO TO 1	AMRK	191
	24 CALL G3	AMRK	192
	GO TO 1	AMRK	193
	25 CALL G4	AMRK	194
	GO TO 1	AMRK	195
62	26 CALL G5	AMRK	196
	GO TO 1	AMRK	197
	27 CALL G6	AMRK	198
	GO TO 1	AMRK	199
	28 CALL S1	AMRK	200
70	GO TO 1	AMRK	201
	29 CALL S2	AMRK	202
	GO TO 1	AMRK	203
	30 CALL S3	AMRK	204
	GO TO 1	AMRK	205
75	31 CALL S4	AMRK	206
	GO TO 1	AMRK	207
	32 CALL S5	AMRK	208
	GO TO 1	AMRK	209
	33 CALL S6	AMRK	210
80	GO TO 1	AMRK	211
	34 CALL S7	AMRK	212
	GO TO 1	AMRK	213
	35 CALL S8	AMRK	214
	GO TO 1	AMRK	215
85	36 CALL S9	AMRK	216
	GO TO 1	AMRK	217
	37 CALL S10	AMRK	218
	GO TO 1	AMRK	219
90	38 CALL SHOT	AMRK	220
	1 CONTINUE	AMRK	221
	PETJRN	AMRK	222
	END	AMRK	223
		AMRK	224

ENTRY POINTS	DEF LINE	REFERENCES
1 AUXSUB	1	13
		91

501

SUBROUTINE AUXSR				FIN 4.2*7.353				07/07/76 11.07.13.				PAGE 4							
STATEMENT LABELS				DEF LINE REFERENCES															
172	1			90	12	15	18	20	22	24	26	28	30						
					32	34	36	38	40	42	44	46	48						
					50	52	54	56	58	60	62	64	66						
					68	70	72	74	76	78	80	82	84						
					86	88													
01	2			17	15														
03	3			19	15														
05	4			21	15														
07	5			23	15														
09	6			25	15														
11	7			27	15														
13	8			29	15														
15	9			31	15														
17	10			33	15														
19	11			35	15														
21	12			37	15														
23	13			39	15														
25	14			41	15														
27	15			43	15														
29	16			45	15														
31	17			47	15														
33	18			49	15														
35	19			51	15														
37	20			53	15														
39	21			55	15														
41	22			57	15														
43	23			59	15														
45	24			61	15														
47	25			63	15														
49	26			65	15														
51	27			67	15														
53	28			69	15														
55	29			71	15														
57	30			73	15														
59	31			75	15														
61	32			77	15														
63	33			79	15														
65	34			81	15														
67	35			83	15														
69	36			85	15														
71	37			87	15														
73	38			89	15														
LOOPS LABEL INDEX				FROM-TO	LENGTH	PROPERTIES	EXT	REFS	ENITS										
3	1			12	90	1728													
COMMON BLOCKS				MEMBERS	- BIAS	NAME(LENGTH)													
C				0	C	(3830)													
EQUIV CLASSES				MEMBERS	- BIAS	NAME(LENGTH)													
C				1999	T	(11)	2819	LG04M	(11)	2350	MMOD	(11)							
				2361	XMODNO	(99)	2560	N	(11)	2551	IPL	(100)							
				2663	DER	(1811)	2964	VAR	(1811)										
STATISTICS																			
PROGRAM LENGTH				1778	127														
COMMON LABELLED COMMON LENGTH				78669	3830														

SYMBOLIC REFERENCE MAP TR=31

ENTRY POINTS	DEF LINE	REFERENCES				
1 DUMPO	1	11				
VARIABLES	SN	TYPE	RELOCATION	REFS	DEF LINE	REFERENCES
0 C		REAL	ARRAY	7	7	7
57 I		INTEGER		6	8	DEFINED 3
61 J		INTEGER		7	8	DEFINED 5
62 K		INTEGER		7	8	DEFINED 6
66 P		INTEGER		8	8	DEFINED 4

FILE NAMES	MODE	WRITES
TAPE0	FMT	8

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
ABS	REAL	1	INTSN	7

STATEMENT LABELS	DEF LINE	REFERENCES
0 100	8	3
0 200	7	5
53 200	FMT	10 8

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT-REFS
3	100	I	3	7	350	INSTACK
11	203	J	5	7	73	EXT-REFS NOT INNER

COMMON BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)
C	3830	0	C (3830)

STATISTICS	PROGRAM LENGTH	51
CM LABELED COMMON LENGTH	73668	3030


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IF (IPLAS .LE. 0) GO TO 200
WRITE(6,201)
201 FORMAT(10H,*RESET DATA ARRAY EXCEEDED DURING LAST RUN.*/
11H *40H*****ABNORMAL TERMINATION*****//)
CALL EXIT
STOP
200 CONTINUE
JAB = 0
WRITE(6,31)
31 FORMAT(11H,INPUT DATA/)
1 READ(5,2)IR(1),(ALPHA(JC),J=1,3),IR(2),IR(3),TPR,TPSGMA,
*VR(1),VR(2),VR(3),IR(4),VR(4)
IF (IPLAS .GT. 50) GO TO 55
55 CONTINUE
WRITE(6,30)IR(1),(ALPHA(JC),J=1,3),IR(2),IR(3),TPR,TPSGMA,
*VR(1),VR(2),VR(3),
*IR(4),VR(4)
30 FORMAT(1X,12,3A6,15,12,A1,F5.2,2E15.7,F10.4,I5,F7.4)
7 IF (IR(1) .NE. 1) GO TO 3
SUBNO(NOSUB) = IR(2)
GO TO 1
3 IF (IR(1) .NE. 2) GO TO 4
NOSUB = NOSUB + 1
SUBNO(NOSUB) = IR(2)
GO TO 1
4 IF (IR(1) .NE. 3) GO TO 5
L = IR(2)
C(L) = VR(1)
IF (VR(2) .EQ. 0) GO TO 1
IF (NLIST .LE. 49) GO TO 10
WRITE(6,109) (ALPHA(J),J=1,3),IR(2)
109 FORMAT(10H,*RESET VARIABLE LIST EXCEEDED *3A6,* C-LOCATION *15,
1* EXCLUDED FROM RESET LIST*)
IFLAG = 1
GO TO 1
10 CONTINUE
NLIST = NLIST + 1
LISTNO(NLIST) = L
VALUE(NLIST) = VR(1)
GO TO 1
5 IF (IR(1) .NE. 49) GO TO 6
WRITE(6,11) (ALPHA(J),J=1,3),IR(2)
11 FORMAT(10H,*OUTPUT LIST EXCEEDED *3A6,* C-LOCATION *15
1* EXCLUDED FROM OUTPUT LIST*)
GO TO 1
12 CONTINUE
NOUT = NOUT + 1
IF (NOUT .GT. 50) GO TO 1
NAME1(NOUT) = ALPHA(2)
NAME2(NOUT) = ALPHA(3)
OUTNO(NOUT) = IR(2)
GO TO 1
6 IF (IR(1) .NE. 5) GO TO 16
READ(5,16)

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115 WRITE(TOTDAP)
GO TO 1
16 IF (IK(1).NE.7) GO TO 19
IF(NPLOT .LE. 14) GO TO 14
WRITE(6,13) (ALPHA(I),I=1,3),IR(2)
120 FORMAT(1H0,'PLOT LIST EXCEEDED *346* C-LOCATION *15,
1* EXCLUDED FROM LIST*')
GO TO 1
14 CONTINUE
14 NPLOT=NPLOT+1
IF (NPLOT.GT.15) GO TO 1
DECODE (1,9,1PER)ISCALE(NPLOT)
FORMAT(1H0,'PLOT LIST EXCEEDED *346* C-LOCATION *15,
1* EXCLUDED FROM LIST*')
130 YMAX(NPLOT)=VR(1) 3 YMIN(NPLOT)=VR(2)
DO 20 I=1,2
VLAJLE (1,NPLOT)=ALPHA(I+1)
OUTPUT(NPLOT)=IR(2)
GO TO 1
19 IF (IR(1).NE.0) GO TO 18
IF (IR(1).EQ.553) GO TO 194
IF (IR(1).GT.0) GO TO 192
IF (IR(1).NE.0.AND.IR(1).NE.1) GO TO 193
IF (ISGCT .LE. 39) GO TO 22
WRITE(6,21) (ALPHA(I),I=1,3),IR(2)
21 FORMAT(1H0,'INITIAL CONDITION M. C. VARIABLE LIST EXCEEDED *346,
1* C-LOCATION *15* EXCLUDED FROM LIST*')
GO TO 1
22 CONTINUE
ISGCT=ISGCT+1
SIGMA(ISGCT)=VR(1)
SIGMA2(ISGCT)=VR(2)
ISMDX(ISGCT)=VR(3)
ISDST(ISGCT)=IR(2)
GO TO 1
150 IF (IR(1) .NE. 9) GO TO 100
STEP = 11.
REAL(5,8)NP,IBVNSM,IPLOT,XLAMBO,KSSIG,(CEPSIG(I),I=1,5),PSIZE
8 FORMAT(314,2F10.3,5I2,E15.7)
GO TO 1
155 IF (IR(1) .NE. 10) GO TO 191
IF (IMUCT .LE. 9) GO TO 108
WRITE(6,107) (ALPHA(I),I=1,3),IR(2)
107 FORMAT(1H0,'MEAN AND STD. DEV. VARIABLE LIST EXCEEDED *346,
1* C-LOCATION *15* EXCLUDED FROM LIST*')
GO TO 1
160 CONTINUE
IMUCT = IMUCT + 1
IMWDR(IMUCT) = IR(2)
GO TO 1
165 IF (IR(1).GT.5) GO TO 193
IF (ITCT .LE. 9) GO TO 105
WRITE(6,104) (ALPHA(I),I=1,3),IR(2)
104 FORMAT(1H0,'TIME SERIES M. C. VARIABLE LIST EXCEEDED *346,
1* C-LOCATION *15* EXCLUDED FROM LIST*')
GO TO 1
170 CONTINUE
185 CONTINUE

```

174	IF(ICT=IICCT)=1	10
	TPSGMA(IICCT)=VR(1)	10
	TLBI(IICCT)=VR(2)	10
175	TLBI(IICCT)=VR(2)	10
	TLBI(IICCT)=VR(3)	10
	INDEX(IICCT)=IR(2)	10
	IF(VR(4).GT.0) INDEX2(IICCT)=IR(4)	10
	INDEX(IICCT)=IR(2)	10
	INDEX(IICCT)=IR(3)	10
180	TPSGMA(IICCT)=VR(4)	10
	TPSGMA(IICCT)=TPSGMA	10
	TYPEK(IICCT)=9.	10
	IF((IPER*EQ.CPERTV) TYPEK(IICCT)=1.	10
	GO TO 1	10
185	194 NSIRI=VR(1)	10
	GO TO 1	10
	193 WRITE(6,3510)	10
	5510 FORMAT(15,50UNDEFINED DISTRIBUTION TYPE NUMBER ENTERED - CARD REJ	10
	*ECT=0)	10
190	WRITE(6,301IR(1),ALPHA(ICT),JC=1,3),IR(2),IR(3),TPSGMA,	10
	*VR(1),VR(2),VR(3),	10
	*IR(4),VR(4)	10
	GO TO 1	10
195	191 CONTINUE	10
	NCASE=NCASE+1	10
	RETURN	10
	50 STOP	10
	END	10

SUBROUTINE 01NPT1	7474	OPT=1	FTN +.247.355	07/07/75	11.07.16.	PAGE	5
CARD NR. SEVERITY DETAILS	DIAGNOSIS OF PROBLEM						
70	1	33	00	76	FIELD WIDTH OF A CONVERSION DESCRIPTOR SHOULD BE AS LARGE AS THE MINIMUM SPECIFIED FOR THAT DESCRIPTOR.		

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
1 QINPT1 1 196

VARIABLES	SN	TYPE	RELOCATION	REFS	32	72	90	102	109	110	119
850 ALPHA	REAL	ARRAY		REFS	130	157	157	190	DEFINED	68	
852 ATJ	REAL	ARRAY	C	REFS	46	50	54				
857 BATD	REAL	ARRAY	C	REFS	46	51	54				
860 BOTA	REAL	ARRAY	C	REFS	46	53	54				
858 BREF	REAL	ARRAY	C	REFS	46	53	54				
860 C	REAL	ARRAY	C	REFS	13	179	10	11	12	7+13	11+15
				REFS	18	120	21	22	23	24	25
				REFS	26	47	48	49	50	51	52
30 CESSIG	INTEGER	ARRAY	C	REFS	23	49	41	DEFINED	152		
3436 COEFF	REAL	ARRAY	C	REFS	46	47	54				
301 CQRTY	REAL	ARRAY	C	REFS	103	DEFINED	55				
3574 CIA	REAL	ARRAY	C	REFS	46	52	54				
636 I	INTEGER	ARRAY	C	REFS	90	102	119	2+130	188	152	157
				REFS	107	107	112	119	129	138	152
2+ 13VNM	INTEGER	ARRAY	C	REFS	18	DEFINED	132				
731 I01ST	INTEGER	ARRAY	C	REFS	13	35	3+DEFINED	148			
303 IFLAG	INTEGER	ARRAY	C	REFS	59	DEFINED	57	93	DEFINED	152	
725 INACT	INTEGER	ARRAY	C	REFS	26	152	152	163			
713 IAVNUX	INTEGER	ARRAY	C	REFS	25	34	3+DEFINED	163			
25 IPLOT	INTEGER	ARRAY	C	REFS	19	DEFINED	132				
640 IR	INTEGER	ARRAY	C	REFS	31	4+72	177	79	81	83	85
				REFS	30	100	102	111	123	137	149
				REFS	131	2+136	136	147	149	150	155
				REFS	157	165	167	176	2+177	178	179
559+ 15SCALE	INTEGER	ARRAY	C	REFS	27	28	3+DEFINED	126			
507 15JCT	INTEGER	ARRAY	C	REFS	13	137	143	144	145	146	147
				REFS	140	DEFINED	143				
7061 15NDA	INTEGER	ARRAY	C	REFS	13	35	3+DEFINED	147			
7210 15CF	INTEGER	ARRAY	C	REFS	15	165	172	173	174	175	176
				REFS	178	173	180	181	182	183	
				REFS	177						
7262 17J1ST	INTEGER	ARRAY	C	REFS	15	37	3+DEFINED	179			
7250 17NDX	INTEGER	ARRAY	C	REFS	15	37	3+DEFINED	174			
7344 17NDX2	INTEGER	ARRAY	C	REFS	15	37	3+DEFINED	176	177		
831 JAR	INTEGER	ARRAY	C	REFS	63	DEFINED					
832 JC	INTEGER	ARRAY	C	REFS	64	72	130	DEFINED	68	72	130
830 K	INTEGER	ARRAY	C	REFS	64	72	130	DEFINED	68	72	130
27 KSSIG	REAL	ARRAY	C	REFS	22	43	43	DEFINED	152		
355 L	INTEGER	ARRAY	C	REFS	67	97	97	DEFINED	86		
5772 LISTNO	INTEGER	ARRAY	C	REFS	4	30	3+DEFINED	97			
4+71 MOUNO	REAL	ARRAY	C	REFS	4	82	83	DEFINED	63		
7300 NCASC	INTEGER	ARRAY	C	REFS	24	195	3+DEFINED	195			
5771 NO-1ST	INTEGER	ARRAY	C	REFS	4	89	96	97	98		
				REFS	96	DEFINED					
4+70 NOY0J	INTEGER	ARRAY	C	REFS	4	82	93	DEFINED	62		
5130 NOY1	INTEGER	ARRAY	C	REFS	4	101	107	108	109	110	111
				REFS	107	DEFINED					

512

SUBROUTINE QINPT1		74/74	OPT=1	FIN 1.2874353		07/07/75	11.07.16.	PAGE	9
EQUIV CLASSES		LENGTH	MEMBERS - BIAS NAME(LENGTH)						
			3993 SIQUG (100)		3823 ISMOK (100)	3573 IDIST (100)			
			3720 ITCT (11)		3722 TSSYM (10)	3712 TLR (10)			
			3742 TUB (10)		3722 ITMOK (10)	3752 ITDISY (10)			
			3772 TSPEQ (10)		3782 TYP2ER (10)	3732 TPSIG (10)			
			3802 FMXST (10)		3812 ITMOK2 (10)	3824 NCASE (11)			
STATISTICS									
PROGRAM LENGTH		6538	427						
CM LABELED COMMON LENGTH		73663	3838						

		SUBROUTINE OUP13	10	157
		OUTPUT SUBROUTINE OUP13	10	158
		COMMON /C/ C(1838)	10	159
		EQUIVALENCE	10	160
5	C	(C(1838),OUTNO), (C(1838),ONAME1), (C(1838),ONAME2),	10	161
		(C(1838),OTCNT), (C(1838),NOOUT), (C(1838),PCNT),	10	162
		(C(1838),PTCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	163
		(C(1838),TAPENO), (C(1838),DEP), (C(1838),TAPE),	10	164
10	C	(C(1838),PPCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	165
		(C(1838),PPCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	166
		(C(1838),PPCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	167
		(C(1838),PPCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	168
		(C(1838),PPCNT), (C(1838),PPCNT), (C(1838),PPCNT),	10	169
15	C	DIMENSION GRAPH(1838),TIME(1838)	10	170
		DIMENSION TIME(1838),GRAPH(1,1)	10	171
		DIMENSION OUTPLT(15)	10	172
		INTEGER OTCNT,PCGNT,OUTNO	10	173
		INTEGER OPOINT	10	174
		INTEGER OUTPLT	10	175
20	C	SAVE SPOT JITTER MAX/MIN VALUES	10	176
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	177
		IF (C(1838).LT.C(1838)) C(1838) = C(1838)	10	178
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	179
25	C	IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	180
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	181
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	182
30	C	IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	183
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	184
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	185
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	186
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	187
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	188
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	189
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	190
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	191
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	192
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	193
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	194
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	195
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	196
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	197
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	198
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	199
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	200
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	201
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	202
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	203
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	204
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	205
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	206
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	207
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	208
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	209
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	210
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	211
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	212
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	213
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	214
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	215
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	216
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	217
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	218
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	219
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	220
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	221
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	222
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	223
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	224
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	225
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	226
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	227
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	228
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	229
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	230
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	231
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	232
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	233
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	234
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	235
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	236
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	237
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	238
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	239
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	240
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	241
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	242
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	243
		IF (C(1838).GT.C(1838)) C(1838) = C(1838)	10	244

SYMBOLIC REFERENCE MAP (K=3)									
ENTRY POINTS	DEF LINE	REFERENCES							
1 UOPT3	1	52							
VARIABLES	SN	TYPE	RELATION						
207 3	0	C	REAL	13	49	DEFINED	47		
3736 GPP			REAL	63	19*5	12	3*22	3*23	3*24
3147 DER			REAL	47	DEFINED	22	23	24	25
202 DER1			REAL	5	37				
3740 OTENT			REAL	32	32	33	34		
203 I			INTEGER	5	DEFINED				
3735 ITENT			INTEGER	4	13	DEFINED	63	DEFINED	40
204 J			INTEGER	2*48	45	47	49		45
205 K			INTEGER	5	27	28	DEFINED	28	
3136 KPOINT			INTEGER	47	52	53	DEFINED	46	61
3730 KPOINT			INTEGER	55	54	DEFINED	54		
3221 UNAME1			REAL	5	51			48	49
3745 CPPOINT			REAL	5	13	40			
3137 OUTNO			INTEGER	59	13	17	46		
3722 PCNT			REAL	12	19	62			
3737 PGONT			INTEGER	5	33	37	DEFINED	37	
3727 PPOINT			REAL	30	17	38	44	51	
3723 PPT			REAL	5	43	51			
3724 PPT			REAL	5	52	53	DEFINED	53	
3717 T			REAL	5	51				
3741 TASE			REAL	5	34	36	49	52	60
3742 TAPEND			REAL	5					
3750 TIME			REAL	5	15	DEFINED	60		
FILE NAMES									
TAPED			WRITE	34	40	47	56		
EXTERNALS									
DUMPO			TYPE	ARG3	REFERENCES	29			
STATEMENT LABELS									
36 1			DEF LINE	40	44				
145 2			FMT	41	40				
24 3				44	39				
0 4				47	45				
101 5			FMT	50	49				
23 7				32	27				
27 8				36	32				
0 9			INACTIVE	37					
0 10				63	64				
0 13			INACTIVE	56	55				
171 14			FMT	57	56				

STATEMENT LABELS	DEF LINE	REFERENCES	48
77 15	52	35	
112 16	53	55	
123 18	54	55	
131 20	35	34	
FMT			
LOOPS LABEL	INDEX	FROM-TO	LENGTH
41	1	40	100
51	2	45 47	33
120 10	J	51 63	33
COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)	
C	3830	0 C (3830)	
7	1	0 5844 11	
ENVIJ CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)	
C	3830	1984 OUTFLT (15)	
		2003 PPM (11)	1999 T (11)
		2003 N3PLT (11)	2004 PPP (11)
		2015 P5CNT (11)	2013 ITCNT (11)
		2018 TAPEND (11)	2014 CPP (11)
		2003 DER (11)	2017 TAGE (11)
		3217 ONAME1 (50)	2024 TIME (300)
			3166 M03JT (11)
			3157 OUTNO (150)

STATISTICS	
PROG LENGTH	2714 189
CM LABELLED COMMON LENGTH	73008 3830
CM LABELLED COMMON LENGTH	18

```

SUBROUTINE ZERO
COMMON /C/ C(3833)
EQUIVALENCE (C(1984),NPL0T)
EQUIVALENCE (C(2023),OPJINT)
EQUIVALENCE (C(2361),NOMOD)
EQUIVALENCE (C(2461),NOSUB)
EQUIVALENCE (C(3366),NOE13)
EQUIVALENCE (C(3167),NUOUT)
IMAGER UPPOINT
NOSUB = 0
NOMOD = 0
NUOUT = 0
NOE13 = 0
CPJINT=0
NPL0T=0
RETURN
END

```

SYMBOLIC REFERENCE TRIP (R=3)

ENTRY POINTS DEF LINE REFERENCES
1 ZERO 1

VARIABLES	SN	TYPE	RELOCATION	REFS	2	3	4	5	6	7	8	9
3771 NOLIST	C	REAL	C	REFS	7	DEFINED	13					
4470 NOYOD	C	INTEGER	C	REFS	5	DEFINED	11					
4130 NOOUT	C	INTEGER	C	REFS	8	DEFINED	12					
4034 NOSU3	C	INTEGER	C	REFS	6	DEFINED	10					
3077 NP-01	C	INTEGER	C	REFS	3	DEFINED	15					
3740 OPTINT	C	INTEGER	C	REFS	4	DEFINED	14					

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)
C 3030 0 C (3030)

ENVIV CLASSES LENGTH MEMBERS - BIAS NAME(LENGTH)
C 3030 1999 NP-01 111
2460 NOSU3 (1)

2082-000INT 111
3065 NOLIST (1)

2359 NOMOD 111
3156 NOOUT (1)

STATISTICS
PROGRAM LENGTH 68
CM LABELED COMMON LENGTH 73608 3930

FTN 4.2+74.353 07/0775 11.07.24.

SUBROUTINE FLCT4 74/74 OPT=1

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

7	I	X	PREVIOUSLY DIMENSIONED ARRAY. FIRST DIMENSIONS WILL BE RETAINED.
7	I	Y	PREVIOUSLY DIMENSIONED ARRAY. FIRST DIMENSIONS WILL BE RETAINED.

SYMBOLIC REFERENCE MAP (R33)

ENTRY POINTS 3 PL074	DEF LINE 1	REFERENCES 70				
VARIABLES	SN	TYPE	RELOCATION			
417 ALIN	REAL			52	57	71
				9		
420 ALIN2	REAL			30	39	59
				9		68
503 UX	REAL			54	62	71
477 UY	REAL			37	67	52
				2	68	35
476 I	REAL			2	2*11	1
				2*13	2*37	17
				53	2*54	36
				54		43
0 I1	INTEGER			13	24	24
				33		
472 I1K	INTEGER			13		
473 I1K	INTEGER			2*13	21	19
475 I1	INTEGER			9		
0 I1SCALE	INTEGER			15	34	51
0 I1TIME	INTEGER			51	1	1
410 K5	INTEGER			22	9	23
211 L63	INTEGER			2	71	11
213 L3C	INTEGER			7	58	10
421 N2	INTEGER			71	9	
422 N2	INTEGER			69	9	
473 N31	INTEGER			17	14	
474 N31OP	INTEGER			17	73	14
500 N1ICA	INTEGER			58	57	
502 N1ICV	INTEGER			43	42	
0 N1JP	INTEGER			14	35	73
0 VLAB	REAL			1	21	
507 X	REAL			7	2*10	1
				5	54	73
505 X*1	REAL			18	54	
0 X5X	REAL			59	52	62
0 X5IN	REAL			52	54	1
				52	2*54	71
0 X5AVE	REAL			1	14	
204 XA	REAL			7	51	
210 Y	REAL			59	52	57
				5	37	73
501 Y*1	REAL			18	37	
0 Y5X	REAL			44	43	46
0 Y5IN	REAL			35	37	15
				35	2*37	68
0 Y5AVE	REAL			1	13	
500 YV	REAL			7	13	47
				44	46	40
				44	47	47
EXTERNALS						
AXIS	TYPE	AMOD	REFERENCES			
INITIAL	5	5	58			
LINE	2	2	22			
NUMBER	0	0	44			
PLOT	3	3	27			
			59	31	33	39
			30	45	45	55
				46	55	56

EXTERNALS		TYPE	ARGS	REFERENCES	
KJTR			1	50	61
SCALE			5	26	74
SYMBOL			5	57	70
			5	50	64
INLINE FUNCTIONS					
NAME	REAL	TYPE	ARGS	DEF LINE	REFERENCES
AMAXI	REAL		0	INTRIN	37
AMINI	REAL		0	INTRIN	37
STATEMENT LABELS					
			DEF LINE	REFERENCES	
0 10			37		
0 20			49		
211 10			50		
220 11			51		
227 42			72		
0 50			20		
53 60			29		
57 61			32		
437 99	FM		12	18	11
0 100			54		
0 200			63		
LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES					
32 50	1		17 20	48	INSTACK
73 10	1		30 37	69	INSTACK
112 20	*	I	43 49	153	EXT REFS
150 100	I		53 54	68	INSTACK
167 200	*	I	54 63	158	EXT REFS
STATISTICS					
PROGRAM LENGTH				3159	339

SUBROUTINE	SUBLI	74/74	OPT=1	FTN 4,2474,355	07/0775	11.07.30.	PAGE	1
		SUBROUTINE SUBLI						
		COMMON /C/ C(3838)						
		EQUIVALENCE (C(2461),NOSUB), (C(2462),SUBMO)						
		DIMENSION SUBNO(99)						
5		DO 1 I = 1, NOSUB						
		J = SUBNO(I)						
		GO TO 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, J						
	2	CALL INPT1						
		GO TO 1						
10	3	CALL OUTP1						
		GO TO 1						
	4	CALL STGE1						
		GO TO 1						
	5	CALL CNTR1						
		GO TO 1						
15	6	CALL RND41						
		GO TO 1						
	7	CALL AUX41						
		GO TO 1						
20	8	CALL AUX41						
		GO TO 1						
	9	CALL AUXC1						
	1	CONTINUE						
		RETURN						
25		END						

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
1 SUB1 1 24

VARIABLES	SN	TYPE	RELOCATION	REFS	2	20-3
0 C		REAL	ARRAY C	REFS	2	20-3
44 J		INTEGER		REFS	5	DEFINED 5
45 J		INTEGER		REFS	7	DEFINED 6
4034 MOSUB		INTEGER	C	REFS	3	5
4035 SUBNO		REAL	ARRAY C	REFS	3	* 6

EXTERNALS	TYPE	SN	REFERENCES
AUXAL		0	18
AUXH1		0	20
AJAC1		0	22
CNTRI		0	14
INPTI		0	8
OUTPI		0	10
KNJMI		0	16
STGE1		0	12

STATEMENT LABELS	DEF LINE	REFERENCES	7	9	11	13	15	17	19	21
41 1	23	5								
22 2		7								
24 3		10								
26 4		12								
30 5		14								
32 6		16								
34 7		18								
36 8		20								
40 9		22								

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
3 1		5	23	419		

COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3630	0 C	(3830)

EQUIV CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3630	2460 MOSUB (11)	2461 SUBNO (99)

STATISTICS	PROGRAM LENGTH	CM LABELED COMMON LENGTH	73668	3630
			468	38

SYMBOLIC REFERENCE MAP (R=31)

ENTRY POINTS DEF LINE REFERENCES
1 SUBL2 1 25

VARIABLES	SN	TYPE	REAL	ARRAY	RELOCATION	REFS
44 I	1	INTEGER		C		7
43 J	1	INTEGER		C		7
+634 NUSUB		INTEGER		C		4
+635 SUBNO		REAL		C		5

EXTERNALS	TYPE	REFS
AUX42	0	19
AUX82	0	21
AUXC2	0	23
CNTR2	0	15
INPT2	0	9
OUTP2	0	11
KIND2	0	17
STSE2	0	13

STATEMENT LABELS	DEF LINE	REFERENCES	8	10	12	14	16	18	20	22
41 1	24	5	0							
22 2	11	8								
24 3	11	8								
26 4	13	8								
30 5	15	8								
32 6	17	8								
34 7	19	8								
38 8	21	8								
40 9	23	8								

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
3 1	1	5 24	418		

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	0 C (3830)

EQUIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
C	3830	2460 NUSUB (11)

STATISTICS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
PROGRAM LENGTH	468	38
COMMON LENGTH	7868	3830

2461 SUBNO (93)

SYMBOLIC REFERENCE MAP (2-3)

ENTRY POINTS DEF LINE REFERENCES
1 SUBL3 1 24

VARIABLES SN TYPE RELOCATION
0 C REAL ARRAY C

44 I INTEGER REFS 2
45 J INTEGER REFS 6
46 K INTEGER REFS 5
47 L INTEGER REFS 7
48 M INTEGER REFS 3
49 N INTEGER REFS 6
50 O SUBNO REAL ARRAY C

EXTERNALS TYPE REFS
AUX43 0 18
AUX83 0 20
AUXC3 0 22
CMT83 0 14
INPT3 0 8
OUT13 0 10
KNJMS 0 16
STSE3 0 12

STATEMENT LABELS DEF LINE REFERENCES
41 1 23 5 7 9 11 13 15 17 19 21
22 2 8 7
24 3 10 7
26 4 12 7
30 5 14 7
32 6 16 7
34 7 18 7
36 8 20 7
40 9 22 7

LDOPS LABEL INDEX FROM-TO LENGTH PROPERTIES EXT REFS
3 1 5 23 413

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)
C 3830 0 C (3830)

EQUIV CLASSES LENGTH MEMBERS - BIAS NAME(LENGTH)
C 3830 2460 NOSUB (1)

STATISTICS
PROGRAM LENGTH 468 38
CM LABELED COMMON LENGTH 73608 3830

SUBROUTINE	STGE2	7/4/74	OPT=1	FTN 4.2+74.355	07/07/76	11.07.33.	PAGE	1
SUBROUTINE STGE2								
COMMON /C/ C(1830)								
EQUIVALENCE (C(2011),KSTEP 1, (C(2020),LCONV 1, (C(2021),KCONV 1								
KCONV = 0								
LCONV = 0								
KSTEP = 1.								
RETURN								
END								
EXEC 78								
EXEC 79								
EXEC 80								
EXEC 81								
EXEC 82								
EXEC 83								
EXEC 84								
EXEC 85								

SUBROUTINE SIGEL2		74/74	OPI=1	FTN 4.2*74.355	07/07/75	11.07.33-	PAGE	2
SYMBOLIC REFERENCE MAP (R-3)								
ENTRY POINTS		DEF LINE	REFERENCES					
1		STGE2	7					
VARIABLES		SN	TYPE	RELOCATION	REFS			
0		C	REAL	ARRAY	C	2	8+3	
3744		KCONV	INTEGER		C	3	DEFINED	
3732		KSTEP	INTEGER		C	3	DEFINED	
3743		LCONV	INTEGER		C	3	DEFINED	
COMMON BLOCKS		LENGTH	MEMBERS - BIAS NAME(LENGTH)					
C		3838	0 C 138381					
EQUIV CLASSES		LENGTH	MEMBERS - BIAS NAME(LENGTH)					
C		3830	2010 KSTEP (1)			2019	LCONV	(1)
STATISTICS								
PROGRAM LENGTH		58						
CM LABELED COMMON LENGTH		78668 3838.						


```

SUBROUTINE STGL3
COMMON /C/ C(3638)
EQUIVALENCE (C(2001),T), (C(2001),TF), (C(2001),PCAT), (C(2001),PCAT)
EQUIVALENCE (C(2011),KSTEP), (C(2011),KCONV), (C(2011),KCONV), (C(2011),KCONV)
EQUIVALENCE (C(2021),M), (C(2021),M), (C(2021),M), (C(2021),M)
EQUIVALENCE (C(2031),MMAX), (C(2031),MMAX), (C(2031),MMAX), (C(2031),MMAX)
EQUIVALENCE (C(2041),DER), (C(2041),DER), (C(2041),DER), (C(2041),DER)
EQUIVALENCE (C(2051),VAR), (C(2051),VAR), (C(2051),VAR), (C(2051),VAR)
EQUIVALENCE (C(1973),KASE), (C(1973),KASE), (C(1973),KASE), (C(1973),KASE)
DIMENSION DER(101), VAR(101), (C(1974),NJ), (C(1975),NPT), (C(1976),ELT(100))
EXTERNAL AUXSUB
CALL CGL
IF (ABS(T-TF) .LE. 0.01) GO TO 20
IF (T-TF) .LT. 0.01 GO TO 10
IF (C(2011) .EQ. 2) GO TO 20
IF (C(2011) .EQ. 1) GO TO 10
IF (C(2011) .LT. 0.) DER(1)=-DER(1)*.5
RETURN
10 IF (C(2011) .GT. 0.) DER(1)=-DER(1)*.5
KCONV = KCONV + 1
IF (KCONV .GE. 10) GO TO 20
20 PCNT = 1.0
RETJRN
IF (STEP .EQ. 11) GO TO 40
PREJER = DER(1)
DER(1) = 0.
NJ=N-1
NPT=0
CALL AMR(AUXSUB)
DER(1) = PREJER
30 40 CALL OUP3
KSTEP = 2
RETJRN
END
EXEC 86
EXEC 87
EXEC 88
EXEC 89
EXEC 90
EXEC 91
EXEC 92
EXEC 93
EXEC 94
EXEC 95
EXEC 96
EXEC 97
EXEC 98
EXEC 99
EXEC 100
EXEC 101
EXEC 102
EXEC 103
EXEC 104
EXEC 105
EXEC 106
EXEC 107
EXEC 108
EXEC 109
EXEC 110
EXEC 111
EXEC 112
EXEC 113
EXEC 114
EXEC 115
EXEC 116
EXEC 117
EXEC 118

```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS 1 STAGE	DEF LINE 1	REFERENCES 17	21	32
VARIABLES	SN	TYPE	RELOCATION	
0 C	REAL	ARRAY	C	REFS
3147 DER	REAL	ARRAY	C	REFS
				DEFINED
3114 EL	REAL	ARRAY	C	REFS
3460 EU	REAL	ARRAY	C	REFS
3146 MAX	REAL	ARRAY	C	REFS
3149 MIN	REAL	ARRAY	C	REFS
3554 KASE	INTEGER	ARRAY	C	REFS
3724 KCONV	INTEGER	ARRAY	C	REFS
3732 KSTEP	INTEGER	ARRAY	C	REFS
3743 LCONV	INTEGER	ARRAY	C	REFS
3000 N	INTEGER	ARRAY	C	REFS
3055 NJ	INTEGER	ARRAY	C	REFS
3066 NPT	INTEGER	ARRAY	C	REFS
3722 PCVT	REAL	ARRAY	C	REFS
52 PREDER	REAL	ARRAY	C	REFS
3731 STEP	REAL	ARRAY	C	REFS
3717 T	REAL	ARRAY	C	REFS
3720 TP	REAL	ARRAY	C	REFS
3624 VAR	REAL	ARRAY	C	REFS

EXTERNALS

NAME	TYPE	ARGS	REFERENCES
AMK	REAL	1	28
AUXSUB	REAL	0	10
CUPT3	REAL	0	30

INLINE FUNCTIONS

NAME	TYPE	ARGS	DEF LINE	INTRIN	REFERENCES
ABS	REAL	1	1	1	12

STATEMENT LABELS

NAME	DEF LINE	REFERENCES
20 10	18	15
26 20	22	14
41 40	30	23

COMMON BLOCKS

NAME	LENGTH	MEMBERS	BIAS	NAME(LENGTH)
C	3630	0-3	438300	

EXIV CLASSES

NAME	LENGTH	MEMBERS	BIAS	NAME(LENGTH)
C	3630	0-3	438300	
1974 NPT	(1)	1973 NJ	(1)	1974 NPT
2002 PCVT	(1)	2000 TF	(1)	2002 PCVT
2019 LCONV	(1)	2010 KSTEP	(1)	2019 LCONV
2551 MIN	(1)	2560 N	(1)	2551 MIN
2754 EL	(100)	2663 DER	(101)	2754 EL
		2664 VAR	(101)	

STATISTICS

PROGRAM LENGTH	538	43
CH LABELED COMMON LENGTH	73669	3630

SUBROUTINE RESET	74704	OPT=1	FTN 4.2+74355	07/07/75	11.07.34.	PAGE	1
SUBROUTINE RESET							
COMMON /C/ C13810							
EQUIVALENCE (C138681,NOLIST), (C13067),LISTNO), (C13117),VALUE)							
DIMENSION LISTNO(50)							
IF (NOLIST.EQ..0) RETURN							
DO 1 I = 1, NOLIST							
J = LISTNO(I)							
1 C(I) = VALUE(I)							
RETURN							
END							
10				EXEC	119		
				EXEC	120		
				EXEC	121		
				EXEC	122		
				EXEC	123		
				EXEC	124		
				EXEC	125		
				EXEC	126		
				EXEC	127		
				EXEC	128		

07/07/75 11.07.34.

FTN 4.2+74.353

OPT=1

74/74

SUBROUTINE RESET

DIAGNOSIS OF PROBLEM

CARD NR. SEVERITY DETAILS

8 I NOLIST THIS STATEMENT MAY REDEFINE A CURRENT LOOP CONTROL VARIABLE OR PARAMETER.

SYMBOLIC REFERENCE VAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	9
1 RESET	5		
VARIABLES	SN	TYPE	RELOCATION
0 C	ARRAY	C	
11 I	REAL	REFS	2
12 J	INTEGER	REFS	7
3772 LISTNO	INTEGER	REFS	0
3771 NOLIST	INTEGER	REFS	3
3054 VAL-UE	REAL	REFS	3
STATEMENT LABELS	DEF LINE	REFERENCES	
0 1	8	5	
LDOPS LABEL	INDEX	FROM-TO	LENGTH
0 1	1	0 9	38
COMMON BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)
C	3830	0 C	(3830)
EVUIV CLASSES	LENGTH	MEMBERS	- BIAS NAME(LENGTH)
C	3830	3065 NOLIST (1)	
STATISTICS	PROGRAM LENGTH	138	11
	CM LABELED COMMON LENGTH	73669	3830
	3066 LISTNO (50)		3116 VAL-UE (50)

SUBROUTINE TABLE	74/74	OPT=1	FTN +.2+7.355	07/07/75	11.07.34.	PAGE
						1
SUBROUTINE TABLE (X,XI,YI,NX,XK,XLABEL,Y)						
DIMENSION XLABEL (2)						
XK = 0.						
Y = FINIP1 (X,XI,YI,NX,XK,XLABEL)						
RETURN						
END						
5				EXEC	129	
				EXEC	130	
				EXEC	131	
				EXEC	132	
				EXEC	133	
				EXEC	134	

SYMBOLIC REFERENCE MAP (R=37)

[illegible]

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
3 TABL2 1 5

VARIABLES	SN	TYPE	RELOCATION	REFS	DEF	DEFINED
0 X	1	INTEGER	ARRAY	REFS	3	44
0 X	2	REAL		REFS	4	DEFINED
0 X	3	REAL		REFS	4	DEFINED
0 X	4	REAL		REFS	2	DEFINED
0 X	5	REAL		REFS	3	DEFINED
0 X	6	REAL		REFS	4	DEFINED
0 X	7	REAL		REFS	1	DEFINED
0 X	8	REAL		REFS	4	DEFINED
0 X	9	REAL		REFS	1	DEFINED

EXTERNALS TYPE ARGS REFERENCES
FINTP2 REAL 10 4

STATISTICS

PROGRAM LENGTH 408 32

SUBROUTINE TABL3	74/74	OPT=1	FTN 4.2+74.335	07/07/75	11-07-36	PAGE	1
SUBROUTINE TABL3(X,Y,Z,XYZI,WI,NXYZ,XINTER,XLABEL)							
DIMENSION XLABEL(2)							
DIMENSION XYZI(1),NXYZ(1)							
NZI= NXYZ(1) + NXYZ(2) + 1							
XINTER = 0.							
N = FINTP3 (X,Y,Z,XYZI,XYZI(NXYZ+1),XYZI(NZI), #1,NXYZ(3) +							
C NXYZ(2),NXYZ,XINTER,XLABEL)							
RETURN							
END							

EXEC	141
EXEC	142
EXEC	143
EXEC	144
EXEC	145
EXEC	146
EXEC	147
EXEC	148
EXEC	149

SYMBOLIC REFERENCE MAP (3=3)

ENTRY POINTS DEF LINE REFERENCES

3 TABL3 1 5

VARIABLES SN TYPE RELOCATION

VARIABLES	SN	TYPE	RELOCATION	F.P.	REFS	2-4	*6	DEFINED
0 NXYZ		INTEGER	ARRAY	F.P.	REFS	3	4	1
+7 NZI		INTEGER			REFS	1	5	
0 M		REAL		F.P.	DEFINED			
0 H		REAL		F.P.	REFS	5		
0 K		REAL		F.P.	REFS	5	1	
0 X		REAL		F.P.	REFS	5	1	
0 XINTER		REAL		F.P.	REFS	5	1	5
0 XLABEL		REAL	ARRAY	F.P.	REFS	2	5	1
0 XYZI		REAL	ARRAY	F.P.	REFS	3	3+6	1
0 Y		REAL		F.P.	REFS	5	1	
0 Z		REAL		F.P.	REFS	5	1	

EXTERNALS TYPE ARGS REFERENCES

0 12 0

STATISTICS PROGRAM LENGTH

508 40

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES

4 COJIM2 3 12

4 FINTP1 1

VARIABLES SN TYPE RELOCATION

0 F REAL F.P.

40 FINTP1 REAL F.P.

41 I INTEGER F.P.

42 PCI REAL F.P.

0 XI REAL F.P.

0 XL REAL F.P.

0 YI REAL F.P.

STATEMENT LABELS DEF LINE REFERENCES

0 10 7 5

22 20 9 6

31 30 11 4

LOOPS LABEL * I INDEX FROM-TO LENGTH PROPERTIES

15 10 2 7 33 INSTACK EXITS

STATISTICS

PROGRAM LENGTH

438 35

FUNCTION FINTP2

2

SYMBOLIC REFERENCE MAP (R=3)									
ENTRY POINTS		DEF LINE	REFERENCES						
+ FCODE2		3	14						
+ FINTP2		1							
VARIABLES		SN	TYPE	RELOCATION					
				F.P.	REFS	4	12	DEFINED	1
71 FINTP2		0	F	REAL	DEFINED	13			
72 I		72	I	INTEGER	REFS	6	3*9	11	DEFINED
74 J		74	J	INTEGER	REFS	11	12	DEFINED	10
75 L		75	L	INTEGER	REFS	12	11	DEFINED	
0 NX		0	NX	INTEGER	REFS	12	DEFINED	1	
0 ND		0	ND	INTEGER	REFS	2	DEFINED	1	
0 NY		0	NY	INTEGER	REFS	5	9	DEFINED	1
73 PCI		73	PCI	REAL	REFS	13	DEFINED	9	
76 T		76	T	REAL	REFS	2	3*13	DEFINED	12
0 X		0	X	REAL	REFS	12	DEFINED	1	
0 XL		0	XL	REAL	REFS	2	12	DEFINED	1
0 Y		0	Y	REAL	REFS	2	12	DEFINED	1
0 YI		0	YI	REAL	REFS	5	9	DEFINED	1
0 ZI		0	ZI	REAL	REFS	2	5	3*9	DEFINED
					REFS	2	12	DEFINED	1
EXTERNALS		TYPE	ARGS	REFERENCES					
FINTP1		REAL	5	12					
STATEMENT LABELS		DEF LINE	REFERENCES						
0 10		7	5						
26 20		9	6						
33 30		10	4						
0 40		12	10						
LOOPS LABEL		INDEX	FROM-TO	LENGTH	PROPERTIES				
21 10		* I	5	7	38	INSTACK	EXITS		
34 40		* J	10	12	208	EXT REFS	EXT REFS		
STATISTICS									
PROGRAM LENGTH		1008 64							

FUNCTION FINP3	7/4/74	OPT=1	FTN **2*7*355	07/07/75	11.07.39.	PAGE	1
<pre> FUNCTION FINP3(X,Y,ZI,XI,YI,ZI,MI,NZ,NT,NX,F,XL) DIMENSION XI(1), YI(1), ZI(1), MI(NX,NT,1), T(2), XL(2) ENTRY FCOONS DO 10 I=2, NZ IF (ZI(I) .LE. ZI(1)) GO TO 20 10 CONTINUE I = NZ 20 PCT = (ZI(1)-ZI(I))/(ZI(1)-ZI(I-1)) 30 DO 40 J=1,2 L = I + J - 2 40 T(J) = FINTP2(X,Y,XI,YI,MI(I,1,L),NX,NY,NX,F,XL) FINP3 = T(1) + PCT*(T(2)-T(1)) RETURN END </pre>							
				EXEC	170		
				EXEC	171		
				EXEC	172		
				EXEC	173		
				EXEC	174		
				EXEC	175		
				EXEC	176		
				EXEC	177		
				EXEC	178		
				EXEC	179		
				EXEC	180		
				EXEC	181		
				EXEC	182		
				EXEC	183		
				EXEC	184		
				EXEC	185		
				EXEC	186		
				EXEC	187		
				EXEC	188		
				EXEC	189		
				EXEC	190		
				EXEC	191		

SYMBOLIC REFERENCE MAP (R-S)

ENTRY POINTS DEF LINE REFERENCES

4 ECDN3 3 13
4 FINP3 1

VARIABLES	SN	TYPE	RELOCATION	F.P.	REFS	DEF	LINE	REFERENCES
0 F		REAL			DEFINED	11	DEFINED	1
101 FINP3		REAL			REFS	12		
102 I		INTEGER			REFS	5	3*8	10
104 J		INTEGER			REFS	10	11	DEFINED
105 L		INTEGER			REFS	11	DEFINED	10
0 NX		INTEGER			REFS	2	2*11	DEFINED
0 NY		INTEGER			REFS	2	11	DEFINED
0 NZ		INTEGER			REFS	4	7	DEFINED
103 PCT		REAL			REFS	12	3*12	DEFINED
100 T		REAL	ARRAY		REFS	2	11	DEFINED
0 MI		REAL	ARRAY		REFS	2	11	DEFINED
0 XI		REAL	ARRAY		REFS	11	DEFINED	1
0 XL		REAL	ARRAY		REFS	2	11	DEFINED
0 YI		REAL	ARRAY		REFS	11	DEFINED	1
0 ZI		REAL	ARRAY		REFS	5	9	DEFINED
0 ZI		REAL	ARRAY		REFS	2	3	DEFINED

EXTERNALS TYPE ARG'S REFERENCES

FINP2 REAL 10 11

STATEMENT LABELS DEF LINE REFERENCES

0 10 0 4
23 20 8 5
0 30 9
0 40 11 9

LOOPS LABEL INGER FROM-TO LENGTH PROPERTIES

20 10 1 9 11 253
33 40 1 9 11 253

STATISTICS

PROGRAM LENGTH 1104 72

SUBROUTINE DUMMY		
C DUMMY SUBROUTINE		
5	ENTRY A21	EXEC 198
	ENTRY A4	EXEC 193
	ENTRY A41	EXEC 194
	ENTRY A5	EXEC 195
	ENTRY A51	EXEC 196
	ENTRY C21	EXEC 197
	ENTRY C2	EXEC 198
	ENTRY C5	EXEC 199
10	ENTRY C61	EXEC 200
	ENTRY C7	EXEC 201
	ENTRY C71	EXEC 202
	ENTRY C8	EXEC 203
	ENTRY C81	EXEC 204
15	ENTRY C9	EXEC 205
	ENTRY C91	EXEC 206
	ENTRY C10	EXEC 207
	ENTRY C101	EXEC 208
20	ENTRY C3	EXEC 209
	ENTRY C31	EXEC 210
	ENTRY C4	EXEC 211
	ENTRY C41	EXEC 212
	ENTRY C5	EXEC 213
25	ENTRY C51	EXEC 214
	ENTRY C6	EXEC 215
	ENTRY C61	EXEC 216
30	ENTRY C31	EXEC 217
	ENTRY C41	EXEC 218
	ENTRY C51	EXEC 219
	ENTRY C61	EXEC 220
35	ENTRY C71	EXEC 221
	ENTRY C81	EXEC 222
	ENTRY C91	EXEC 223
	ENTRY C101	EXEC 224
	ENTRY C11	EXEC 225
	ENTRY C12	EXEC 226
	ENTRY C13	EXEC 227
	ENTRY C14	EXEC 228
40	ENTRY C15	EXEC 229
	ENTRY C16	EXEC 230
	ENTRY C17	EXEC 231
	ENTRY C18	EXEC 232
	ENTRY C19	EXEC 233
45	ENTRY C20	EXEC 234
	ENTRY C21	EXEC 235
	ENTRY C22	EXEC 236
	ENTRY C23	EXEC 237
	ENTRY C24	EXEC 238
50	ENTRY C25	EXEC 239
	ENTRY C26	EXEC 240
	ENTRY C27	EXEC 241
	ENTRY C28	EXEC 242
	ENTRY C29	EXEC 243
55	ENTRY C30	EXEC 244
	ENTRY C31	EXEC 245
	ENTRY C32	EXEC 246
	ENTRY C33	EXEC 247
	ENTRY C34	EXEC 248

SUBROUTINE DUMMY	74/74	OPT=1	FIN +.247335	07/07/75	11.07.39*	PAGE	2
60	ENTRY INPT3			EXEC	249		
	ENTRY DUP11			EXEC	250		
	ENTRY PROJES			EXEC	251		
	ENTRY KNOM1			EXEC	252		
	ENTRY KNOM2			EXEC	253		
	ENTRY KNOM3			EXEC	254		
	ENTRY STREET			EXEC	255		
65	ENTRY KIKSET			EXEC	256		
	ENTRY COUNTV			EXEC	257		
	ENTRY TIMEV			EXEC	258		
	ENTRY WRITE			EXEC	259		
	RETJRN			EXEC	260		
70	END			EXEC	261		

SYMBOLIC REFERENCE MAP (4-3)

ENTRY POINTS	DEF LINE	REFERENCES
1 AUXAI	44	
1 AUXAE	45	
1 AUXAS	46	
1 AUXSI	47	
1 AUXB2	48	
1 AUXB3	49	
1 AUXCI	50	
1 AUXCE	51	
1 AUXCS	52	
1 RZT	3	
1 F4	4	
1 A+I	5	
1 A5	6	
1 A5I	7	
1 CNFRI	53	
1 CNFRI2	54	
1 CNFRI3	55	
1 CUNTV	66	
1 CIO	18	
1 CIOI	19	
1 C2	3	
1 C2I	8	
1 Co	10	
1 G6I	11	
1 G7	12	
1 G7I	13	
1 L8	14	
1 C8I	15	
1 C9	16	
1 C9I	17	
1 DUMMY	1	
1 G3	20	
1 J3I	21	
1 J4I	22	
1 J4I3	23	
1 J5	24	
1 J4I	25	
1 G1	26	
1 G1I	27	
1 G3I	28	
1 G4I	29	
1 G5I	30	
1 G6	31	
1 G6I	32	
1 IVPII	56	
1 IMP12	57	
1 IMP13	58	
1 K1SET	65	
1 WPII	59	
1 PROCS	60	
1 ENDMI	61	
1 RNDM2	62	
1 RNDMI	63	
1 S1SEI	64	

SUBROUTINE DUMMY				74/74	OPT=1	FTN +.2+7.355	07/07/75	11.07.39.	PAGE	4
ENTRY POINTS	DEF LINE	REFERENCES								
1 S10	42									
1 S11	43									
1 S3	33									
1 S51	34									
1 S8	35									
1 S81	36									
1 S7	37									
1 S71	38									
1 S81	39									
1 S3	40									
1 S91	41									
1 T1REV	67									
1 WRITE	68	69								
STATISTICS										
PROGRAM LENGTH				33	3					

SYMBOLIC REFERENCE MAP (R=3)										
ENTRY PCINTS		DEF LINE	REFERENCES							
3		TERROR	1	10						
VARIABLES		SM	TYPE	RELOCATION						
0	C	REAL	ERRAY	C	REFS	5				
17+3	LCUNV	INTEGER		C	REFS	5				
0	KLABEL	REAL		P.P.	REFS	6	DEFINED	1		
FILE NAMES		MODE								
TAPE0	FMT		WRITES	6						
EXTERNALS		TYPE	ARGS	REFERENCES						
EXIT			0	9						
STATEMENT LABELS		DEF LINE	REFERENCES							
10	10	FMT	7	0						
COMMON BLOCKS		LENGTH	MEMBERS - BIAS NAME(LENGTH)							
0		3830	0 0 (3830)							
ENJIV CLASSES		LENGTH	MEMBERS - BIAS NAME(LENGTH)							
0		3830	2019 LCUNV (1)							

SUBROUTINE AEROR	7/7/74	DPT=1	FTN 4,2+74355	07/07/75	11.07.48.	PAGE	1
SUBROUTINE AEROR (XLABEL)							
COMMON /C/ C(3833)							
EQUIVALENCE (C(2820),LCONV)							
WRITE (6,20) XLABEL							
3	RETURN						
20 FORMAT (1,43H0 OUT OF AERO TABLE ARGUMENT ARRAY , 5X,							
C FMTABLE , 18F7)							
DO 40 I=1,202,1251,7							
10	40 WRITE(6,30) C(I),C(I+1),C(I+2),C(I+3),C(I+4),C(I+5),C(I+6)						
30 FORMAT(14,7E15,7)							
WRITE (6,30) C(2800),C(367),C(368),C(369),C(369),C(370),C(1117),							
C C(1118),C(1119),C(1120)							
LCONV=C							
RETURN							
15	END						

SUBROUTINE ERROR	74/74	OPI=1	FTN 4.2+74.355	07/07/76	11.07.40.	PAGE	2
CARD NR. SEVERITY DETAILS	DIAGNOSIS OF PROBLEM						
0	1	THERE IS NO PATH TO THIS STATEMENT.					

SYMBOLIC REFERENCE MAP (R-3)									
ENTRY POINTS	DEF LINE	REFERENCES							
3 AERKOR	1	5	14						
VARIABLES	SN	TYPE	RELOCATION						
0 C		REAL	ARRAY C						
101 I		INTEGER							
3743 LCONV		INTEGER	C						
0 XLABEL		REAL	F.P.						
FILE NAMES	MODE								
TR=20	FMT		WRITES	4	9	11			
STATEMENT LABELS	DEF LINE	REFERENCES							
37 20	FMT	6							
61 30	FMT	10	9	11					
0 40		9	8						
LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES				
11 40	* I		8 9	178	EXT REFS				
COMMON BLOCKS	LENGTH		MEMBERS	- BIAS NAME(LENGTH)					
C	3 80		0 C	(3830)					
EQUIV CLASSES	LENGTH		MEMBERS	- BIAS NAME(LENGTH)					
C	3830		2019 LCONV (11)						
STATISTICS									
PROGRAM LENGTH	1028	65							
CH LABELED COMMON LENGTH	73668	3830							

FUNCTION SIND	7/4/74	OPT=1	FTN +027,355	07/07/75	11.07.41.	PAGE
FUNCTION SIND (X)				EXEC	287	
SIND= SIN (X/57.29578)				EXEC	288	
RETURN				EXEC	289	
END				EXEC	290	

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES			
4 SIND	1	3			
VARIABLES	SN	TYPE	RELOCATION		
12 SIND	REAL		DEFINED	2	DEFINED 1
0 A	REAL		REFS	2	
			F.P.		
EXTERNALS	SIN	TYPE	ARGS	REFERENCES	
	REAL		1 LIBRARY	2	
STATISTICS					
PROGRAM LENGTH				138	11

FUNCTION COSD 7474 OPT=1 FTN 4.2*74355 07/07/75 11.07.41. PAGE 1

FUNCTION COSD (N)
COSD= COS (X/57.29576)
RETURN
END

EXEC 291
EXEC 292
EXEC 293
EXEC 294

=FUNCTION COSD		74/74		OPT=1		FT4 4.2*74355		07/07/76		11.07.41.		PAGE		2	
SYMBOLIC REFERENCE MAP (R-S)															
ENTRY POINTS		DEF LINE		REFERENCES											
4 COSD		1		3											
VARIABLES		SN		TYPE		RELOCATION		DEFINED		REFS		DEFINED		1	
12 COSD		REAL						2		2		DEFINED			
0 X		REAL						F.P.							
EXTERNALS		TYPE		ARGS		REFERENCES									
COS		REAL		1		LIBRARY		2							
STATISTICS															
PROGRAM LENGTH												138		11.	

FUNCTION ATAND	7/4/74	DPF=1	FTN 4,2*74,355	07/07/76	11-07-51.	PAGE 1
FUNCTION ATAND (Y,X)						
ATAND= 57.29578*ATAM2 (Y,X)						
RETURN						
END						
EXEC 295						
EXEC 296						
EXEC 297						
EXEC 298						

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS DEF LINE REFERENCES
4 ATAND 1 3

VARIABLES	SN	TYPE	RELOCATION	DEFINED	REFS	DEFINED	REFS
13 ATAND		REAL		2	2	2	2
0 X		REAL					
0 Y		REAL					

EXTERNALS ATAND2 TYPE ARGUS REFERENCES
REAL 2 LIBRARY 2

STATISTICS
PROGRAM LENGTH 148 12

SUBROUTINE S21	7474	OPT=1	FTN 4.2474.355	07/07/76	11.07.42.	PAGE 3
115	C	DATA FFOV, TARM, TARMO, TAU, AGV, CFREQ, WUI, KWD, KPD, KPT		S2	116	
	C			S2	117	
	C	DATA K80, K81, K80O, KOAI		S2	119	
120	C			S2	120	
	C			S2	121	
	C	IS3=0		S2	122	
	C			S2	123	
125	C			S2	124	
	C			S2	125	
	C			S2	126	
	C			S2	127	
	C	IF (S266).GT..0005)WRITE(6,112)		S2	128	
130	C	112 FORMAT('*****INTEGRATION STEP SIZE IS GREATER THAN THE RECOMMENDED VALUE FOR SEEKER MODEL S2.4,11X,RECOMMENDED VALUE IS .0 S2		S2	129	
	C	3805 SEC. CHECK RESULTS FOR VALIDITY.~,10(f))		S2	130	
	C	GO TO 10		S2	131	
	C			S2	132	
	C			S2	133	
	C			S2	134	
135	C	ENTRY S31		S2	135	
	C	C**LOW FREQUENCY SEEKER		S2	136	
	C			S2	137	
	C			S2	138	
	C			S2	139	
	C			S2	140	
140	C	IPLIN=500		S2	141	
	C	IPLIN=11=501		S2	142	
	C	IPLIN=21=506		S2	143	
	C	IPLIN=31=507		S2	144	
	C	IPLIN=41=512		S2	145	
	C	IPLIN=51=513		S2	146	
	C	IPLIN=61=514		S2	147	
	C	IPLIN=71=520		S2	148	
	C	IPLIN=81=424		S2	149	
	C	IPLIN=91=426		S2	150	
	C	N=10		S2	151	
150	C	GO TO 20		S2	152	
	C			S2	153	
	C			S2	154	
	C			S2	155	
155	C			S2	156	
	C			S2	157	
	C			S2	158	
	C			S2	159	
160	C			S2	160	
	C			S2	161	
	C			S2	162	
	C			S2	163	
	C			S2	164	
165	C			S2	165	
	C			S2	166	
	C			S2	167	
	C			S2	168	
	C			S2	169	
170	C			S2	170	
	C			S2	171	
	C			S2	172	

SUBROUTINE S21	7/4/74	OPT=1	FTN 4.2+74.355	07/07/75	11.07.82.	PAGE	4
175	20	CONTINUE				S2	175
	1	C(1)=0.				S2	176
		C(155)=C(2000)-C(2654)				S2	177
		DO 7 I=1,6				S2	178
180		C(655-I)=C(656-I)-C(2664)				S2	179
		C(655+I)=0.				S2	180
		C(651+I)=0.				S2	181
185	7	CONTINUE				S2	182
		C(13)=1.				S2	183
		C(451)=0.				S2	184
		C(452)=0.				S2	185
		C(453)=0.				S2	186
		C(454)=0.				S2	187
190		IF(501*W6111) 50 TO 3				S2	188
		C(451)=1.				S2	189
		C(452)=1.				S2	190
		C(453)=1.				S2	191
		C(454)=1.				S2	192
195	3	CONTINUE				S2	193
		TO=1440.				S2	194
		C(451)=0.				S2	195
		C(452)=0.				S2	196
		C(453)=0.				S2	197
		C(454)=0.				S2	198
200		DEFSV=.002				S2	199
		BEFSV=0.				S2	200
		BEFSV=0.				S2	201
		TUI=0.				S2	202
205		GQ1=KQ1*KQ2/CK40				S2	203
		GRI=KK1*KR2/CR40				S2	204
		GQ2=KQ3*WQ2/WTQ1				S2	205
		GR2=KK3*WR2/WTQ1				S2	206
210		GQ3=KQ5*WQ3*WQ35*WQ4/(WQ1*WQ3*WQ5)				S2	207
		GR3=KK5*WR5*WR5*WR4/(WR1*WR3*WR5)				S2	208
		GQ4=KQ6*KQ7				S2	209
		GR4=KK6*KR7				S2	210
215		GQ5=KQ10*WQ2*WQ12/CR40				S2	211
		GR5=KR10*WR2*WR12/CR40				S2	212
		GQ6=KQ11*WQ3*WQ34				S2	213
		GR6=KR11*WR3*WR34				S2	214
		RANGE=SQRT(C(1635)*C(1635)+C(1636)*C(1636)+C(1637)*C(1637))				S2	215
		THI2=ATAN2(THI1,RANGE)/2.				S2	216
		THI2=ATAN2(THI1,RANGE)/2.				S2	217
220	C	1005=10				S2	218
		IF(153*EQ.0) GO TO 6				S2	219
		GQ3=KQ5*WQ4/WQ1/WQ3				S2	220
		GR3=KK5*WR4/WR1/WR3				S2	221
225		GQ5=KQ10*KQ11/CR40				S2	222
		GR5=KR10*KR11/CR40				S2	223
	5	CONTINUE				S2	224
	6					S2	225

SUBROUTINE S21	7/4/74	OPT=1	FTN 4.2+74.355	07/07/75	11.07.42	PAGE	5
230			00 30 1-1,13512			230	
			100=1			231	
	C					232	
	C		C**MONTE CARLO MASS UNBALANCE ON SEEKER GYRO			233	
	C					234	
235			IF(1SNX(1).EQ.611)CALL MCARLO(100, 1, 100)			235	
			IF(1SNX(1).EQ.611)CALL RANUM(10, 1, 100, 1, 100)			236	
			KUU=SIGN(KUU, RN)			237	
			IF(1SNX(1).EQ.612)CALL MCARLO(100, 1, 100)			238	
			IF(1SNX(1).EQ.612)CALL RANUM(10, 1, 100, 1, 100)			239	
			CHI=360.*RN			240	
240	C		C**MONTE CARLO SEEKER RATE GYRO ERRORS			241	
	C					242	
			IF(1SNX(1).EQ.613)CALL MCARLO(100, 1, 100)			243	
			IF(1SNX(1).EQ.614)CALL MCARLO(100, 1, 100)			244	
245			IF(1SNX(1).EQ.615)CALL MCARLO(100, 1, 100)			245	
			IF(1SNX(1).EQ.615)CALL RANUM(10, 1, 100, 1, 100)			246	
			CHI=360.*RN			247	
			IF(1SNX(1).EQ.616)CALL MCARLO(100, 1, 100)			248	
			IF(1SNX(1).EQ.617)CALL MCARLO(100, 1, 100)			249	
250			IF(1SNX(1).EQ.618)CALL MCARLO(100, 1, 100)			250	
			UCC=COS(4CHI)			251	
			USC=SIN(4CHI)			252	
			UCC=COS(4CHI)			253	
			USC=SIN(4CHI)			254	
255	30		CONTINUE			255	
			RETURN			256	
			END			257	
						258	

ENTRY POINTS	DEF LINE	REFERENCES
1	1	1
2	2	2
3	3	3
4	4	4
5	5	5
6	6	6
7	7	7
8	8	8
9	9	9
10	10	10
11	11	11
12	12	12
13	13	13
14	14	14
15	15	15
16	16	16
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18	18	18
19	19	19
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93	93	93
94	94	94
95	95	95
96	96	96
97	97	97
98	98	98
99	99	99
100	100	100

VARIABLES	SN	TYPE	RELOCATION	DEFINED	DEFINITION	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000
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ARMY MISSILE RESEARCH DEVELOPMENT AND ENGINEERING LAB--ETC F/G 16/4
THAD T-7 MISSILE MONTE-CARLO TERMINAL HOMING SIMULATION UTILIZI--ETC(U)
JUL 76 C L LEWIS, W R HOOKER, A W LEE

UNCLASSIFIED

RG-7T-2

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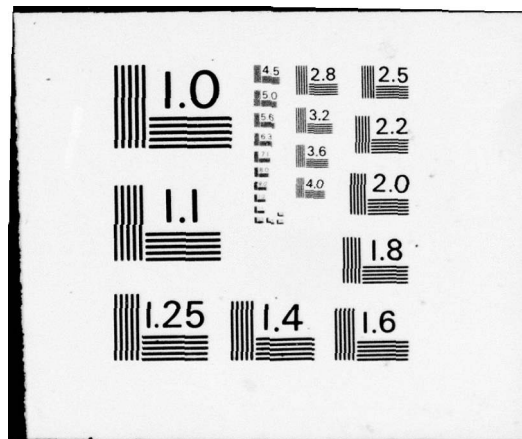
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VARIABLES	SN	TYPE	RELOCATION	REFS	23	212	DEFINED	104	104
1053 KRP	REAL	C		9	23	212	DEFINED	104	104
1053 PR3	REAL	C		9	23	212	DEFINED	104	104
423 KR3	REAL	*UNDEF		9	23	212	DEFINED	104	104
1113 KUI	REAL	C		10	90	216	DEFINED	116	116
1112 KUD	REAL	C		10	90	216	DEFINED	116	116
1000 N	INT:GER	C		83	133	140	141	142	143
				140	147	148	149	150	151
				151	156	156	159	160	161
				153	165	166	167	168	169
				171	173	174	DEFINED	149	174
				172	173	174	DEFINED	149	174
				173	173	174	DEFINED	149	174
				174	173	174	DEFINED	149	174
1057 OPTM4	REAL	C		38	190				
1072 QEG	REAL	C		38	190				
774 Q1	REAL	C		62					
774 Q2	REAL	C		62					
1002 G3	REAL	C		64					
1013 Q4	REAL	C		66					
1024 Q5	REAL	C		69					
1035 Q6	REAL	C		72					
1035 Q6	REAL	C		74					
1132 RAYG2	REAL	C		56	249	219	DEFINED	212	212
1132 RAYG2	REAL	C		48	79	DEFINED	113		
1124 RCL	REAL	C		36	DEFINED	113			
1073 R2G	REAL	C		39					
431 RN	REAL	C		235	235	210	239	246	247
430 RNSTR	REAL	C		235	239	246			
777 R1	REAL	C		63					
775 R2	REAL	C		65					
1008 R3	REAL	C		67					
1014 R4	REAL	C		70					
1025 R5	REAL	C		73					
1036 R6	REAL	C		75					
1130 TATM	REAL	C		46	49	210	DEFINED	116	116
1131 TARM	REAL	C		46	49	210	DEFINED	116	116
1127 TAJ	REAL	C		39	DEFINED	116			
1125 TC-Q	REAL	C		37	DEFINED	113			
1126 TCR	REAL	C		30	DEFINED	113			
1137 TOLAY	REAL	C		51	79	DEFINED	196		
1130 TMT3	REAL	C		51	79	DEFINED	196	210	219
1141 TMT3	REAL	C		51	79	DEFINED	196	219	219
1023 TMT3V	REAL	C		52					
1135 TLAG	REAL	C		36	DEFINED	203			
1078 TUI	REAL	C		37	DEFINED	204			
1071 TUD	REAL	C		34	DEFINED	241			
1122 UG3	REAL	C		94	DEFINED	251			
1134 UG3	REAL	C		95	DEFINED	253			
1153 US3	REAL	C		94	DEFINED	252			
1155 US3	REAL	C		95	DEFINED	254			
1100 WQ1	REAL	C		16	269	253	DEFINED	187	187
1102 WQ2	REAL	C		18					
1104 WQ3	REAL	C		20	269	253	DEFINED	187	187
1106 WQ4	REAL	C		22	269	253	DEFINED	187	187
1110 WQ5	REAL	C		24	269	253	DEFINED	187	187
1112 WQ6	REAL	C		26	2*209	DEFINED	118		
1101 WQ7	REAL	C		17	269	254	DEFINED	187	187
1103 WQ8	REAL	C		19					
1105 WQ9	REAL	C		21	269	254	DEFINED	187	187
1107 WQ9	REAL	C		23	210	254	DEFINED	187	187
1111 WQ9	REAL	C		25	240	DEFINED	118		

VARIABLES	SN	TYPE	RELOCATION	REFS	27	2*210	DEFINED	110
1113 MGR6	REAL	C		REFS	71			
1012 M1	REAL	C		REFS	60			
1004 M0	REAL	C		REFS	28			
1114 M21	REAL	C		REFS	30	2*213	DEFINED	110
1116 M22	REAL	C		REFS	32			
1120 M23	REAL	C		REFS	34	2*215	DEFINED	110
1122 M24	REAL	C		REFS	29			
1115 M21	REAL	C		REFS	31	2*214	DEFINED	110
1117 M22	REAL	C		REFS	33			
1121 M23	REAL	C		REFS	35	2*216	DEFINED	110
1123 M24	REAL	C		REFS	12	207	DEFINED	107
1074 M21	REAL	C		REFS	14	208	DEFINED	107
1076 M22	REAL	C		REFS	13	209	DEFINED	107
1075 M21	REAL	C		REFS	15			
1077 M22	REAL	C		REFS				

FILE NAMES	MODE	WRITES	126
EXTERNALS	TYPE	ARGS	REFERENCES
ATAND	REAL	2	210 219
COSD	REAL	1	251 253
MCARLO	REAL	3	234 237 243
MANNUM	REAL	3	235 238 246
SIND	REAL	1	252 254
SURT	REAL	1	LIBRARY 217

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
SIGN	REAL	2	INTRIN	236

STATEMENT LABELS	DEF LINE	REFERENCES
0 1	177	176
132 3	195	190
236 6	227	222
0 7	184	190
36 10	151	132
101 20	179	190
0 30	255	229
366 112	127	126

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
103 1	1	176 177	23	INSTACK	
113 7	1	180 184	28	INSTACK	
237 30	1	229 255	770	EXT REFS	

COMMON BLOCKS	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3830	0 C	(3930)

STUDY CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
C	3830	37U RANGE (1)	423 BTHG (1)
		+27 BPSIG (1)	426 3THG (1)
		+80 G21 (1)	479 GQ1 (1)
		+83 G23 (1)	492 GR2 (1)
		+86 G24 (1)	495 GQ4 (1)
		+90 G26 (1)	499 GR5 (1)
		+99 G21 (1)	495 GEOS (1)
		+99 G21 (1)	502 01 (1)
		+99 G21 (1)	506 002 (1)

ELIUV CLASSES	LENGTH	MEMBERS	BIAS NAME(LENGTH)
503 02	(1)	503 02	(1)
513 03	(1)	513 03	(1)
515 04	(1)	515 04	(1)
519 04	(1)	519 04	(1)
521 04	(1)	521 04	(1)
524 04	(1)	524 04	(1)
525 04	(1)	525 04	(1)
526 04	(1)	526 04	(1)
527 04	(1)	527 04	(1)
530 05	(1)	530 05	(1)
533 05	(1)	533 05	(1)
536 05	(1)	536 05	(1)
541 06	(1)	541 06	(1)
545 06	(1)	545 06	(1)
548 06	(1)	548 06	(1)
551 06	(1)	551 06	(1)
554 06	(1)	554 06	(1)
557 06	(1)	557 06	(1)
561 06	(1)	561 06	(1)
564 06	(1)	564 06	(1)
567 06	(1)	567 06	(1)
570 06	(1)	570 06	(1)
573 06	(1)	573 06	(1)
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579 06	(1)	579 06	(1)
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588 06	(1)	588 06	(1)
591 06	(1)	591 06	(1)
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597 06	(1)	597 06	(1)
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612 06	(1)	612 06	(1)
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618 06	(1)	618 06	(1)
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984 06	(1)	984 06	(1)
987 06	(1)	987 06	(1)
990 06	(1)	990 06	(1)
993 06	(1)	993 06	(1)
996 06	(1)	996 06	(1)
999 06	(1)	999 06	(1)

STATISTICS
PROGRAM LENGTH 4343 28*
ON LABELED COMMON LENGTH 73668 3038


```

      DMZ=TAZ*J0*CRAD
      GAO=DMZ*DMZ
      CONTINUE
      73      TCOMR=KRS*BPSIG/CRAD
      IF (ABS(9*PSIGD).LE.4.E-4) GO TO 80
      TFR=SIGN(FRI,BPSIG)
      TFR=TFR-TFR*TCOMR-TUI
      290      UMI=TA*CRAD/JI
      GO TO 83
      295      CONTINUE
      MRES=UCT*MRDUST*MPD
      TFR=IMR*TCOMR-TUI
      IF (ABS(MRES).GT.4.E-4) TFR=SIGN(FRI,TFR)
      300      NCOR=(TFR+SIGN(FRI,MRES))*CRAD/JI
      DMZ=NCOR
      IF (ABS(MRES).GT.4.E-4) DMZ=NCOR
      TFR=TFR-TFR*TCOMR-TUI
      DMZ=TAZ*JI*CRAD
      DMZ=DMZ*DMZ
      305      CONTINUE
      BTHGO=MI-MJ
      BPSIG=MI-(MR*UCT+MP*UST)
      3      CONTINUE
      RETURN
      310      END

```

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	
1 S2	1	309	
VARIABLES	SN	TYPE	RELOCATION
703 ANS	REAL		
704 ANX	REAL		
705 ANY	REAL		
706 ANZ	REAL		
707 ANA	REAL		
708 ANB	REAL		
709 ANC	REAL		
710 AND	REAL		
711 ANE	REAL		
712 ANF	REAL		
713 ANG	REAL		
714 ANH	REAL		
715 ANI	REAL		
716 ANJ	REAL		
717 ANK	REAL		
718 ANL	REAL		
719 ANM	REAL		
720 ANN	REAL		
721 ANO	REAL		
722 ANP	REAL		
723 ANQ	REAL		
724 ANR	REAL		
725 ANS	REAL		
726 ANT	REAL		
727 ANU	REAL		
728 ANV	REAL		
729 ANW	REAL		
730 ANX	REAL		
731 ANY	REAL		
732 ANZ	REAL		
733 ANA	REAL		
734 ANB	REAL		
735 ANC	REAL		
736 AND	REAL		
737 ANE	REAL		
738 ANF	REAL		
739 ANG	REAL		
740 ANH	REAL		
741 ANI	REAL		
742 ANJ	REAL		
743 ANK	REAL		
744 ANL	REAL		
745 ANM	REAL		
746 ANN	REAL		
747 ANO	REAL		
748 ANP	REAL		
749 ANQ	REAL		
750 ANR	REAL		
751 ANS	REAL		
752 ANT	REAL		
753 ANU	REAL		
754 ANV	REAL		
755 ANW	REAL		
756 ANX	REAL		
757 ANY	REAL		
758 ANZ	REAL		
759 ANA	REAL		
760 ANB	REAL		
761 ANC	REAL		
762 AND	REAL		
763 ANE	REAL		
764 ANF	REAL		
765 ANG	REAL		
766 ANH	REAL		
767 ANI	REAL		
768 ANJ	REAL		
769 ANK	REAL		
770 ANL	REAL		
771 ANM	REAL		
772 ANN	REAL		
773 ANO	REAL		
774 ANP	REAL		
775 ANQ	REAL		
776 ANR	REAL		
777 ANS	REAL		
778 ANT	REAL		
779 ANU	REAL		
780 ANV	REAL		
781 ANW	REAL		
782 ANX	REAL		
783 ANY	REAL		
784 ANZ	REAL		
785 ANA	REAL		
786 ANB	REAL		
787 ANC	REAL		
788 AND	REAL		
789 ANE	REAL		
790 ANF	REAL		
791 ANG	REAL		
792 ANH	REAL		
793 ANI	REAL		
794 ANJ	REAL		
795 ANK	REAL		
796 ANL	REAL		
797 ANM	REAL		
798 ANN	REAL		
799 ANO	REAL		
800 ANP	REAL		
801 ANQ	REAL		
802 ANR	REAL		
803 ANS	REAL		
804 ANT	REAL		
805 ANU	REAL		
806 ANV	REAL		
807 ANW	REAL		
808 ANX	REAL		
809 ANY	REAL		
810 ANZ	REAL		
811 ANA	REAL		
812 ANB	REAL		
813 ANC	REAL		
814 AND	REAL		
815 ANE	REAL		
816 ANF	REAL		
817 ANG	REAL		
818 ANH	REAL		
819 ANI	REAL		
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821 ANK	REAL		
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824 ANN	REAL		
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827 ANQ	REAL		
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829 ANS	REAL		
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831 ANU	REAL		
832 ANV	REAL		
833 ANW	REAL		
834 ANX	REAL		
835 ANY	REAL		
836 ANZ	REAL		
837 ANA	REAL		
838 ANB	REAL		
839 ANC	REAL		
840 AND	REAL		
841 ANE	REAL		
842 ANF	REAL		
843 ANG	REAL		
844 ANH	REAL		
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846 ANJ	REAL		
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850 ANN	REAL		
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853 ANQ	REAL		
854 ANR	REAL		
855 ANS	REAL		
856 ANT	REAL		
857 ANU	REAL		
858 ANV	REAL		
859 ANW	REAL		
860 ANX	REAL		
861 ANY	REAL		
862 ANZ	REAL		
863 ANA	REAL		
864 ANB	REAL		
865 ANC	REAL		
866 AND	REAL		
867 ANE	REAL		
868 ANF	REAL		
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875 ANM	REAL		
876 ANN	REAL		
877 ANO	REAL		
878 ANP	REAL		
879 ANQ	REAL		
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882 ANT	REAL		
883 ANU	REAL		
884 ANV	REAL		
885 ANW	REAL		
886 ANX	REAL		
887 ANY	REAL		
888 ANZ	REAL		
889 ANA	REAL		
890 ANB	REAL		
891 ANC	REAL		
892 AND	REAL		
893 ANE	REAL		
894 ANF	REAL		
895 ANG	REAL		
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897 ANI	REAL		
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901 ANM	REAL		
902 ANN	REAL		
903 ANO	REAL		
904 ANP	REAL		
905 ANQ	REAL		
906 ANR	REAL		
907 ANS	REAL		
908 ANT	REAL		
909 ANU	REAL		
910 ANV	REAL		
911 ANW	REAL		
912 ANX	REAL		
913 ANY	REAL		
914 ANZ	REAL		
915 ANA	REAL		
916 ANB	REAL		
917 ANC	REAL		
918 AND	REAL		
919 ANE	REAL		
920 ANF	REAL		
921 ANG	REAL		
922 ANH	REAL		
923 ANI	REAL		
924 ANJ	REAL		
925 ANK	REAL		
926 ANL	REAL		
927 ANM	REAL		
928 ANN	REAL		
929 ANO	REAL		
930 ANP	REAL		
931 ANQ	REAL		
932 ANR	REAL		
933 ANS	REAL		
934 ANT	REAL		
935 ANU	REAL		
936 ANV	REAL		
937 ANW	REAL		
938 ANX	REAL		
939 ANY	REAL		
940 ANZ	REAL		
941 ANA	REAL		
942 ANB	REAL		
943 ANC	REAL		
944 AND	REAL		
945 ANE	REAL		
946 ANF	REAL		
947 ANG	REAL		
948 ANH	REAL		
949 ANI	REAL		
950 ANJ	REAL		
951 ANK	REAL		
952 ANL	REAL		
953 ANM	REAL		
954 ANN	REAL		
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957 ANQ	REAL		
958 ANR	REAL		
959 ANS	REAL		
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961 ANU	REAL		
962 ANV	REAL		
963 ANW	REAL		
964 ANX	REAL		
965 ANY	REAL		
966 ANZ	REAL		
967 ANA	REAL		
968 ANB	REAL		
969 ANC	REAL		
970 AND	REAL		
971 ANE	REAL		
972 ANF	REAL		
973 ANG	REAL		
974 ANH	REAL		
975 ANI	REAL		
976 ANJ	REAL		
977 ANK	REAL		
978 ANL	REAL		
979 ANM	REAL		
980 ANN	REAL		
981 ANO	REAL		
982 ANP	REAL		
983 ANQ	REAL		
984 ANR	REAL		
985 ANS	REAL		
986 ANT	REAL		
987 ANU	REAL		
988 ANV	REAL		
989 ANW	REAL		
990 ANX	REAL		
991 ANY	REAL		
992 ANZ	REAL		
993 ANA	REAL		
994 ANB	REAL		
995 ANC	REAL		
996 AND	REAL		
997 ANE	REAL		
998 ANF	REAL		
999 ANG	REAL		
1000 ANH	REAL		

SUBROUTINE S2			74/74	OPT=1	FTN 4.2*74355			08/07/73	11.07.46.	PAGE	10	
VARIABLES	SN	TYPE	RELOCATION									
740 TFR		REAL			291	292	293	299	302	DEFINED	291	297
716 TATQAR		REAL			REFS	234	237	DEFINED	232			
717 THQAR		REAL			REFS	235	237	DEFINED	233			
1140 THIQ		REAL		C	REFS	60	193	232	DEFINED	191		
1141 THIR		REAL		C	REFS	60	194	233	DEFINED	192		
3717 TIME		REAL		C	REFS	71	190	199	190	195	206	238
1211 TIMESV		REAL		C	REFS	79	193	175	196	197		
					DEFINED	175	190					
1135 FLAG		REAL		C	REFS	61	195					
727 TMQ		REAL			REFS	276	290	291	285	DEFINED	267	
730 TFR		REAL			REFS	282	297	296	302	DEFINED	268	
725 TX		REAL			REFS	2*265	267	DEFINED	263	265		
726 TX		REAL			REFS	2*266	269	DEFINED	264	266		
707 IT-AU		REAL			REFS	196	197	DEFINED	195			
1070 TUI		REAL		C	REFS	46	292	297	302	DEFINED	463	
1071 TUD		REAL		C	REFS	47	275	290	285	DEFINED	162	
004 U811		REAL			REFS	149	153	DEFINED	136			
005 U812		REAL			REFS	149	153	DEFINED	139			
006 U813		REAL			REFS	149	153	DEFINED	140			
007 U821		REAL			REFS	150	157	DEFINED	141			
070 U822		REAL			REFS	150	157	DEFINED	142			
071 U823		REAL			REFS	150	157	DEFINED	143			
072 U831		REAL			REFS	151	153	DEFINED	144			
073 U832		REAL			REFS	151	153	DEFINED	145			
074 U833		REAL			REFS	151	153	DEFINED	146			
1152 UC2		REAL		C	REFS	122	163					
1154 UC2G		REAL		C	REFS	123	159					
002 UC3		REAL			REFS	138	140	142	222	DEFINED	136	
000 UC7		REAL			REFS	139	141	146	162	222	296	307
					DEFINED	134						
1153 US2		REAL		C	REFS	122	163					
1152 US2G		REAL		C	REFS	123	153					
003 US4		REAL			REFS	139	141	143	222	DEFINED	137	
001 US7		REAL			REFS	140	143	144	162	222	296	307
					DEFINED	135						
734 M00Q		REAL			REFS	2*284	299	332				
743 M00R		REAL			REFS	2*301	299					
1100 M01		REAL		C	REFS	26	255					
1102 M02		REAL		C	REFS	28						
1104 M03		REAL		C	REFS	30	254					
1100 M04		REAL		C	REFS	32	256					
1110 M05		REAL		C	REFS	34	261					
1112 M06		REAL		C	REFS	36	3*258					
1101 M081		REAL		C	REFS	27	257					
1103 M082		REAL		C	REFS	29						
1105 M083		REAL		C	REFS	31	253					
1107 M084		REAL		C	REFS	33	257					
1111 M085		REAL		C	REFS	35	264					
1113 M086		REAL		C	REFS	37	3*259					
712 M087		REAL		C	REFS	205	DEFINED	204	205			
1012 M1		REAL		C	REFS	97	224	307				
022 M1M2		REAL		C	REFS	105	DEFINED	244				
020 M1M3		REAL		C	REFS	107	DEFINED	245				
1004 M1		REAL		C	REFS	94	222	306				
1112 M1		REAL		C	REFS	67	222	307				

C JYMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

C 3850 0 138301

C EUJIV CLASSES LENGTH MEMBERS - BINS NAME(LENGTH)

C 3850

370 RANGE	(1)	371 RV3A	(1)	372 RV3A	(1)
373 R25A	(1)	402 MLCAR	(1)	405 MLCAR	(1)
423 BTHJG	(1)	426 BTHJG	(1)	427 SP51G	(1)
430 BPSZS	(1)	434 BPSZS	(1)	435 BPSZS	(1)
479 G31	(1)	481 G32	(1)	481 G32	(1)
482 G32	(1)	483 G33	(1)	484 G33	(1)
485 G34	(1)	486 G34	(1)	486 G35	(1)
489 G35	(1)	490 G35	(1)	491 G35	(1)
492 DTHCQ	(1)	493 DTHCQ	(1)	494 DTHCQ	(1)
495 BTHKSR	(1)	496 BTHKSR	(1)	499 D04	(1)
500 D31	(1)	502 D31	(1)	513 D31	(1)
505 D02	(1)	506 D02	(1)	508 D32	(1)
509 D2	(1)	511 D03	(1)	512 D03	(1)
513 D40	(1)	514 D3	(1)	515 D3	(1)
516 D3	(1)	517 D0D4	(1)	518 D0D4	(1)
519 D01	(1)	520 D04	(1)	521 D04	(1)
522 M1SPYSV	(1)	523 D04	(1)	524 D04	(1)
525 BPSZS	(1)	526 D0D5	(1)	527 D0D5	(1)
528 BPSZS	(1)	529 D05	(1)	530 D05	(1)
532 D5	(1)	533 D5	(1)	535 D0D5	(1)
536 D0D6	(1)	538 D06	(1)	539 D06	(1)
541 D5	(1)	542 D6	(1)	544 D04	(1)
545 K31	(1)	546 K02	(1)	547 K02	(1)
548 K03	(1)	549 K03	(1)	550 K05	(1)
551 K35	(1)	552 K05	(1)	553 K05	(1)
554 K27	(1)	555 K07	(1)	556 K08	(1)
557 K08	(1)	558 K010	(1)	559 K010	(1)
560 K011	(1)	561 K011	(1)	562 K012	(1)
563 K012	(1)	564 JI	(1)	565 JI	(1)
566 F01	(1)	567 F01	(1)	568 T01	(1)
569 T01	(1)	570 QRG	(1)	571 R05	(1)
572 M101	(1)	573 M101	(1)	574 M102	(1)
575 M102	(1)	576 M021	(1)	577 M021	(1)
578 M022	(1)	579 M022	(1)	580 M021	(1)
581 M023	(1)	582 M024	(1)	583 M024	(1)
584 M025	(1)	585 M025	(1)	586 M026	(1)
587 M026	(1)	588 M021	(1)	589 M021	(1)
590 M022	(1)	591 M022	(1)	592 M023	(1)
593 M023	(1)	594 M024	(1)	595 M024	(1)
596 M02	(1)	597 M024	(1)	598 M024	(1)
599 T01	(1)	600 T02	(1)	601 T02	(1)
602 R0LOCK	(1)	603 F0V	(1)	604 T0C5	(1)
605 T0AG	(1)	606 B0KQ	(1)	607 T0ELAY	(1)
608 T0TQ	(1)	609 T0TQ	(1)	610 K00	(1)
611 K01	(1)	612 K01	(1)	613 K01	(1)
614 K02	(1)	615 K01	(1)	616 K02	(1)
617 K0AI	(1)	618 UCC	(1)	619 UCC	(1)
620 D0G6	(1)	621 D0G6	(1)	624 IRL	(1)
649 T0MESV	(1)	655 L0S2	(1)	651 L0S2	(1)
1675 ANGZ	(1)	1676 ANGZ	(1)	1677 ANGZ	(1)
1735 M0	(1)	1736 M0	(1)	1739 M00	(1)
1742 M0	(1)	1743 M00	(1)	1746 M0	(1)
1750 C0AD	(1)	1751 T045	(1)	2019 L0OMP	(1)
3511 B551E	(1)	3533 IS0JX	(1)		

SUBROUTINE S2 74/74 OPT=1 FTN 4.2+74.355 07/07/75 11.07446. PAGE 13

STATISTICS

PROGRAM LENGTH	7906	485
CM LABELED COMMON LENGTH	73663	3830

60	EQUIVALENCE (C(11743), M)	53	59
	EQUIVALENCE (C(11743), M)	53	60
	EQUIVALENCE (C(11747), M)	53	61
	EQUIVALENCE (C(11751), CRAD)	53	62
	EQUIVALENCE (C(12000), TIME)	53	63
	EQUIVALENCE (C(371), RANGE)	53	64
	EQUIVALENCE (C(11667), ANG1)	53	65
	EQUIVALENCE (C(11677), ANG2)	53	66
	EQUIVALENCE (C(11678), ANG3)	53	67
	EQUIVALENCE (C(11736), MPD)	53	68
	EQUIVALENCE (C(11740), MDS)	53	69
	EQUIVALENCE (C(11744), MDD)	53	70
70	EQUIVALENCE (C(370), TIME3)	53	71
	EQUIVALENCE (C(556), LOSZ)	53	72
	EQUIVALENCE (C(562), LOSY)	53	73
	REAL LOSZ, LOSY	53	74
75	DIMENSION TIMESV(6), LOSZ(6), LOSY(6), XL(2)	53	75
	C	53	76
	C**STATE VARIABLES	53	77
	EQUIVALENCE (C(424), BPSIG)	53	78
	EQUIVALENCE (C(428), BPSIG)	53	79
	EQUIVALENCE (C(500), DUL)	53	80
80	EQUIVALENCE (C(501), DR1)	53	81
	EQUIVALENCE (C(506), D2)	53	82
	EQUIVALENCE (C(507), DR2)	53	83
	EQUIVALENCE (C(512), DR3)	53	84
	EQUIVALENCE (C(513), DR3)	53	85
85	EQUIVALENCE (C(514), DR3)	53	86
	EQUIVALENCE (C(517), DR3)	53	87
	EQUIVALENCE (C(520), DR3)	53	88
	C**OTHER OUTPUTS	53	89
90	EQUIVALENCE (C(435), BPSY)	53	90
	EQUIVALENCE (C(436), BPSY)	53	91
	EQUIVALENCE (C(403), MLAMQ)	53	92
	EQUIVALENCE (C(407), MLAMR)	53	93
	EQUIVALENCE (C(526), BPSYSV)	53	94
95	EQUIVALENCE (C(527), BPSYSV)	53	95
	EQUIVALENCE (C(493), DTHC3)	53	96
	EQUIVALENCE (C(495), DTHRC3)	53	97
	EQUIVALENCE (C(520), LCOM4)	53	98
	EQUIVALENCE (C(507), BRKQ)	53	99
100	C**UNTE CARLO PARAMETERS	53	100
	EQUIVALENCE (C(503), ISNOK)	53	101
	EQUIVALENCE (C(511), KUI)	53	102
	EQUIVALENCE (C(513), K81)	53	103
105	EQUIVALENCE (C(515), K81)	53	104
	EQUIVALENCE (C(517), K81)	53	105
	EQUIVALENCE (C(519), K81)	53	106
	EQUIVALENCE (C(521), K81)	53	107
	EQUIVALENCE (C(519), UG3)	53	108
	EQUIVALENCE (C(521), UG3)	53	109
110	DATA FOW**	53	110
	C INTEGRATION SWITCHING TEST	53	111
	C	53	112
	IF (U3).LE.0.1) GO TO 1	53	113
	G(113)=-1.	53	114
		53	115

SUBROUTINE S3	74/74	OPT=1	FTN 4,2,74,355	07/07/75	11.08.03.	PAGE	3
119	C12547=TRUAIMTTRU/C127047					S3	116
	1	CONTINUE				S3	117
	C					S3	118
	C**DIRECTION COSINES FOR BODY TO PLATFORM TRANSFORMATION					S3	119
120	UCT=COS(THIC)					S3	120
	UST=SIN(THIC)					S3	121
	UCP=COS(THIC)					S3	122
	USP=SIN(THIC)					S3	123
	UB11=UCT*UCP					S3	124
	UB12=USP					S3	125
125	UB13=UCP*UST					S3	126
	UB21=UCT*USP					S3	127
	UB22=USP					S3	128
	UB23=UST*USP					S3	129
	UB31=UST					S3	130
130	UB32=0.					S3	131
	UB33=UCT					S3	132
	C					S3	133
	C**TRANSFORM LOS FROM BODY TO GINIAL AXES					S3	134
	RLG=UB11*RXBA+UB12*RYBA+UB13*RZBA					S3	135
	RYG=UB21*RXBA+UB22*RYBA+UB23*RZBA					S3	136
135	RZG=UB31*RXBA+UB32*RYBA+UB33*RZBA					S3	137
	IF(13542.LE.0.160 TO 5					S3	138
	C**CYRO ERRORS					S3	139
	C					S3	140
140	C**TRANSFORM NORMALIZED ACCELERATIONS FROM BODY TO GINIAL AXES					S3	141
	ANGX=UB11*ANGX+UB12*ANGY+UB13*ANGZ					S3	142
	ANGY=UB21*ANGX+UB22*ANGY+UB23*ANGZ					S3	143
	ANGZ=UB31*ANGX+UB32*ANGY+UB33*ANGZ					S3	144
	ANG=ANGZ*UCCG+ANGY*USCG					S3	145
145	GRG=KRG*KPI*ANG+KRG*MPD					S3	146
	RLG=KRG*KPI*ANG+KRG*MPD					S3	147
	TUO=KRG*(ANG*UCT+ANG*UST)					S3	148
	TUI=KUI*(ANGY*UCC+ANG*UCC)					S3	149
150	CONTINUE					S3	150
	C					S3	151
	C**LOS ERRORS IN PLATFORM COORDINATES					S3	152
	IF(C11375).LE.0.160 TO 32					S3	153
	BEPSZ=ATAN2(R2G,R1G)					S3	154
	BEPSZ=ATAN2(R1G,R2G)					S3	155
155	C****SAVE THE PREVIOUS FIVE POINTS IN TIME OF BEPSZ AND BEPSY FOR FLAG.					S3	156
	DO 2 L=2,6					S3	157
	TIME=SVTL-17=TIME+VTL					S3	158
	LOSZ(L-1)=LOSZ(L)					S3	159
	LOSZ(L)=LOSZ(L)					S3	160
160	CONTINUE					S3	161
	TIME=SV(L)=TIME					S3	162
	LOSZ(L)=BEPSZ					S3	163
	LOSZ(L)=BEPSY					S3	164
165	CONTINUE					S3	165
	C					S3	166
	C					S3	167
	C					S3	168
	C					S3	169
	C					S3	170
170	C**ZON AT DELAY-TAU AND TIME DELAY-FLAG					S3	171
	IF(TIME+VTL-17).GT.0.000110R.C(1761).LE.0.160 TO 30					S3	172
	LOC=AY=TIME+VTL					S3	173


```

175  TMT2=TIME-TMRMT2-RANGE
    BRKQ=(BEP2-BEPS2)/12.*TMTQ
    BRKR=(BEP2-BEPS2)/12.*TMTQ
    TLAG=TIME-TLAG $ N=6 $ #0.
    BEPS2=INTPI1 TLAG,TIME,LOSZ,N,F,XL
    BEPS2=INTPI1 TLAG,TIME,LOSZ,N,F,XT
    IF (ABS(BRKQ) .LT. .5) GO TO 30
    C**BREAKLOCK DETERMINATION
    IF (OCS.NE.-10) GO TO 30
    IBL=IBL+1
    LCONV=2
    GOCS=9
    WHICH = 10H IN PITCH
    IF (ABS(BRKQ) .GE. .5) WHICH = 10H IN YAW
    WRITE(6,10) TIME,RANGE,WHICH
101  * RANGE = *F10.2,A10,100(1H*))
190  30 CONTINUE
    CELAYQ=Q1*BEP2SV
    DELAYR=GR1*BEP2SV
    Q1= DELAYQ-WTQ2*Q1
    ORI= DELAYR-WTQ2*Q1
    DTMCQ=40Q1-WTQ1*Q1*GQ2
    DTMCQ=ORI-WTQ1*Q1*GQ2
    RATE COMMAND LIMIT
    IF (ABS(DTMCQ).GT.RCL) DTMCQ=SIGN(RCL,DTMCQ)
    IF (ABS(DTMCQ).GT.RCL) DTMCQ=SIGN(RCL,DTMCQ)
200  C
    C RATE GYRO LOOP
    C
    WLO=WD*UCP-(WP*UCL-WR*UST)*JSP
    WGO=GO*(WIQ+QERG)
    WGR=GR*(WI+KERS)
    DTMCQ=Q12*WGO
    DTMCQ=KRL2*WGR
210  C**BLIND RANGE DETERMINATION
    TMTQ=TMTQ+ABS(BEPS2)
    TMTQ=TMTQ+ABS(BEPS2)
    BLNQ=TMTQ+2.*FOV
    BLNR=TMTQ+2.*FOV
    TESTFOV=FOV*FOV*2.
    IF (TMTQ.LT.TESTFOV) TMTQ=TMTQ+2.*FOV
    IF (OCS.LE.0) WRITE(6,100) TIME,RANGE
100  FORMAT (10H,100(1H*)) * OCS BLIND RANGE SIGNAL HOLD AT TIME = *F5.2,
    * RANGE = *F10.2/100(1H*))
    GOCS=10
    GO TO 21
220  20 CONTINUE
    C
    C**OUTPUT TO AUTOPILOT
    WLAB=GEOS*WGO
    WLAB=GEOS*WGR
    IF (ABS(WLAB).GT.1) TLAG=ABS(WLAB)+TLAG
    IF (ABS(WLAB).GT.1) TLAG=ABS(WLAB)+TLAG
21  CONTINUE

```

SUBROUTINE S3	74774	UPI=1	FTN 4.2+74355	07/0775	11.08.03.	PAGE	5
230	C	C	SAIN COMPENSATION	S3	230		
	C		DTHEQ=OTHQ-OTHQ2	S3	231		
			DTHTER=OTHCR-OTHGR	S3	232		
			DQ2= DTHTEQ	S3	233		
235			DR2= DTHTER	S3	234		
			LQ3=D2+MGQ1*Q2-MGQ4*Q3	S3	235		
			DR3=DK2+MGK1*R2-MGK4*R3	S3	236		
240	C	C	SEEKER TORQUE MOTOR	S3	237		
	C		TQ=Q33+TQ33+MGQ3*Q3	S3	238		
			TR=K3*(Q33+MGK3*R3)	S3	239		
			IF (ABS(TQ).GT.TCLQ)TQ=SIGN(TCLQ,TQ)	S3	240		
			IF (ABS(TR).GT.TCLR)TR=SIGN(TCLR,TR)	S3	241		
245			TQ=Q33+TQ	S3	242		
			TR=Q33+TR	S3	243		
	C		SEEKER GIMBAL ANGLE RATES	S3	244		
	C		C**COULOM3 FRICTION MODEL	S3	245		
250			TCUM=KQ3*BTHG/CRAO	S3	246		
			IF (ABS(BTHG).LE.*E-4)GO TO 70	S3	247		
			IFQ= SIGN(FRQ*BTHG)	S3	248		
255			TAQ=INQ-TFQ-TCONQ-TUO	S3	249		
			DMU=TAQ*CRAO/JO	S3	250		
	70		GO TO 73	S3	251		
			CONTINUE	S3	252		
260			IFQ=INQ-TCONQ-TUO	S3	253		
			IF (ABS(TFQ).GT.*E-4)TFQ=SIGN(TFQ,TFQ)	S3	254		
			MCCQ=IFQ*SIGN(FRQ,MQ3)*CRAO/JO	S3	255		
			DMJQ=MCCQ	S3	256		
			IF (ABS(MQ3).GT.ABS(MCQ3))DMJQ=MCCQ	S3	257		
			TAQ=INQ-TFQ-TCONQ-TUO	S3	258		
265			DMJQ=TAQ/JO*CRAO	S3	259		
	73		DMQ=DMJQ+DMQ	S3	260		
			CONTINUE	S3	261		
			TCUM=KQ3*BPSIG/CRAO	S3	262		
			IF (ABS(BPSIG).LE.*E-4)GO TO 80	S3	263		
270			TFQ=SIGN(FRQ,BPSIG)	S3	264		
			TAR=TR-TFR-TCONR-TUI	S3	265		
			DMT=TAR*CRAD/JO	S3	266		
	80		CONTINUE	S3	267		
			HRCS=UCT*HRQ+UST*MFQ	S3	268		
275			TFM=TRM-TCONR-TUI	S3	269		
			IF (ABS(TFR).GT.FRI)TFQ=SIGN(FRI,TFM)	S3	270		
			MCCQ=TFQ*SIGN(FRI,MRES)*CRAD/JO	S3	271		
			DMK=MCCQ	S3	272		
			IF (ABS(MRES).GT.ABS(MCONR))DMK=MCCQ	S3	273		
280			TAR=TR-TFR-TCONR-TUI	S3	274		
			DMR=TAR/JO*CRAO	S3	275		
			DMI=DMK+DMR	S3	276		
	83		CONTINUE	S3	277		
			BTMGU=HQ-MQ	S3	278		
285			BPSIG=MI-(TR*UCT+MP*UST)	S3	279		

SUBROUTINE S3 7/4/74 OPT=1 FTN 4.2.74353 07/07/75 11.08.03. PAGE 6

3 CONTINUE
RETURN
END

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S3
S3
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VARIABLES		SN	TYPE	RELOCATION	REFS	10	194	203	178
1077	MT2		REAL	C	REFS	204	DEFIN'D		
650	M12		REAL		REFS	74	177		
703	XL		REAL	ARRAY					
FILE NAMES		MODE	WRITES	187	216				
TAP26		FMT							
EXTERNALS		TYPE	ARGS	REFERENCES	154	172	173		
ATAND		REAL	2	153					
COSD		REAL	1	119	121				
PINTPI		REAL	5	177	170				
SIND		REAL	1	120	122				
INLINE FUNCTIONS		TYPE	ARGS	DEF LINE REFERENCES	106	199	210	211	2+227
ABS		REAL	1	INTRIN	243	252	2+262	260	2+279
AINT		REAL	1	INTRIN	115				
SL2N		REAL	2	INTRIN	198	199	243	253	259
					276	277		260	269
STATEMENT LABELS		DEF LINE	REFERENCES						
10	1	116							
0	1	160							
0	1	INACTIVE							
114	1	149		137					
301	20	221		285					
314	21	228		280					
214	30	190		170	179	181			
136	32	164		152					
371	70	257		252					
423	73	266		256					
440	80	273		258					
475	83	263		272					
566	100	FMT		217					
547	101	FMT		180					
LOOPS LABEL		INDEX	FROM-TO	LENGTH	PROPERTIES				
127	2	L	156	160	3B INSTACK				
COMMON BLOCKS		LENGTH	MEMBERS	- BIAS NAME(LENGTH)					
C		3030		0 C (3030)					
EQUIV CLASSES		LENGTH	MEMBERS	- BIAS NAME(LENGTH)					
C		3030		370 RANGE (11)	371 RXBA (11)	372 RYBA (11)			
				373 REBA (11)	402 MLAMB (11)	405 MLAMB (11)			
				423 BTHICQ (11)	425 BTHICQ (11)	427 BTHICQ (11)			
				430 BPSIG (11)	434 BPSIG (11)	435 BPSIG (11)			
				473 G21 (11)	480 G21 (11)	491 G21 (11)			
				482 G22 (11)	483 G22 (11)	494 G22 (11)			
				485 G24 (11)	486 G24 (11)	498 G24 (11)			
				489 G25 (11)	490 G25 (11)	491 G25 (11)			
				492 DTHCQ (11)	493 DTHCQ (11)	494 DTHCQ (11)			
				495 DTHCQ (11)	496 DTHCQ (11)	497 DTHCQ (11)			
				500 D21 (11)	502 D21 (11)	503 D21 (11)			
				505 D22 (11)	506 D22 (11)	507 D22 (11)			
				509 D2 (11)	511 D2 (11)	512 D2 (11)			
				513 D40 (11)	514 D40 (11)	515 D40 (11)			

EQUIV CLASSES	LENGTH	MEMBERS - BIAS NAME(LENGTH)
516 K21	(1)	519 DM1 (1)
525 BEPSYSV(1)	(1)	526 BEPSYSV(1)
545 K21	(1)	546 K22 (1)
549 K23	(1)	550 K25 (1)
551 K25	(1)	552 K26 (1)
554 K27	(1)	555 K28 (1)
557 K29	(1)	558 K29 (1)
560 K311	(1)	561 K311 (1)
563 K312	(1)	564 J1 (1)
566 F21	(1)	567 F21 (1)
569 T20	(1)	570 QERS (1)
572 M21	(1)	573 M21 (1)
575 M22	(1)	576 M22 (1)
578 M22	(1)	579 M22 (1)
581 M23	(1)	582 M24 (1)
584 M25	(1)	585 M25 (1)
587 M26	(1)	588 M26 (1)
590 M27	(1)	591 M27 (1)
593 M28	(1)	594 M28 (1)
596 K21	(1)	597 K21 (1)
599 T20	(1)	600 T20 (1)
602 RELOCK	(1)	603 F20 (1)
605 T20	(1)	606 T20 (1)
608 T20	(1)	609 T20 (1)
611 K21	(1)	612 K21 (1)
614 K21	(1)	615 K21 (1)
617 K21	(1)	618 K21 (1)
620 J20	(1)	621 J20 (1)
649 TIMESV	(6)	655 LOSZ (6)
1675 ANGZ	(1)	1676 ANGZ (1)
1735 M20	(1)	1736 M20 (1)
1742 M2	(1)	1743 M2 (1)
1750 C20	(1)	1999 TIME (1)
3511 I3512	(1)	3633 ISNOX (1)

STATISTICS

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